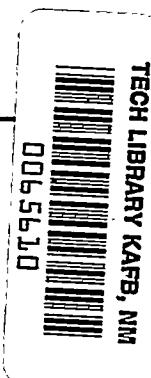


NACA TN 2451 E 488



NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

TECHNICAL NOTE 2451

MATHEMATICAL IMPROVEMENT OF METHOD FOR COMPUTING POISSON
INTEGRALS INVOLVED IN DETERMINATION OF VELOCITY
DISTRIBUTION ON AIRFOILS

By I. Flügge-Lotz

Stanford University



Washington
October 1951

AFMRC
TECHNICAL LIBRARY
AFGL 2811



0065610

TECHNICAL NOTE 2451

MATHEMATICAL IMPROVEMENT OF METHOD FOR COMPUTING POISSON

INTEGRALS INVOLVED IN DETERMINATION OF VELOCITY

DISTRIBUTION ON AIRFOILS

By I. Flügge-Lotz

SUMMARY

The Poisson integral involved in the determination of the change in velocity distribution resulting from a change in airfoil profile in parallel incompressible flow is solved.

First, three well-developed numerical methods of evaluating this integral, all based on the division of the range of integration into small equal intervals, and the difficulties involved in each method, are discussed. Then a new method, based on the use of unequal intervals, is developed, and compared with the other methods by means of several examples. The new method is found to give good results for both the direct and inverse airfoil problems and is easily adaptable to rather complicated problems. It is particularly recommended for all those functions where steep slopes in small portions of the region to be integrated exist.

INTRODUCTION

The ordinary thin airfoil at small angles of attack produces only slight disturbances in the flow of a parallel incompressible fluid. Hence, the influences of camber and thickness upon the velocity distribution may be computed independently and their effects superimposed. The effect of camber may be represented by vortices distributed along the chord line of the airfoil section; the effect of the thickness, by sources and sinks also along the same chord line. The velocities produced by these singularity distributions enable one to compute the pressure distribution on the airfoil rather quickly.

Allen (reference 1) has presented this singularity method in a form which has proved to be very practical for common usage. However, in special cases the unavoidable evaluation of the Poisson integral in

the course of the computations has given rise to numerical difficulties. Such integrals are usually computed by the application of finite differences using intervals of equal length. However, changes in airfoil shape, which result in marked changes in the function to be integrated in only small portions of the range of integration, require that extremely small interval sizes be employed in this range, and, consequently over the entire range of integration. This leads to a considerable amount of computational work; hence, it appears reasonable to discuss the possibility of employing intervals of varying lengths for the evaluation of the Poisson integral.

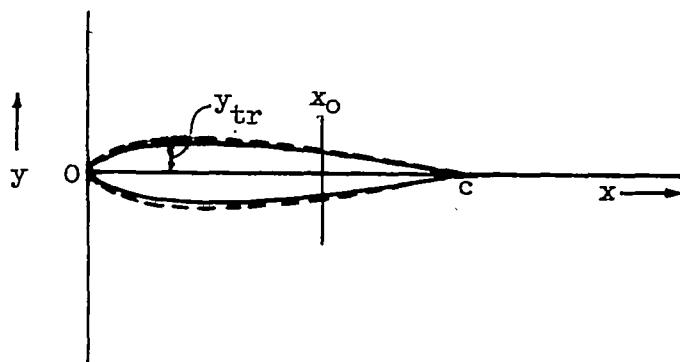
This investigation was prompted by the difficulties arising from the problem of small changes in the shape of symmetrical airfoils at the angle of zero lift. The examples included in the present report are restricted to this case, but the results obtained are in no way specialized and may be applied to all problems wherein the Poisson integral occurs.

This work was done at Stanford University under the sponsorship and with the financial assistance of the National Advisory Committee for Aeronautics.

The author wishes to express her appreciation to Mr. H. Norman Abramson for his intelligent and skillful help in the computational work and for his assistance in writing the final report. The author also wishes to extend her thanks to Mr. R. E. Dannenberg and the computing staff of the 7- by 10-foot wind-tunnel section of the Ames Aeronautical Laboratory, Moffett Field, California, for preparing the extended tables of the functions j_{no} and j_{no}^* .

DISCUSSION OF PROBLEM

The basic reference profile may be given by $y_{tr} = f(x)$, and its velocity distribution may be known from an earlier computation. The problem at hand is that of determining the change in the velocity distribution resulting from a change in the shape of the profile (indicated by the dotted line in the following fig.). The difference of these two shapes is designated as Δy_t .



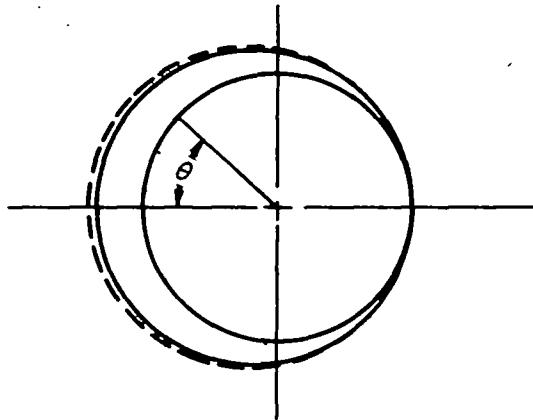
Allen (reference 1, p. 7) gives for the change of velocity the equation

$$\frac{\Delta v(x_0)}{V_o} = -\frac{1}{\pi} \int_0^c \frac{d(\Delta y_t)}{\frac{dx}{x - x_0}} dx \quad (1)$$

where V_o is the velocity of the basic parallel flow. If, by conformal mapping of the outside flow region, the center line of the profile is transformed into a circle by the relation

$$x = \frac{c}{2} (1 - \cos \theta) \quad (2)$$

then the profile is transformed into a curve approximating the circle shown below.



The change in velocity due to a change in form will then be given as

$$\frac{\Delta v}{V_o} (\theta_0) = - \frac{1}{2\pi} \int_0^{2\pi} \frac{d(\Delta y_t)}{dx} \cot \frac{\theta - \theta_0}{2} d\theta \quad (3)$$

defining

$$\left[\frac{d(\Delta y_t)}{dx} \right]_{\pi+\theta} = - \left[\frac{d(\Delta y_t)}{dx} \right]_{\pi-\theta}$$

This is the form most often used for computation purposes, because the inverse problem (that of computing the change in shape due to a change in velocity distribution) utilizes the analytic form

$$\left[\frac{d(\Delta y_t)}{dx} \right]_{x_0} = \frac{1}{2\pi} \int_0^{2\pi} \frac{\Delta v}{V_o} \cot \left(\frac{\theta - \theta_0}{2} \right) d\theta \quad (4)$$

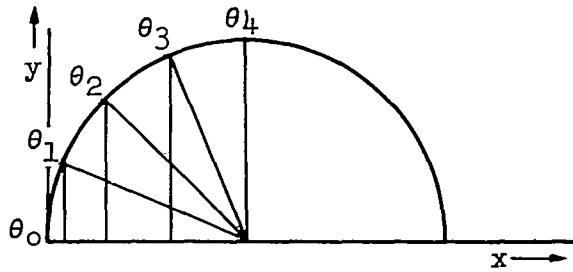
defining

$$\left(\frac{\Delta v}{V_o} \right)_{\pi+\theta} = \left(\frac{\Delta v}{V_o} \right)_{\pi-\theta}$$

which is strikingly similar. The corresponding formula in the original x,y coordinate system is given by

$$\left[\frac{d(\Delta y_t)}{dx} \right]_{x_0} = \frac{1}{\pi} \int_0^c \frac{\frac{\Delta v}{V_o}}{x - x_0} \frac{\sqrt{x_0(c - x_0)}}{\sqrt{x(c - x)}} dx \quad (5)$$

The evaluation of equation (3) may be accomplished by any one of several different methods; however, all of these methods employ the device of replacing the integral over the range 0 to 2π by a sum of integrals over intervals of equal length $\Delta\theta$. The equally distributed points θ_n have corresponding values x_n which are not equally distributed (see following fig.).



This arrangement is sometimes favorable, and sometimes not, depending upon the particular form of $\frac{d(\Delta y_t)}{dx}$. (See discussion following equation (43).)

The use of the angular coordinate θ has the advantage that the functions $\frac{d(\Delta y_t)}{dx}$ or $\frac{\Delta v}{V_0}$ are periodic functions in θ , and this

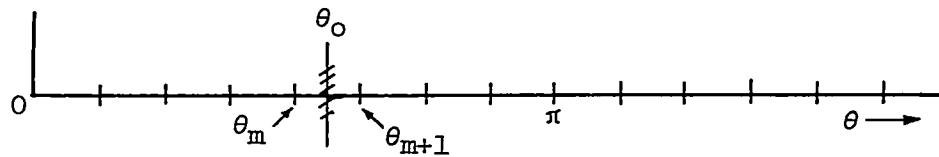
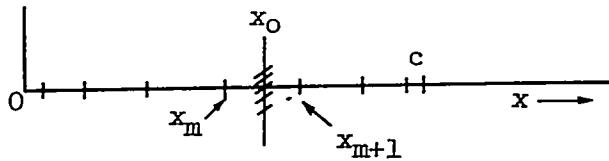
periodicity facilitates the organization of the numerical computations. The disadvantage arises from the fact that these functions are usually given as functions of x , and, since the analytic form is not usually known, any transformations made will lead to small errors. For example,

if $\frac{d(\Delta y_t)}{dx}$ or $\frac{\Delta v}{V_0}$ is given at special points which do not correspond

to $\theta_n = n\Delta\theta$, then the computer must obtain the values of these functions for the values θ_1, θ_2 , and so forth by interpolation.

DISCUSSION OF SOME OF THE EXISTING NUMERICAL SOLUTIONS OF POISSON INTEGRAL

The difficulty encountered in the solution of the Poisson integral arises from the fact that the term $\cot \frac{(\theta - \theta_0)}{2}$ or $\frac{1}{x - x_0}$ (equations (1) and (3), e.g.) approaches infinity when θ approaches θ_0 or when x approaches x_0 . The difficulty is of much less consequence when the function $\frac{d(\Delta y_t)}{dx}$ or $\frac{\Delta v}{V_0}$ is given analytically than when a numerical computation is undertaken. As a consequence, any simple integration, performed by replacing the integral with a summation over smaller intervals, always requires that the interval in which θ_0 or x_0 is located be given special consideration (see following fig.).



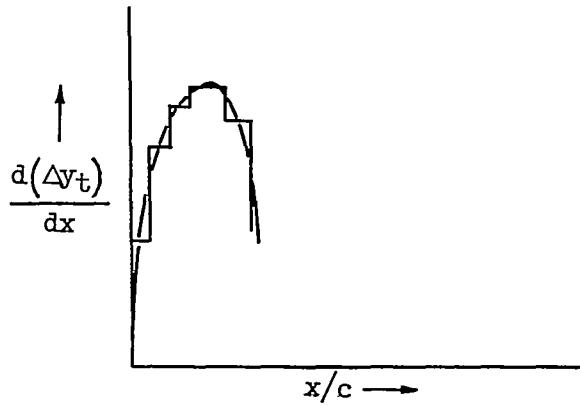
A majority of the solutions currently in use have been developed to such an extent that, for example, $\frac{\Delta v}{v_o}(\theta_0)$ is given by a sum of products of single values of $\left(\frac{d(\Delta y_t)}{dx} \right)_n$ and known factors A_n ; that is,

$$\begin{aligned}
 \frac{\Delta v}{v_o}(\theta_0) &= -\frac{1}{2\pi} \int_0^{2\pi} \frac{d(\Delta y_t)}{dx} \cot \left(\frac{\theta - \theta_0}{2} \right) d\theta \\
 &= -\frac{1}{2\pi} \int_{-\theta_0}^{2\pi - \theta_0} \frac{d(\Delta y_t)}{dx} \cot \frac{\theta^*}{2} d\theta^* \\
 &= -\frac{1}{2\pi} \sum_n \int_{\theta_n^*}^{\theta_{n+1}^*} \frac{d(\Delta y_t)}{dx} \cot \frac{\theta^*}{2} d\theta^* \quad (6)
 \end{aligned}$$

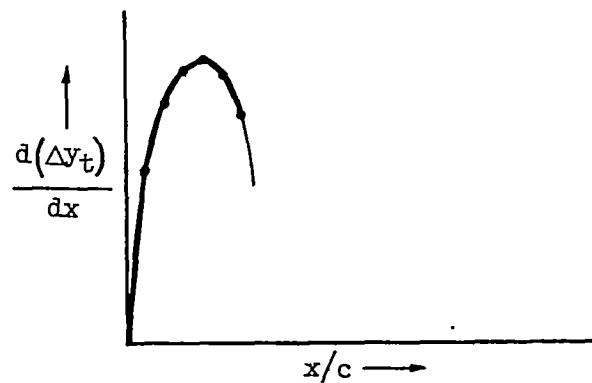
which leads to (see reference 2, e.g.)

$$\frac{\Delta v}{v_o}(\theta_0) = \sum_n A_{no} \left[\frac{d(\Delta y_t)}{dx} \right]_n \quad (7)$$

The coefficients A_{no} depend upon the particular method of numerical integration which is employed. If, for example, $\frac{d(\Delta y_t)}{dx}$ is replaced by a step-curve, that is, assumed constant in every interval (see fig. below), one set of values of A_{no} would be obtained.



Greater accuracy would be obtained by the assumption that $\frac{d(\Delta y_t)}{dx}$ is replaced by straight-line segments (see fig. below), in which case a second set of values of A_{no} would be obtained.



A further refinement would be that of assuming $\frac{d(\Delta y_t)}{dx}$ to be composed of segments of parabolas, and so forth. Since the accuracy of the resulting values of $\frac{\Delta v}{V_0}$ depends upon both the character of the approximate curve and the size of interval taken, it is apparent that the same degree of accuracy might be achieved from many different combinations of interval sizes and approximations to the function $\frac{d(\Delta y_t)}{dx}$.

Naiman (reference 2) has used Simpson's rule for computing the Poisson integral, which corresponds to the replacement of the product $\left[\frac{d(\Delta y_t)}{dx} \cot \frac{\theta^*}{2} \right]$ by segments of parabolas. The "critical interval" (i.e., where $\cot \frac{\theta^*}{2} \rightarrow \infty$) was carefully treated by using differences of higher order (including the fifth derivative of $\frac{d(\Delta y_t)}{dx}$). Naiman divided the period of 2π in 20 or 40 intervals and calculated the corresponding sets of values of A_{no} . Other workers at the NACA have extended the calculation of these values of A_{no} to 80 and 160 intervals (unpublished information).¹

Obviously, the time required for computing $\frac{\Delta v}{V_0}$ increases with the number of intervals taken because of the increased number of multiplications to be performed. In addition, greater preparations for the computing process are necessarily involved, particularly since the values of $\frac{d(\Delta y_t)}{dx}$ needed must usually be obtained by interpolation.

This interpolation has to be done rather carefully as it is often not sufficient simply to take the values of the plotted curve of $\frac{d(\Delta y_t)}{dx}$. This curve should be checked by difference tables if the values $\left[\frac{d(\Delta y_t)}{dx} \right]_n$ are to represent a smooth curve.

For those functions of Δy_t which may be well-represented by a Fourier series, there exists a simple method of evaluating the Poisson integral which has apparently been overlooked until the present time. This method has the advantage of leading to a computation which does not involve the derivative of Δy_t .

¹Naiman has also suggested a second method for computing the Poisson integral (see reference 3). In this second method he uses Fourier polynomials to represent the function $\frac{d(\Delta y_t)}{dx}$. The computing procedure is very simple; however, the results depend largely on the degree of approximation of $\frac{d(\Delta y_t)}{dx}$ by such a polynomial. Thus, for large families of functions results are good; however, cases are known to the author where results were not satisfactory because regions with steep gradients may not be represented well enough by a Fourier polynomial of moderate order.

Equation (6) may be written in a different form (reference 1, equation (43)) as follows:

$$\frac{\Delta v}{V_0} = \frac{1}{\pi} \int_0^\pi \frac{d(\Delta y_t)}{dx} \frac{\sin \theta}{\cos \theta - \cos \theta_0} d\theta \quad (8)$$

and this may be rewritten as

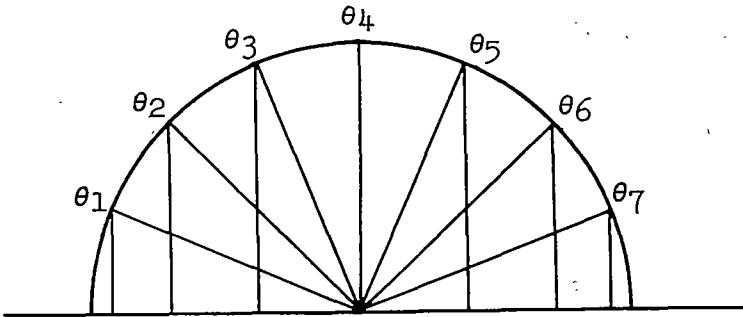
$$\frac{\Delta v}{V_0} = \frac{1}{\pi c} \int_0^\pi \frac{d(\Delta y_t)}{d\theta} \frac{d\theta}{\cos \theta - \cos \theta_0} \quad (9)$$

Equation (9) is strikingly similar to an integral occurring in the theory of the lift distribution of a finite wing in incompressible flow. There, the induced angle α_1 is given by

$$\alpha_1 = \frac{1}{2\pi} \int_0^\pi \frac{dy}{d\theta^*} \frac{d\theta^*}{\cos \theta^* - \cos \theta} \quad (10)$$

where γ is the local dimensionless circulation.

Multhopp (reference 4) has given a solution for equation (10). He divides the range of integration into $(m_1 + 1)$ intervals (see fig. below)



with

$$\left. \begin{aligned} \theta_n &= \frac{n}{m_1 + 1} \pi \\ \gamma_n &= \gamma(\theta_n) \end{aligned} \right\} \quad (11)$$

and computes α_1 at the points θ_n . He assumes that γ may be expanded in the form

$$\gamma = \sum C_\mu \sin \mu\theta$$

or

$$\gamma = \frac{2}{m+1} \sum_{n=1}^{m_1} \gamma_n \sum_{\mu=1}^{m_1} \sin \mu\theta_n \sin \mu\theta \quad (12)$$

He then obtains the expression

$$\alpha_{iv} = b_{vv}\gamma_v - \sum_1^{m_1} b_{vn}\gamma_n \quad (13)$$

The prime on the summation symbol indicates that $n = v$ is to be omitted from the summation because that special term has already been considered in the first term of the right-hand side (i.e., $b_{vv}\gamma_v$). Reference 4 presents tables for the coefficients b_{vv} and b_{vn} for $m_1 = 7, 15$, and 31 . Applied to the problem at hand, $m_1 = 31$ would appear to be rather small; therefore a table for $m_1 = 63$ has been computed and is included in the present report (appendix A). As a comparison: For $m_1 = 63$, $\Delta\theta = 2.8125^\circ$; for Naiman's method with 160 points, $\Delta\theta = 2.25^\circ$.

Utilizing this method of integration which was developed by means of Fourier series, an expression may be obtained for the velocity distribution as follows:

$$\frac{\Delta v}{v_o}(\theta_o) = \frac{4}{c} \left(b_{vv} \Delta y_v - \sum_1^{m_1} b_{vn} \Delta y_n \right) \quad (14)$$

The great advantage of this method is that of simplicity: (1) The actual computational procedure is very simple and (2) the derivative $\frac{d(\Delta y_t)}{dx}$ is avoided. The simplicity of computation is reflected in the fact that the time required for computing $\frac{\Delta v}{v_o}$ at one value of θ_o is approximately half that required by the method of Naiman when the intervals have approximately the same size. It should be noted,

however, that the accuracy of the method of Naiman will be greater than that of Multhopp in those cases where the differentiation of Δy_t by Fourier expansion (equation (12)) does not give good results.

A third method of evaluating the Poisson integral became known during the course of the present investigation. In a paper by Timman (reference 5), the integral is studied in the form

$$\tau(\phi) = -\frac{1}{2\pi} \int_0^{2\pi} \bar{\sigma}(\psi) \cot \frac{\phi - \psi}{2} d\psi \quad (15)$$

Timman assumes that $\bar{\sigma}(\psi)$ is not given analytically, but only at equidistant points. An interpolation polynomial (reference 6) for $\bar{\sigma}(\psi)$ is employed, and these polynomials replace the function $\bar{\sigma}(\psi)$ in a single interval by a function of third order. The polynomial function thus introduced has a continuous first derivative,² and it is evident that this continuity is essential for the attainment of good results.

Timman has divided the period 2π into 36 intervals of equal length and established a computing scheme. The function $\bar{\sigma}(\psi)$ is separated into its symmetrical and unsymmetrical parts so that

$$\bar{\sigma}(\psi) = s + d \quad (16)$$

Then

$$\tau(\psi_l) = \sum_{k=0}^{18} \alpha_{kl} s_k - \sum_{k=0}^{18} \beta_{kl} d_k \quad (17)$$

where the factors α_{kl} and β_{kl} are given in tabular form. In the present particular case $\frac{d(\Delta y_t)}{dx}$ is antisymmetrical (equation (3)) and $\frac{\Delta v}{V_o}$ is symmetrical (equation (4)). Thus the separation indicated by equation (16) does not require any additional work.

Timman's method should give good results provided that a sufficient number of intervals are taken - the division of 36 intervals over a period of 2π (i.e., 18 intervals over the chord of the profile) appears to be insufficient for an accurate representation of the function which occurs, $\frac{d(\Delta y_t)}{dx}$ or $\frac{\Delta v}{V_o}$.

²The polynomials used in the classical interpolation formulas are less smooth (see reference 5, pp. 7 and 10, figs. 1 and 2).

The time required for computing one point by the method of Timman is approximately the same as for Naiman's method with the same interval size.

Other methods of evaluating the Poisson integral have been suggested. They will not be discussed here as it is the intention of this section to consider only the most practical of the known methods. The three methods already discussed have their own particular advantages and have been especially developed for rapid and simple computation; however, all three of these methods, when $\frac{d(\Delta y_t)}{dx}$ or $\frac{\Delta v}{v_0}$,

change rapidly in magnitude, become cumbersome, and require that very small intervals be taken over the entire range of integration because the scheme of equal interval size is utilized.

EVALUATION OF POISSON INTEGRAL BY A METHOD

EMPLOYING UNEQUAL INTERVALS

Development of Method

As the change in airfoil shape, or the change in velocity distribution, is given originally as a function of x it appears logical to retain the coordinate x in selecting the size of the different intervals. Hence, the Poisson integral may be studied in the form

$$\tau(x_0) = -\frac{1}{\pi} \int_0^c \sigma(x) \frac{dx}{x - x_0} \quad (18)$$

which corresponds to equation (1). Conforming with its physical meaning $\sigma(x) = \frac{d(\Delta y_t)}{dx}$ is assumed to be a function which is finite in every point of its range of definition.³

Define

$$\Delta x_n = x_{n+1} - x_n \quad (19a)$$

with

$$n = 0, 1, 2, 3, \dots$$

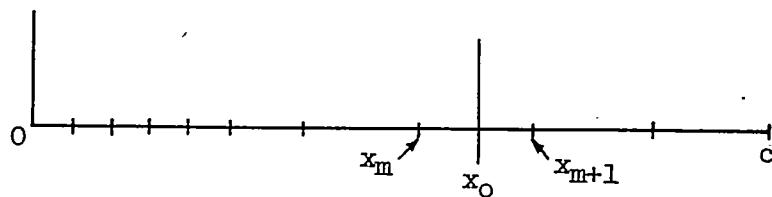
³This restriction will be dropped later; see discussion beginning with the first paragraph after equation (32).

and

$$x_m < x_0 < x_{m+1} \quad (19b)$$

For convenience, there is chosen (see following fig.)

$$x_0 = \frac{x_m + x_{m+1}}{2} \quad (19c)$$



The function $\sigma(x)$ is approximated by straight-line segments (see third sketch in preceding section). Then, for $x_n < x < x_{n+1}$,

$$\begin{aligned} \sigma(x) &= \sigma(x_n) + \frac{\sigma(x_{n+1}) - \sigma(x_n)}{\Delta x_n}(x - x_n) \\ &= \sigma_n + \frac{\sigma_{n+1} - \sigma_n}{\Delta x_n}(x - x_n) \end{aligned} \quad (20)$$

from which there is obtained

$$\begin{aligned}
 \tau(x_0) &= -\frac{1}{\pi} \int_0^c \sigma(x) \frac{dx}{x - x_0} = -\frac{1}{\pi} \sum \int_{x_n}^{x_{n+1}} \frac{\sigma_n + \frac{\sigma_{n+1} - \sigma_n}{\Delta x_n} (x - x_n)}{x - x_0} dx \\
 &= -\frac{1}{\pi} \left[\sum \int_{x_n}^{x_{n+1}} \frac{\sigma_n + \frac{\sigma_{n+1} - \sigma_n}{\Delta x_n} (x - x_0 + x_0 - x_n)}{x - x_0} dx \right] \\
 &= -\frac{1}{\pi} \left\{ \sum \left(\frac{\sigma_{n+1} - \sigma_n}{\Delta x_n} \right) \Delta x_n + \right. \\
 &\quad \left. \sum \left[\sigma_n + \frac{\sigma_{n+1} - \sigma_n}{\Delta x_n} (x_0 - x_n) \right] \left(\int_{x_n}^{x_{n+1}} \frac{dx}{x - x_0} \right) \right\} \tag{21}
 \end{aligned}$$

Also,

$$\int_{x_n}^{x_{n+1}} \frac{dx}{x - x_0} = j_{no} \tag{22}$$

by definition. The function j_{no} , in the different regions of x , is given by different expressions as follows:

$$j_{no} = \left\{ \begin{array}{ll} \log_e \frac{x_{n+1} - x_0}{x_n - x_0} & \text{for } x_{n+1} > x_n > x_0 \\ \log_e \frac{x_{n+1} - x_0}{x_0 - x_n} & \text{for } x_{n+1} > x_0 > x_n \\ \log_e \frac{x_0 - x_{n+1}}{x_0 - x_n} & \text{for } x_0 > x_{n+1} > x_n \end{array} \right\} \tag{23}$$

Introducing j_{no} into equation (21), there results

$$\begin{aligned}\tau(x_o) &= -\frac{1}{\pi} \left\{ \sum (\sigma_{n+1} - \sigma_n) + \sum \left[\sigma_n + \frac{\sigma_{n+1} - \sigma_n}{\Delta x_n} (x_o - x_n) \right] j_{no} \right\} \\ &= -\frac{1}{\pi} \left[\sum \sigma_n j_{no} + \sum (\sigma_{n+1} - \sigma_n) \left(1 + \frac{x_o - x_n}{\Delta x_n} j_{no} \right) \right] \quad (24)\end{aligned}$$

Or, defining

$$1 + \frac{x_o - x_n}{\Delta x_n} j_{no} = j_{no}^* \quad (25)$$

there results, finally,

$$\tau(x_o) = -\frac{1}{\pi} \left[\sum \sigma_n j_{no} + \sum (\sigma_{n+1} - \sigma_n) j_{no}^* \right] \quad (26)$$

Since $x_{n+1} = x_n + \Delta x_n$, the functions j_{no} and j_{no}^* may be written as

$$\left. \begin{aligned}j_{no}^* &= 1 + \frac{x_o - x_n}{\Delta x_n} j_{no} \\ j_{no} &= \log_e \left(1 + \frac{\Delta x_n}{x_n - x_o} \right) \text{ for } x_n > x_o \\ &= \log_e \left(-1 + \frac{\Delta x_n}{x_o - x_n} \right) \text{ for } x_n + \Delta x_n > x_o > x_n \\ &= \log_e \left(1 + \frac{\Delta x_n}{x_n - x_o} \right) \text{ for } x_o > x_n + \Delta x_n\end{aligned} \right\} \quad (27a)$$

and this form shows that j_{no} and j_{no}^* are functions of $\frac{x_n - x_o}{\Delta x_n}$ only.

$$\left. \begin{array}{l} \text{For } \frac{x_n - x_0}{\Delta x_n} \rightarrow \pm\infty \quad j_{no} \rightarrow 0 \quad j_{no}^* \rightarrow 0 \\ \text{For } x_0 - x_n = \frac{1}{2} \Delta x_n \quad j_{no} = 0 \quad j_{no}^* = 1 \end{array} \right\} \quad (27b)$$

$$\left. \begin{array}{l} \text{For very large } \frac{x_n - x_0}{\Delta x_n} = \xi, \\ j_{no} \rightarrow \frac{1}{\xi} - \frac{1}{2\xi^2} + \dots \\ j_{no}^* \rightarrow \frac{1}{2\xi} - \frac{1}{3\xi^2} + \dots \end{array} \right\} \quad (27c)$$

$$\left. \begin{array}{l} \text{For very large negative } \frac{x_n - x_0}{\Delta x_n} \text{ with } \left| \frac{x_n - x_0}{\Delta x_n} \right| = \xi^*, \\ j_{no} \rightarrow -\frac{1}{\xi^*} - \frac{1}{2\xi^{*2}} + \dots \\ j_{no}^* \rightarrow -\frac{1}{2\xi^*} - \frac{1}{3\xi^{*2}} + \dots \end{array} \right\} \quad (27d)$$

These functions are given in figure 1 and in table I.

It is seen that high absolute values of j_{no} and j_{no}^* occur near those values of $\frac{x_n - x_0}{\Delta x_n}$ which characterize the critical interval.⁴

Figure 1 gives an idea of the characteristic qualities of j_{no} and j_{no}^* as functions of $\frac{x_n - x_0}{\Delta x_n}$; however, the representation is not sufficient for picking out values for a computation. Table I gives the values of j_{no} and j_{no}^* for $-49.5 < \frac{x_n - x_0}{\Delta x_n} < 49.5$. This table might

⁴If $x_0 = \frac{x_m + x_{m+1}}{2}$ (equation (19c)) the critical interval is given by $-0.5 < \frac{x_n - x_0}{\Delta x_n} < 0.5$.

be used for rough computation and for getting acquainted with the method. In general, it is advisable to use those tables which are given in appendix B.

It will prove of benefit to investigate the exactness of that portion of the integral which contains the singularity. Recalling that the function $\sigma(x)$ was replaced by a straight line in every interval (equation (20)), there is obtained:

$$-\frac{1}{\pi} \int_{x_0 - \frac{\Delta x}{2}}^{x_0 + \frac{\Delta x}{2}} \frac{\sigma(x)}{x - x_0} dx = -\frac{1}{\pi} (\sigma_{m+1} - \sigma_m) \quad (28)$$

if $x_m < x_0 < x_{m+1}$. Now, let an expansion of the function $\sigma(x)$ in the critical interval around x_0 be assumed as follows:

$$\begin{aligned} \sigma(x) &= \sigma(x_0) + \sigma'(x_0)(x - x_0) + \frac{\sigma''(x_0)}{2!}(x - x_0)^2 + \\ &\quad \frac{\sigma'''(x_0)}{3!}(x - x_0)^3 + \frac{\sigma^{iv}(x_0)}{4!}(x - x_0)^4 + \dots \end{aligned} \quad (29)$$

Then,

$$\begin{aligned} -\frac{1}{\pi} \int_{x_0 - \frac{\Delta x}{2}}^{x_0 + \frac{\Delta x}{2}} \frac{\sigma(x)}{x - x_0} dx &= -\frac{1}{\pi} \left[\sigma'(x_0) \Delta x + \frac{\sigma'''(x_0)}{3!} \frac{2(\Delta x)^3}{3(2)} + \dots \right] \\ &= -\frac{1}{\pi} \left[\frac{13}{12}(\sigma_{m+1} - \sigma_m) - \frac{1}{36}(\sigma_{m+2} - \sigma_{m-1}) \right] \\ &= -\frac{1}{\pi} \left\{ \frac{19}{18}(\sigma_{m+1} - \sigma_m) - \right. \\ &\quad \left. \frac{1}{36} \left[(\sigma_{m+2} - \sigma_{m+1}) + (\sigma_m - \sigma_{m-1}) \right] \right\} \quad (30) \end{aligned}$$

Comparison of formulas (30) and (28) shows that the error in the critical interval is approximately given by

$$- \frac{1}{\pi} \left\{ \frac{1}{18} (\sigma_{m+1} - \sigma_m) - \frac{1}{36} \left[(\sigma_{m+2} - \sigma_{m+1}) + (\sigma_m - \sigma_{m-1}) \right] \right\} \quad (31)$$

The error of evaluating the whole integral by finite differences may be estimated by using two different interval distributions and comparing the results for a given x_0 .

However, in addition to that error of the result produced by replacing the Poisson integral by a sum there exists another error. This sum cannot be computed exactly, but has a certain error depending on the accuracy of the given data for $\sigma_n(x)$ and the tabulated values

of j_{no} and j_{no}^* . As the function $\sigma(x) = \frac{d(\Delta y_t)}{dx}$ usually has an error of $\epsilon_1 = 1 \times 10^{-3}$ it has proved amply satisfactory to give j_{no} and j_{no}^* to four decimal places, the error being less than $\epsilon_2 = 5 \times 10^{-5}$. The error of

$$\tau(x_0) = - \frac{1}{\pi} \left[\sum \sigma_n j_{no} + \sum (\sigma_{n+1} - \sigma_n) j_{no}^* \right]$$

is smaller than its upper limit given by

$$\frac{1}{\pi} \left[\epsilon_1 \left(\sum |j_{no}| + 2 \sum |j_{no}^*| \right) + \epsilon_2 \left(\sum |\sigma_n| + \sum |\sigma_{n+1} - \sigma_n| \right) \right] \quad (32)$$

This formula shows that the influence of ϵ_1 is stronger than the influence of ϵ_2 as long as $\sum |\sigma_n| + \sum |\sigma_{n+1} - \sigma_n|$ is smaller than 1 - as it is in our later examples - and the sums $\sum |j_{no}|$ and $\sum |j_{no}^*|$ are always larger than 1. An increase of subdivisions makes the sums in the upper limit of the error (32) grow, thus requiring a higher accuracy, especially in σ_n and perhaps also in the values of j_{no} and j_{no}^* .

In establishing the solution of equation (18) it was assumed that $\sigma(x)$ is finite throughout its range of definition. If it is desired to compute the change in shape due to a proposed change of velocity distribution, this restriction must be eliminated, as will be recognized immediately.

Equation (5) may be written in the form

$$\frac{d(\Delta y_t)}{dx} = \frac{1}{\pi} \sqrt{x_0(c - x_0)} \int_0^c \frac{\Delta v/v_o}{\sqrt{x(c - x)}} \frac{dx}{x - x_0} \quad (5*)$$

Omitting the factor $\sqrt{x_0(c - x_0)}$, which does not affect the integration process, the integral may be reduced to the form of equation (18) by defining

$$\frac{\Delta v/v_o}{\sqrt{x(c - x)}} = \sigma_1(x) \quad (33)$$

However, $\sigma_1(x)$ will be infinite at $x = 0$ and $x = c$ if $(\frac{\Delta v}{v_o})_o \neq 0$ and $(\frac{\Delta v}{v_o})_c \neq 0$; therefore, a special consideration of the neighborhood of $x = 0$ and $x = c$ is required. This is done by splitting the integral into the following three parts:

$$\begin{aligned} \int_0^c \sigma_1(x) \frac{dx}{x - x_0} &= \int_0^{\epsilon_1} \sigma_1(x) \frac{dx}{x - x_0} + \int_{\epsilon_1}^{c - \epsilon_2} \sigma_1(x) \frac{dx}{x - x_0} + \\ &\quad \int_{c - \epsilon_2}^c \sigma_1(x) \frac{dx}{x - x_0} \end{aligned} \quad (34)$$

with ϵ_1 and ϵ_2 being small compared with c . The integral

$$\int_{\epsilon_1}^{c - \epsilon_2} \sigma_1(x) \frac{dx}{x - x_0}$$

may be treated as was explained formerly for

$$\int_0^c \sigma(x) \frac{dx}{x - x_0}$$

(see equation (18)) because $\sigma_1(x)$ is finite for $\epsilon_1 < x < c - \epsilon_2$. For the first and third integrals, however, a new integration formula must be developed. By introducing

$$\mu = c - x \quad \text{and} \quad \sigma_1(x) = \sigma_1[\mu(x)] = \sigma_1^*(\mu)$$

there is obtained

$$\int_{c-\epsilon_2}^c \sigma_1(x) \frac{dx}{x - x_0} = - \int_0^{\epsilon_2} \sigma_1^*(\mu) \frac{d\mu}{\mu - \mu_0} \quad (35)$$

Hence, the method used for the first integral will also apply to the third. In most cases $\left(\frac{\Delta v}{V_0}\right)_c$ will be zero and there will be no need for a special evaluation in the neighborhood of $x = c$.

The integral

$$\int_0^{\epsilon_1} \sigma_1(x) \frac{dx}{x - x_0} = \int_0^{\epsilon_1} \frac{\Delta v/V_0}{\sqrt{x(c - x)}} \frac{dx}{x - x_0} \quad (36)$$

will have an important influence on the result of equation (34) only if x_0 is near to ϵ_1 . First the general formula will be given and then a simplification will be discussed for $x_0 \gg \epsilon_1$.

The integral (36) will be solved assuming that

$$\frac{\Delta v}{V_0} = a_0 + a_1 \left(\frac{x}{c} \right) + a_2 \left(\frac{x}{c} \right)^2 \quad \text{for } 0 < x < \epsilon_1 \quad (37)$$

Only the final formula of this procedure is given here; the details of the solution will be found in appendix C.

$$F_1(x_o) = \int_0^{\epsilon_1} \frac{\Delta v/V_o}{\sqrt{x(c-x)}} \frac{dx}{x-x_o} = \frac{1}{c} \left[M_o - \frac{1}{\sqrt{\frac{x_o}{c}}} \left[a_o + a_1^* \left(\frac{x_o}{c} \right) + a_2^* \left(\frac{x_o}{c} \right)^2 \right] + 2 \sqrt{\frac{\epsilon_1}{c}} \left[a_1^* + a_2^* \left(\frac{x_o}{c} \right) \right] + \frac{2}{3} a_2^* \sqrt{\frac{\epsilon_1}{c}}^3 \right] \quad (38)$$

with M_o given in figure 2, and

$$a_o = \left(\frac{\Delta v}{V_o} \right)_o$$

$$a_1^* = a_1 + \frac{1}{2} a_o$$

with

$$a_1 = \frac{c}{2\epsilon_1} \left[-3 \left(\frac{\Delta v}{V_o} \right)_o + 4 \left(\frac{\Delta v}{V_o} \right)_{\epsilon_1} - \left(\frac{\Delta v}{V_o} \right)_{2\epsilon_1} \right] \quad (39)$$

$$a_2^* = a_2 + \frac{1}{2} a_1 + \frac{3}{8} a_o$$

with

$$a_2 = \frac{c^2}{2\epsilon_1^2} \left[\left(\frac{\Delta v}{V_o} \right)_o - 2 \left(\frac{\Delta v}{V_o} \right)_{\epsilon_1} + \left(\frac{\Delta v}{V_o} \right)_{2\epsilon_1} \right]$$

The coefficients a_o , a_1 , and a_2 may be determined first, as they do not depend upon the particular value of x_o , and then $F_1(x_o)$ may be computed. The term depending on a_1 and a_2 will exert an influence only for small values of x_o/c . After a brief training the computer should be able to decide rather accurately when the formula

$$F_1(x_o) = \frac{1}{c} M_o \frac{a_o}{\sqrt{\frac{x_o}{c}}} \rightarrow \frac{a_o}{x_o} \left(-2 \sqrt{\frac{\epsilon_1}{c}} \right) \quad (40)$$

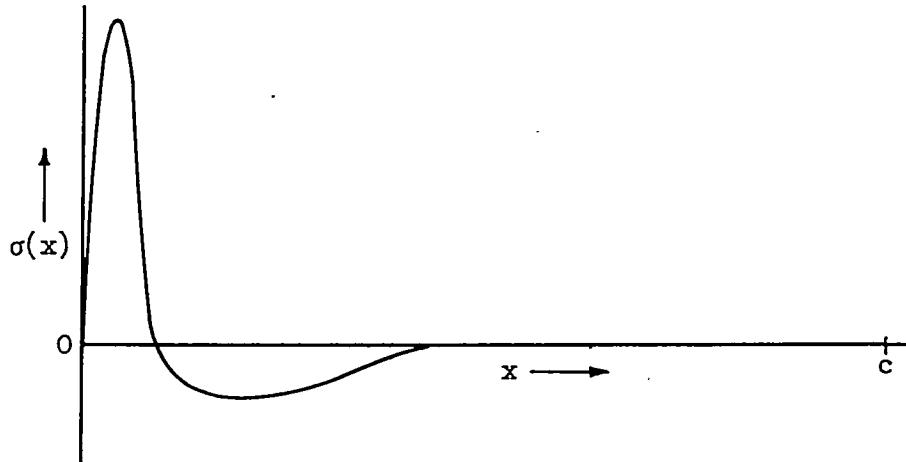
is sufficient and when the more exact expression (equation (38)) is required (also see fig. 2).

Organization of Computational Procedure for Unequal Intervals;

Transition from One Size of Interval to Another

A thorough understanding of the method is best achieved by following through a rather simple example; in addition various short cuts to the method will be demonstrated.

Assume a function $\sigma(x)$ of the type shown in the following figure.



It appears reasonable to take rather small intervals for small values of x because of the form of the curve $\sigma(x)$; therefore, the following arrangement of interval sizes is arbitrarily selected:

$$\bar{\Delta}x = 0.002 \text{ for } 0 < x < 0.030$$

$$\overline{\Delta}x = 0.006 \text{ for } 0.030 < x < 0.096$$

Compute $\tau(0.009)$ with the help of equation (26). Note that the critical interval extends from 0.008 to 0.010. Table II(a) gives the values of x/c , σ_n , $\sigma_{n+1} - \sigma_n$, j_{no} , and j_{no}^* for the range with $\bar{\Delta}x = 0.002$. At $x = 0.030$ the interval changes to $\overline{\Delta}x = 0.006$ and the same functions are given for the range with this size of interval in table II(b). Naturally the range above the broken line in table II(b) is not utilized in the computation since this portion has been considered in table II(a).

Note that $\frac{x_n - x_0}{\Delta x}$ progresses in table II(b) in the same manner as in table II(a); this is due to the special choice of $\overline{\Delta x}$. If $\overline{\Delta x} = 0.006$ were used starting with $x = 0$ the critical interval for $x_0 = 0.009$ would extend from 0.006 to 0.012. Hence, for $\overline{\Delta x} = 0.006$, $j_{no} = 0$ and $j_{no}^* = 1$ is to be found at $x/c = 0.006$.

For rapid computation it is best to have j_{no} and j_{no}^* as functions of $\frac{x_n - x_0}{\Delta x}$ on a paper strip and to place this strip adjacent to the columns headed by σ_n and $\sigma_{n+1} - \sigma_n$. If $\frac{x_n - x_0}{\Delta x}$ progresses as indicated in table I, the correct location of $j_{no} = 0$ and $j_{no}^* = 1$ at the beginning of the critical interval fixes the placement of the strip.

In the example just treated, the transition from one size of interval to another is very easy because x_0 lies at the midpoint of an interval of the size 0.006 as well as of the size 0.002, if starting with $x = 0$.

If $\overline{\Delta x}$ had been chosen 0.004, such a desirable arrangement would not have resulted because $x_0 = 0.009$ would not be located at the midpoint of an interval of this size (starting with such intervals at $x = 0$).

As a second example compute the value of τ at $x_0 = 0.015$.

Again, $\frac{x_n - x_0}{\Delta x}$ and $\frac{x_n - x_0}{\overline{\Delta x}}$ will progress as in table I. The values $j_{no} = 0$ and $j_{no}^* = 1$ will be placed opposite $x/c = 0.014$ for the region with $\Delta x = 0.002$ and opposite $x/c = 0.012$ for the region with $\overline{\Delta x} = 0.006$. As long as $\overline{\Delta x} = 3\Delta x$, $\Delta x = 3\overline{\Delta x}$, and so forth and if x_0 is chosen so as to be at the midpoint of the largest size of interval, the computation may be accomplished by shifting the strip with j_{no} and j_{no}^* corresponding to table I.

But suppose that the interval sizes are so arranged and it is desired to compute a point where x_0 does not lie at the midpoint of the largest size of interval; for example, $x_0 = 0.013$. The value $x_0 = 0.013$ lies at the midpoint of an interval with $\overline{\Delta x} = 0.002$; hence,

for the range $0 < x < 0.030$, j_{no} and j_{no}^* may be taken directly from table I. However, at $x/c = 0.030$, intervals of the size $\overline{\Delta x} = 0.006$ commence and there is obtained

$$\frac{x_n - x_0}{\overline{\Delta x}} = \frac{0.030 - 0.013}{0.006} = 2.833$$

The value of $\frac{x_n - x_0}{\Delta x}$ progresses by 1, that is, 2.833; 3.833, 4.833, Thus the functions j_{no} and j_{no}^* are needed for values of $\frac{x_n - x_0}{\Delta x}$ which are not given in table I. One might think of taking them out of an enlarged diagram (see fig. 1); however, it is much more convenient to take them out of an extended table, which is conveniently arranged for "advancing by 1." Such tables are given in appendix B.

The example presented by the figure at the beginning of this section suggested starting at $x = 0$ with the smallest intervals. However, other examples may suggest another distribution of intervals. The smallest size of intervals may lie at any part of $0 < x < c$. There are no restrictions in the arrangement of intervals. (See, e.g., discussion following equation (43).)

Accuracy of Method, Examined by Means of an Analytical Example

The accuracy of the result depends directly upon the size of the interval taken and the reliability of the data comprising the function $\sigma(x)$. Because the function $\sigma(x)$ will be replaced by a broken line, a glance at the curve will quickly suggest an arrangement of intervals. In addition, the error in the critical interval may be used as a first test of the choice of intervals.

As a test of the quality of this new method, involving unequal intervals, a function $\sigma(x) = \frac{d(\Delta y_t)}{dx}$ has been treated which allows the analytical computation of $\tau(x) = \frac{\Delta v}{V_0}$.

The function $\sigma(x)$ is given analytically as

$$0 \leq x \leq 2\Delta \quad \frac{d(\Delta y_t)}{dx} = Bx(2\Delta - x)$$

$$2\Delta \leq x \leq c_1 \quad \frac{d(\Delta y_t)}{dx} = -D(c_1 - x)(x - 2\Delta)$$

$$c_1 \leq x \leq c \quad \frac{d(\Delta y_t)}{dx} = 0$$

The following arbitrary values have been selected:

$$c_1 = 0.35$$

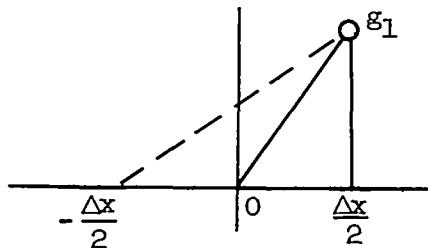
$$c = 1.0$$

$$D = \text{Some multiple of } B \text{ so that } \int_0^{c_1} \frac{d(\Delta y_t)}{dx} dx = 0$$

The functions Δy_t and $\frac{d(\Delta y_t)}{dx}$ are given in figures 3(a) and 3(b), respectively.

The analytical computation of $\frac{\Delta v}{V_0}$ for figure 3(b) is given in figures 4(a) and 4(b). The arrangement of the unequal division for the numerical computation of $\frac{\Delta v}{V_0}$ is indicated in figure 4(a).⁵

⁵ It was desirable to obtain the value of $\frac{\Delta v}{V_0}$ at $x_0 = 0$; hence, the first interval has been placed so that $-0.001 < x_0 < 0.001$ and the function $\frac{d(\Delta y_t)}{dx} = 0$ for $-0.001 < x < 0$. Since the function $\frac{d(\Delta y_t)}{dx} = g$ is replaced in every interval by a straight line, the error might be expected to be large. However, $g = 0$ at $x_0 = 0$ will aid in preventing the error from being too large.



A more exact solution would be obtained by putting

$$g = 0 \quad -\frac{\Delta x}{2} < x < 0$$

$$g = \frac{g_1}{\frac{\Delta x}{2}} x \quad 0 < x < \frac{\Delta x}{2}$$

$$-\frac{1}{\pi} \int_0^{\Delta x/2} \left(\frac{g_1}{\frac{\Delta x}{2}} x \right) \frac{dx}{x - x_0} = -\frac{1}{\pi} g_1 \times 1$$

For the interval $-\frac{\Delta x}{2} < x < \frac{\Delta x}{2}$ equation (26) would yield

$$-\frac{1}{\pi} \int_{-\Delta x/2}^{\Delta x/2} g \frac{dx}{x - x_0} = -\frac{1}{\pi} \left[(g_1 - 0) j_{no}^* + 0 \times j_{no} \right] = -\frac{1}{\pi} g_1$$

and no error is introduced. For $x_0 \neq 0$ there is a very small error which may be avoided by respecting the change of size of the interval near $x = 0$.

Also given in figure 4(a) are points of the $\frac{\Delta v}{V_0}$ curve determined by the method of unequal intervals. Figure 4(b) presents the same information plotted to a larger scale.

For comparative purposes the same problem has been treated by the three methods of computation discussed earlier, namely, those of Naiman, Multhopp, and Timman. Figures 5(a) and 5(b) show the results obtained by the method of Naiman; obviously, the 40-point solution does not use a sufficiently accurate representation of the $\frac{d(\Delta y_t)}{dx}$ curve, while the 80- and 160-point solutions are quite good, with the exception of the maximum and minimum points of the $\frac{\Delta v}{V_0}$ curve. In order to obtain a value at approximately $\frac{x}{c} = 0.036$ a solution involving 320 points would be required. In this respect the method of unequal intervals is more adaptable to special conditions without involving much new work than is the method of Naiman.

The results obtained by Multhopp's method are given in figures 6(a) and 6(b). The 31-point solution (in Multhopp's somewhat odd manner of designation) corresponds to $\Delta\theta = 5.625^\circ$; the 63-point solution, to $\Delta\theta = 2.8125^\circ$. The computation is very simple and the results of the method with 63 points are comparable with that of Naiman with 80 points, with the exception of those near the region $0 < x < 0.01$ (this is shown most clearly in fig. 6(b)). The very steep peak of $\frac{d(\Delta y_t)}{dx}$ at $x/c = 0.02$ requires rather high harmonics for the representation of Δy_t ; consequently, good accuracy in the region near the origin may not be expected. This is substantiated by the fact that for the 63-point method the highest effective harmonic would have three waves in the region $0 < x < 0.04$; obviously a sufficient degree of accuracy in the differentiation process cannot be obtained.

As mentioned earlier, Timman's method might be expected to give good results if the size of interval is properly chosen. Inasmuch as only a table for $\Delta\theta = \frac{360}{36} = 10^\circ$ was available, the result of the computation for $\frac{\Delta v}{V_0}$ cannot be expected to be good, as is evidenced by observing figure 7. The result obtained is comparable with that of Multhopp's 15-point and Naiman's 40-point solutions.

An excellent method of examining the accuracy of these methods still further is simply that of solving the inverse problem. From the curves of $\frac{\Delta v}{V_0}$ just discussed, values for $\frac{d(\Delta y_t)}{dx}$ have been computed

and are presented in figure 8. The method of unequal intervals gives good results, indicating that the arrangement of intervals chosen was as good for the inverse problem as for the direct problem. It is apparent that Naiman's method requires even smaller divisions than 160 points in order to avoid inaccuracies near the point $x/c = 0.04$.

The reader may wonder that the inverse problem is not given by Multhopp's method. It must be recalled that Multhopp's method of solving the direct problem does not involve the differentiation of Δy_t ; that is, it is particularly fit for this problem and presents, on the other hand, no analogy for the inverse problem:

$$\frac{d(\Delta y_t)}{dx} = \frac{1}{2\pi} \int_0^{2\pi} \frac{\Delta v}{V_o} \cot \frac{\theta - \theta_o}{2} d\theta = - \frac{1}{\pi} \int_0^{\pi} \frac{\Delta v}{V_o} \frac{\sin \theta_o}{\cos \theta - \cos \theta_o} d\theta$$

Because more extended tables for Timman's method are not available, and the results obtained from the 36-point method for which tables exist are very poor, no further examples of the application of this method will be given.

COMPARISONS OF METHODS OF NAIMAN AND MULTHOPP WITH METHOD EMPLOYING
UNEQUAL INTERVALS BASED ON ACTUAL EXAMPLES OF CHANGES IN
AIRFOIL SHAPE

The method of unequal intervals has shown good qualities when applied to a problem where the function $\sigma(x)$ is known analytically. However, as mentioned earlier, this function is not usually known in analytic form. This section, therefore, will compare the three principle methods, those of Naiman, Multhopp, and unequal intervals, on the basis of actual design problems, solving the direct problem for $\frac{\Delta v}{V_o}$ and using these results to solve the inverse problem (excluding Multhopp for the inverse problem).

Figure 9(a) shows the Δy_t relations for examples I and II and figure 9(b), the $\frac{d(\Delta y_t)}{dx}$ relations. Note that the slope of $\left[\frac{d(\Delta y_t)}{dx} \right]$ for example II is more than twice that of example I near $x/c = 0$.

The direct problem for example I by Naiman's method is given in figure 10. The 160-point solution does not show any appreciable deviation from the 80-point solutions at the region of $\left(\frac{\Delta v}{V_o}\right)_{\max}$; however, near the origin, at $\left(\frac{\Delta v}{V_o}\right)_{\min}$, the influence of the smaller-sized intervals ($80:\Delta\theta = 4.5^\circ$; $160:\Delta\theta = 2.25^\circ$) is quite pronounced.

The solution by Multhopp's method is given in figure 11;⁶ 31 points around the half circle are not sufficient for a solution comparable with Naiman's 80-point solution, and even a solution based on 63 points does not offer much improvement. The results are poor, as might be expected, in the region very near the origin (see preceding section).

Figure 12 presents the results obtained by the method of unequal intervals, compared with results obtained by Naiman's 80- and 160-point solutions. The method of unequal intervals gives results corresponding to those established by Naiman's 160-point solution. The subdivision used is shown in the figure.

As before, the inverse problem was solved, and is given in figure 13. In each case the computed curve of $\frac{\Delta v}{V_o}$ was the one used in obtaining the values for the $\frac{d(\Delta y_t)}{dx}$ curve. Both methods give good results, thus proving that the chosen number of divisions was sufficient in Naiman's method and in the method employing unequal intervals.

The value of $\frac{d(\Delta y_t)}{dx}$ computed at $x/c = 0.171$ is of some interest.

This point was computed by the method of unequal intervals in two different ways: First, the arrangement of intervals shown in figure 13 was utilized to compute the lower point. Then a new arrangement of intervals ($\Delta x = 0.018$ for $0 < x < 0.36$) was set up and the same point computed. The idea was to determine the inaccuracies that would result. One might predict that, since the point $x/c = 0.171$ lies at a considerable distance from the region of rapid changes in $\frac{\Delta v}{V_o}$, errors of only small magnitude would be introduced; this is fairly well substantiated by the results shown in the figure because the error thus introduced is approximately that of the deviation of Naiman's 160-point solution.

⁶ Recall that this method does not involve the differentiation of Δy_t .

Now, turning our attention to example II, which, it will be recalled, has a slope of $\frac{d(\Delta y_t)}{dx}$ of approximately twice that of example I, the results given in figures 14 to 17 are obtained.

For the direct problem Naiman's method of 160 points and the method employing unequal intervals give results which are in good agreement. For the inverse problem (fig. 17) it is apparent that the method using unequal intervals is superior (see the deviation at $\left[\frac{d(\Delta y_t)}{dx} \right]_{\max}$ given by the method of Naiman). Multhopp's method gives a rather good result (fig. 15), which may be attained when the Fourier representation of the Δy curve is adequate.

The two examples thus far presented are favorable for Naiman's method because the steep slopes of $\sigma(x)$ occur near $x = 0$ where the points Naiman uses are close together. However, going to still steeper slopes near $x = 0$ would require a rapidly increasing number of points. The new method offers another possibility here. Assume that in that critical region $x_k < x < x_{k+1}$ (x_k may be 0) $\sigma(x)$ may be represented by $\sigma(x) = \sum a_n x^n$. Then the integral

$$\int_0^c \frac{\sigma(x)}{x - x_0} dx$$

may be split into three integrals

$$\begin{aligned} \int_0^c \frac{\sigma(x)}{x - x_0} dx &= \int_0^{x_k} \frac{\sigma(x)}{x - x_0} dx + \int_{x_k}^{x_{k+1}} \frac{\sigma(x)}{x - x_0} dx + \\ &\quad \int_{x_{k+1}}^c \frac{\sigma(x)}{x - x_0} dx \end{aligned} \quad (41)$$

The first and third of these integrals may be solved in the usual manner using the functions j_{no} and j_{no}^* . The second integral will be solved analytically.

This simple form, due to the use of the coordinate x in the Poisson integral, allows a rapid integration, because the integral

$$k_{n,o} = \int_{x_k}^{x_{k+1}} \frac{x^n}{x - x_o} dx$$

can be solved by recurrence as follows:

$$k_{n,o} = \frac{x_{k+1}^n - x_k^n}{n} + x_o k_{n-1,o} \quad \text{for } n \geq 1 \quad (42)$$

with

$$k_{0,o} = j_{no} \left(\frac{x_k - x_o}{x_{k+1} - x_k} \right) \quad (43)$$

Thus even very steep slopes cause no difficulties.

As already mentioned, examples I and II correspond well to the qualities demanded by Naiman's method insofar as the rather steep slopes occur in those portions where the points θ_n are close together. If those steep slopes should occur in other portions of the chord, however, a very great number of points in the Naiman method would be needed in order to represent $\sigma(x)$ adequately, and to get reliable results. In such a case the method using unequal intervals shows its advantage by allowing a free subdivision of the chord.

A third example will serve to illustrate this. Figure 18 shows a function $\sigma(x) = \frac{d(\Delta y_t)}{dx}$. The essential values of the function lie in a part of the chord where even Naiman's method with 160 points is not sufficient to represent the function accurately. This is forcibly shown by the two curves of $\frac{\Delta v}{V_o}$. If the function $\sigma(x)$ is modified (dotted line) so as to eliminate the high peak, then the $\frac{\Delta v}{V_o}$ curve by unequal intervals can be made to agree with the original $\frac{\Delta v}{V_o}$ by Naiman's 160-point solution, thus definitely proving that, in this example, Naiman's method with 160 points is insufficient.

Table III indicates the computation for the point $x_o = 0.065$ by unequal intervals.

CONCLUDING DISCUSSION

The new method of evaluating the Poisson integral developed herein is to be recommended for all those functions $\sigma(x)$, where steep slopes in small portions of the region to be integrated exist. In these portions a very small size of interval may be chosen without requiring that this same size of interval be used throughout the region of integration. In this manner, the work required for computation may be maintained at a reasonable level even for the most complicated problems.

The analytical treatment of special parts of the integral is possible (evaluating the remainder by the new method; see preceding section). In those problems where a transition to very small intervals in part of the integration range would require the determination of a great many values of σ_n , this idea might be used to advantage.

It should be noted that the smoothness of the function $\sigma(x)$ and its accurate representation by single points is essential for good results. If, for example, single points σ_n are simply taken from a curve for x_n very close to one another it may be compulsory to check these values by a table of differences.

Stanford University
Stanford, Calif., December 6, 1950

APPENDIX A

VALUES OF $b_{\nu n}$ FOR $\nu_1 = 63$

ν	1	3	5	7	9	11	13	15	17	19	21	23	25	27	29	31	$b_{\nu n}$
n	586.5974	109.0141	68.8699	47.4876	37.4551	31.1890	26.8610	23.8240	21.5948	19.9200	18.6643	17.6989	16.9936	16.4942	16.1762	16.0192	$b_{\nu n}$
3	117.7051	43.5039	24.4288	9.3670	0.1841	0.0810	0.0418	0.0237	0.0146	0.0095	0.0065	0.0048	0.0035	0.0027	0.0021	0.0017	62
4	9.5258	45.5448	26.5068	1.9794	.5176	.3015	.0967	.0539	.0319	.0206	.0140	.0100	.0073	.0056	.0044	.0036	60
5	2.5926	4.5623	26.6869	15.9041	1.8605	.4620	.1920	.0973	.0858	.0547	.0338	.0161	.0118	.0089	.0069	.0055	58
6	1.0858	1.4036	26.8072	19.1646	15.1443	1.3683	.4108	.1788	.0839	.0584	.0356	.0245	.0174	.0159	.0098	.0078	56
10	.5395	.6410	.9450	8.0744	15.1465	12.8165	1.1878	.3703	.1864	.0999	.0644	.0356	.0248	.0181	.0156	.0107	54
12	.3100	.3491	.4528	.7188	1.6503	12.5226	10.8609	1.0699	.3396	.1561	.0862	.0658	.0364	.0281	.0186	.0142	53
14	.1944	.2122	.2853	.3491	.8777	1.3788	10.8639	9.6347	.9643	.3183	.1480	.0851	.0352	.0255	.0189	.0129	50
16	.1300	.1588	.1898	.2011	.9850	.4855	1.1870	9.6917	6.7687	.8996	.2867	.1414	.0808	.0513	.0561	.0255	48
18	.0910	.0960	.1078	.1881	.1865	.2421	.4841	1.0690	6.7421	7.9460	.7702	.2820	.1564	.0768	.0508	.0368	46
20	.0653	.0682	.0748	.0863	.1067	.1408	.2093	.3738	.0538	7.9885	7.4640	.7823	.8886	.1313	.0768	.0601	44
22	.0496	.0514	.0554	.0624	.0736	.0985	.1851	.1895	.5436	.8913	7.5161	7.1773	.7650	.5848	.1508	.0775	42
24	.0380	.0398	.0418	.0468	.0631	.0638	.0816	.1117	.1730	.5182	.8506	7.1818	6.9070	.7392	.4594	.1297	40
26	.0298	.0306	.0324	.0358	.0894	.0404	.0869	.0735	.1029	.1605	.8986	.7948	6.8901	6.8481	.7450	.2666	38
28	.0238	.0243	.0285	.0376	.0906	.0549	.0614	.0514	.0674	.9066	.1605	.2857	.7616	6.6920	6.5771	.7161	36
30	.0190	.0195	.0204	.0218	.0240	.0859	.0313	.0376	.0472	.0628	.0698	.1431	.2782	.7594	6.5535	.6508	34
32	.0156	.0159	.0168	.0177	.0191	.0218	.0848	.0894	.0546	.0441	.0691	.0666	.1376	.2648	.6816	.6104	33
34	.0129	.0132	.0156	.0144	.0154	.0170	.0191	.0221	.0268	.0383	.0418	.0564	.0823	.1538	.2697	.7203	30
36	.0108	.0110	.0113	.0119	.0187	.0158	.0155	.0175	.0204	.0246	.0508	.0596	.0541	.0798	.1511	.2578	28
38	.0086	.0091	.0094	.0098	.0105	.0114	.0125	.0140	.0168	.0191	.0250	.0890	.0580	.0582	.0788	.1898	26
40	.0075	.0077	.0079	.0068	.0085	.0095	.0108	.0115	.0150	.0180	.0180	.0819	.0378	.0349	.0615	.0775	24
42	.0064	.0065	.0065	.0069	.0075	.0078	.0086	.0093	.0108	.0121	.0143	.0171	.0811	.0470	.0560	.0609	22
44	.0053	.0063	.0064	.0065	.0059	.0055	.0068	.0078	.0085	.0094	.0110	.0162	.0156	.0194	.0250	.0338	20
46	.0046	.0048	.0047	.0049	.0051	.0054	.0059	.0064	.0071	.0080	.0091	.0107	.0128	.0168	.0198	.0259	18
48	.0038	.0039	.0040	.0041	.0045	.0045	.0049	.0053	.0058	.0065	.0074	.0086	.0108	.0132	.0151	.0193	16
50	.0031	.0031	.0033	.0034	.0056	.0038	.0040	.0043	.0048	.0058	.0060	.0069	.0080	.0095	.0117	.0146	14
52	.0026	.0026	.0026	.0027	.0028	.0030	.0033	.0056	.0059	.0045	.0048	.0055	.0064	.0076	.0090	.0118	12
54	.0020	.0021	.0021	.0028	.0023	.0034	.0026	.0028	.0030	.0034	.0058	.0043	.0050	.0068	.0070	.0085	10
56	.0016	.0016	.0016	.0017	.0018	.0018	.0020	.0021	.0025	.0026	.0028	.0038	.0044	.0058	.0068	.0085	8
58	.0016	.0018	.0018	.0018	.0013	.0014	.0014	.0016	.0017	.0018	.0081	.0025	.0027	.0051	.0058	.0045	6
60	.0008	.0008	.0008	.0008	.0008	.0009	.0009	.0010	.0011	.0012	.0013	.0015	.0017	.0020	.0024	.0038	4
62	.0004	.0004	.0004	.0004	.0004	.0004	.0005	.0005	.0006	.0007	.0007	.0008	.0010	.0013	.0014	.0014	3
	63	61	59	57	55	53	51	49	47	45	43	41	39	37	35	33	ν

μ	2	4	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36	38	40	42	44	46	48	50	52	54	56	58	60	62	64	66	68	70	72	74	76	78	80	82	84	86	88	90	92	94	96	98	100	102	104	106	108	110	112	114	116	118	120	122	124	126	128	130	132	134	136	138	140	142	144	146	148	150	152	154	156	158	160	162	164	166	168	170	172	174	176	178	180	182	184	186	188	190	192	194	196	198	200	202	204	206	208	210	212	214	216	218	220	222	224	226	228	230	232	234	236	238	240	242	244	246	248	250	252	254	256	258	260	262	264	266	268	270	272	274	276	278	280	282	284	286	288	290	292	294	296	298	300	302	304	306	308	310	312	314	316	318	320	322	324	326	328	330	332	334	336	338	340	342	344	346	348	350	352	354	356	358	360	362	364	366	368	370	372	374	376	378	380	382	384	386	388	390	392	394	396	398	400	402	404	406	408	410	412	414	416	418	420	422	424	426	428	430	432	434	436	438	440	442	444	446	448	450	452	454	456	458	460	462	464	466	468	470	472	474	476	478	480	482	484	486	488	490	492	494	496	498	500	502	504	506	508	510	512	514	516	518	520	522	524	526	528	530	532	534	536	538	540	542	544	546	548	550	552	554	556	558	560	562	564	566	568	570	572	574	576	578	580	582	584	586	588	590	592	594	596	598	600	602	604	606	608	610	612	614	616	618	620	622	624	626	628	630	632	634	636	638	640	642	644	646	648	650	652	654	656	658	660	662	664	666	668	670	672	674	676	678	680	682	684	686	688	690	692	694	696	698	700	702	704	706	708	710	712	714	716	718	720	722	724	726	728	730	732	734	736	738	740	742	744	746	748	750	752	754	756	758	760	762	764	766	768	770	772	774	776	778	780	782	784	786	788	790	792	794	796	798	800	802	804	806	808	810	812	814	816	818	820	822	824	826	828	830	832	834	836	838	840	842	844	846	848	850	852	854	856	858	860	862	864	866	868	870	872	874	876	878	880	882	884	886	888	890	892	894	896	898	900	902	904	906	908	910	912	914	916	918	920	922	924	926	928	930	932	934	936	938	940	942	944	946	948	950	952	954	956	958	960	962	964	966	968	970	972	974	976	978	980	982	984	986	988	990	992	994	996	998	1000	1002	1004	1006	1008	1010	1012	1014	1016	1018	1020	1022	1024	1026	1028	1030	1032	1034	1036	1038	1040	1042	1044	1046	1048	1050	1052	1054	1056	1058	1060	1062	1064	1066	1068	1070	1072	1074	1076	1078	1080	1082	1084	1086	1088	1090	1092	1094	1096	1098	1100	1102	1104	1106	1108	1110	1112	1114	1116	1118	1120	1122	1124	1126	1128	1130	1132	1134	1136	1138	1140	1142	1144	1146	1148	1150	1152	1154	1156	1158	1160	1162	1164	1166	1168	1170	1172	1174	1176	1178	1180	1182	1184	1186	1188	1190	1192	1194	1196	1198	1200	1202	1204	1206	1208	1210	1212	1214	1216	1218	1220	1222	1224	1226	1228	1230	1232	1234	1236	1238	1240	1242	1244	1246	1248	1250	1252	1254	1256	1258	1260	1262	1264	1266	1268	1270	1272	1274	1276	1278	1280	1282	1284	1286	1288	1290	1292	1294	1296	1298	1300	1302	1304	1306	1308	1310	1312	1314	1316	1318	1320	1322	1324	1326	1328	1330	1332	1334	1336	1338	1340	1342	1344	1346	1348	1350	1352	1354	1356	1358	1360	1362	1364	1366	1368	1370	1372	1374	1376	1378	1380	1382	1384	1386	1388	1390	1392	1394	1396	1398	1400	1402	1404	1406	1408	1410	1412	1414	1416	1418	1420	1422	1424	1426	1428	1430	1432	1434	1436	1438	1440	1442	1444	1446	1448	1450	1452	1454	1456	1458	1460	1462	1464	1466	1468	1470	1472	1474	1476	1478	1480	1482	1484	1486	1488	1490	1492	1494	1496	1498	1500	1502	1504	1506	1508	1510	1512	1514	1516	1518	1520	1522	1524	1526	1528	1530	1532	1534	1536	1538	1540	1542	1544	1546	1548	1550	1552	1554	1556	1558	1560	1562	1564	1566	1568	1570	1572	1574	1576	1578	1580	1582	1584	1586	1588	1590	1592	1594	1596	1598	1600	1602	1604	1606	1608	1610	1612	1614	1616	1618	1620	1622	1624	1626	1628	1630	1632	1634	1636	1638	1640	1642	1644	1646	1648	1650	1652	1654	1656	1658	1660	1662	1664	1666	1668	1670	1672	1674	1676	1678	1680	1682	1684	1686	1688	1690	1692	1694	1696	1698	1700	1702	1704	1706	1708	1710	1712	1714	1716	1718	1720	1722	1724	1726	1728	1730	1732	1734	1736	1738	1740	1742	1744	1746	1748	1750	1752	1754	1756	1758	1760	1762	1764	1766	1768	1770	1772	1774	1776	1778	1780	1782	1784	1786	1788	1790	1792	1794	1796	1798	1800	1802	1804	1806	1808	1810	1812	1814	1816	1818	1820	1822	1824	1826	1828	1830	1832	1834	1836	1838	1840	1842	1844	1846	1848	1850	1852	1854	1856	1858	1860	1862	1864	1866	1868	1870	1872	1874	1876	1878	1880	1882	1884	1886	1888	1890	1892	1894	1896	1898	1900	1902	1904	1906	1908	1910	1912	1914	1916	1918	1920	1922	1924	1926	1928	1930	1932	1934	1936	1938	1940	1942	1944	1946	1948	1950	1952	1954	1956	1958	1960	1962	1964	1966	1968	1970	1972	1974	1976	1978	1980	1982	1984	1986	1988	1990	1992	1994	1996	1998	2000	2002	2004	2006	2008	2010	2012	2014	2016	2018	2020	2022	2024	2026	2028	2030	2032	2034	2036	2038	2040	2042	2044	2046	2048	2050	2052	2054	2056	2058	2060	2062	2064	2066	2068	2070	2072	2074	2076	2078	2080	2082	2084	2086	2088	2090	2092	2094	2096	2098	2100	2102	2104	2106	2108	2110	2112	2114	2116	2118	2120	2122	2124	2126	2128	2130	2132	2134	2136	2138	2140	2142	2144	2146	2148	2150	2152	2154	2156	2158	2160	2162	2164	2166	2168	2170	2172	2174	2176	2178	2180	2182	2184	2186	2188	2190	2192	2194	2196	2198	2200	2202	2204	2206	2208	2210	2212	2214	2216	2218	2220	2222	2224	2226	2228	2230	2232	2234	2236	2238	2240	2242	2244	2246	2248	2250	2252	2254	2256	2258	2260	2262	2264	2266	2268	2270	2272	2274	2276	2278	2280	2282	2284	2286	2288	2290	2292	2294	2296	2298	2300	2302	2304	2306	2308	2310	2312	2314	2316	2318	2320	2322	2324	2326	2328	2330	2332	2334	2336	2338	2340	2342	2344	2346	2348	2350	2352	2354	2356	2358	2360	2362	2364	2366	2368	2370	2372	2374	2376	2378	2380	2382	2384	2386	2388	2390	2392	2394	2396	2398	2400	2402	2404	2406	2408	2410	2412	2414	2416	2418	2420	2422	2424	2426	2428	2430	2432	2434	2436	2438	2440	2442	2444	2446	2448	2450	2452	2454	2456	2458	2460	2462	2464	2466	2468	2470	2472	2474	2476	2478	2480	2482	2484	2486	2488	2490	2492	2494	2496	2498	2500	2502	2504	2506	2508	2510	2512	2514	2516	2518	2520	2522	2524	2526	2528	2530	2532	2534	2536	2538	2540	2542	2544	2546	2548	2550	2552	2554	2556	2558	2560	2562	2564	2566	2568	2570	2572	2574	2576	2578	2580	2582	2584	2586	2588	2590	2592	2594	2596	2598	2600	2602	2604	2606	2608	2610	2612	2614	261

APPENDIX B

VALUES OF j_{no} AND j_{no}^* AS FUNCTIONS OF $\frac{x_n - x_0}{\Delta x}$

The values of the functions j_{no} and j_{no}^* are presented as indicated in the following table. The values are tabulated in a form selected to minimize the necessity for interpolation except for the region containing the singularities of the functions j_{no} and j_{no}^* . For ease in computation, tables B-I to B-VIII, inclusive, are arranged so that the vertical increment of $\frac{x_n - x_0}{\Delta x}$ is unity. Table B-IX gives additional values for the region containing the singularities of the functions j_{no} and j_{no}^* .

TABLE NO.	RANGE OF $\frac{x_n - x_0}{\Delta x}$	INCREMENT OF $\frac{x_n - x_0}{\Delta x}$
B-I	-189 to -90	1.0
B-II	-89.5 to -40.0	.5
B-III	-39.9 to -20.0	.1
B-IV	-19.99 to 0	.01
B-V	0 to 19.99	.01
B-VI	20.0 to 39.9	.1
B-VII	40.0 to 89.5	.5
B-VIII	90 to 189	1.0
B-IX	-1.000 to 0.000	0.001

TABLE B-I.— VALUES OF j_{no} AND j_{no}^* USED IN EVALUATING EQUATION (26)

$$-189 \leq \frac{x_n - x_0}{\Delta x} \leq -90$$

$\frac{x_n - x_0}{\Delta x}$	-18x.0		-1.		-16x.0		-15x.0		-14x.0		-13x.0		-12x.0		-11x.0		-10x.0		-9x.0	
x	j_{no}	j_{no}^*																		
9	-0.0053	-0.0027	-0.0056	-0.0028	-0.0059	-0.0030	-0.0063	-0.0032	-0.0067	-0.0034	-0.0072	-0.0036	-0.0078	-0.0039	-0.0084	-0.0042	-0.0092	-0.0046	-0.0102	-0.0051
8	-0.0053	-0.0027	-0.0056	-0.0028	-0.0060	-0.0030	-0.0063	-0.0032	-0.0068	-0.0034	-0.0073	-0.0036	-0.0078	-0.0039	-0.0085	-0.0043	-0.0093	-0.0047	-0.0103	-0.0051
7	-0.0054	-0.0027	-0.0057	-0.0028	-0.0060	-0.0030	-0.0064	-0.0032	-0.0068	-0.0034	-0.0073	-0.0037	-0.0079	-0.0040	-0.0086	-0.0043	-0.0094	-0.0047	-0.0104	-0.0052
6	-0.0054	-0.0027	-0.0057	-0.0029	-0.0060	-0.0030	-0.0064	-0.0032	-0.0069	-0.0034	-0.0074	-0.0037	-0.0080	-0.0040	-0.0087	-0.0043	-0.0095	-0.0047	-0.0105	-0.0053
5	-0.0054	-0.0027	-0.0057	-0.0029	-0.0061	-0.0030	-0.0065	-0.0032	-0.0069	-0.0035	-0.0074	-0.0037	-0.0080	-0.0040	-0.0087	-0.0044	-0.0096	-0.0047	-0.0106	-0.0053
4	-0.0054	-0.0027	-0.0057	-0.0029	-0.0061	-0.0031	-0.0065	-0.0033	-0.0070	-0.0035	-0.0075	-0.0037	-0.0081	-0.0041	-0.0088	-0.0045	-0.0097	-0.0048	-0.0107	-0.0053
3	-0.0055	-0.0027	-0.0058	-0.0029	-0.0062	-0.0031	-0.0066	-0.0033	-0.0071	-0.0035	-0.0076	-0.0038	-0.0082	-0.0041	-0.0090	-0.0045	-0.0099	-0.0049	-0.0109	-0.0054
2	-0.0055	-0.0028	-0.0058	-0.0029	-0.0062	-0.0031	-0.0066	-0.0033	-0.0071	-0.0036	-0.0077	-0.0038	-0.0083	-0.0042	-0.0090	-0.0045	-0.0100	-0.0050	-0.0110	-0.0055
1	-0.0055	-0.0028	-0.0059	-0.0029	-0.0062	-0.0031	-0.0066	-0.0033	-0.0071	-0.0036	-0.0077	-0.0039	-0.0084	-0.0042	-0.0091	-0.0046	-0.0101	-0.0050	-0.0112	-0.0056
0	-0.0056	-0.0028	-0.0059	-0.0030	-0.0063	-0.0031	-0.0067	-0.0033	-0.0072	-0.0036	-0.0077	-0.0039	-0.0084	-0.0042	-0.0091	-0.0046	-0.0101	-0.0050	-0.0112	-0.0056

TABLE B-II.— VALUES OF j_{no} AND j_{no}^* USED IN EVALUATING EQUATION (26)

$$-89.5 \leq \frac{x_n - x_0}{\Delta x} \leq -40.0$$

$\frac{x_n - x_0}{\Delta x}$	-8x.5		-8x.0		-7x.5		-7x.0		-6x.5		-6x.0		-5x.5		-5x.0		-4x.5		-4x.0	
x	j_{no}	j_{no}^*																		
9	-0.0112	-0.0056	-0.0113	-0.0057	-0.0127	-0.0064	-0.0127	-0.0064	-0.0145	-0.0073	-0.0146	-0.0073	-0.0169	-0.0085	-0.0171	-0.0087	-0.0204	-0.0102	-0.0206	-0.0103
8	-0.0114	-0.0057	-0.0114	-0.0058	-0.0128	-0.0064	-0.0129	-0.0064	-0.0147	-0.0074	-0.0148	-0.0074	-0.0172	-0.0086	-0.0174	-0.0087	-0.0208	-0.0104	-0.0211	-0.0105
7	-0.0115	-0.0058	-0.0116	-0.0058	-0.0130	-0.0065	-0.0131	-0.0065	-0.0149	-0.0075	-0.0150	-0.0075	-0.0173	-0.0088	-0.0177	-0.0089	-0.0213	-0.0107	-0.0215	-0.0108
6	-0.0116	-0.0058	-0.0117	-0.0059	-0.0132	-0.0066	-0.0132	-0.0067	-0.0152	-0.0076	-0.0153	-0.0076	-0.0179	-0.0090	-0.0180	-0.0090	-0.0217	-0.0109	-0.0220	-0.0110
5	-0.0118	-0.0059	-0.0118	-0.0059	-0.0133	-0.0067	-0.0134	-0.0067	-0.0154	-0.0077	-0.0155	-0.0078	-0.0182	-0.0092	-0.0184	-0.0093	-0.0222	-0.0112	-0.0225	-0.0112
4	-0.0119	-0.0059	-0.0120	-0.0060	-0.0133	-0.0067	-0.0136	-0.0068	-0.0156	-0.0078	-0.0157	-0.0079	-0.0185	-0.0093	-0.0187	-0.0094	-0.0227	-0.0114	-0.0230	-0.0116
3	-0.0120	-0.0060	-0.0121	-0.0061	-0.0137	-0.0068	-0.0138	-0.0069	-0.0159	-0.0079	-0.0160	-0.0080	-0.0189	-0.0094	-0.0190	-0.0095	-0.0233	-0.0117	-0.0235	-0.0118
2	-0.0122	-0.0061	-0.0123	-0.0061	-0.0139	-0.0070	-0.0140	-0.0070	-0.0161	-0.0081	-0.0163	-0.0081	-0.0192	-0.0096	-0.0194	-0.0097	-0.0238	-0.0120	-0.0241	-0.0121
1	-0.0123	-0.0062	-0.0124	-0.0062	-0.0141	-0.0071	-0.0142	-0.0071	-0.0164	-0.0082	-0.0165	-0.0083	-0.0195	-0.0099	-0.0196	-0.0100	-0.0244	-0.0122	-0.0247	-0.0124
0	-0.0125	-0.0062	-0.0126	-0.0063	-0.0143	-0.0071	-0.0144	-0.0072	-0.0167	-0.0084	-0.0168	-0.0084	-0.0200	-0.0101	-0.0202	-0.0102	-0.0250	-0.0125	-0.0253	-0.0127

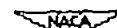


TABLE B-III.— VALUES OF j_{no} AND j_{no}^* USED IN EVALUATING EQUATION (26)

$$-39.9 \leq \frac{x_2 - x_0}{\Delta x} \leq -20.0$$

$\frac{x_2 - x_0}{\Delta x}$	9		8		7		6		5		4		3		2		1		0	
	j_{no}	j_{no}^*																		
-39.9	-0.0254	-0.0127	-0.0254	-0.0128	-0.0255	-0.0128	-0.0256	-0.0128	-0.0256	-0.0129	-0.0257	-0.0129	-0.0258	-0.0130	-0.0258	-0.0130	-0.0259	-0.0130	-0.0260	-0.0131
-38.	-0.0260	-0.0131	-0.0261	-0.0131	-0.0262	-0.0132	-0.0262	-0.0132	-0.0263	-0.0132	-0.0264	-0.0133	-0.0265	-0.0133	-0.0266	-0.0134	-0.0267	-0.0134	-0.0268	-0.0134
-37.	-0.0267	-0.0134	-0.0268	-0.0135	-0.0269	-0.0135	-0.0270	-0.0135	-0.0270	-0.0136	-0.0271	-0.0137	-0.0272	-0.0137	-0.0273	-0.0137	-0.0274	-0.0138	-0.0275	-0.0138
-36.	-0.0273	-0.0138	-0.0276	-0.0138	-0.0276	-0.0139	-0.0277	-0.0139	-0.0276	-0.0139	-0.0279	-0.0140	-0.0279	-0.0140	-0.0280	-0.0141	-0.0281	-0.0141	-0.0282	-0.0141
-35.	-0.0283	-0.0142	-0.0283	-0.0142	-0.0284	-0.0142	-0.0285	-0.0143	-0.0286	-0.0143	-0.0287	-0.0144	-0.0287	-0.0145	-0.0288	-0.0145	-0.0289	-0.0145	-0.0290	-0.0146
-34.	-0.0291	-0.0146	-0.0292	-0.0146	-0.0292	-0.0147	-0.0293	-0.0147	-0.0294	-0.0148	-0.0295	-0.0148	-0.0296	-0.0149	-0.0297	-0.0149	-0.0298	-0.0150	-0.0299	-0.0150
-33.	-0.0299	-0.0150	-0.0300	-0.0151	-0.0301	-0.0151	-0.0302	-0.0152	-0.0303	-0.0153	-0.0304	-0.0153	-0.0305	-0.0154	-0.0306	-0.0154	-0.0307	-0.0154	-0.0308	-0.0155
-32.	-0.0309	-0.0156	-0.0310	-0.0156	-0.0311	-0.0156	-0.0312	-0.0157	-0.0313	-0.0157	-0.0314	-0.0158	-0.0315	-0.0158	-0.0315	-0.0158	-0.0316	-0.0159	-0.0317	-0.0160
-31.	-0.0319	-0.0160	-0.0320	-0.0161	-0.0321	-0.0161	-0.0322	-0.0162	-0.0323	-0.0162	-0.0324	-0.0163	-0.0325	-0.0163	-0.0326	-0.0164	-0.0327	-0.0164	-0.0328	-0.0165
-30.	-0.0329	-0.0165	-0.0330	-0.0166	-0.0331	-0.0166	-0.0332	-0.0167	-0.0333	-0.0167	-0.0334	-0.0168	-0.0336	-0.0169	-0.0337	-0.0169	-0.0338	-0.0170	-0.0339	-0.0171
-29.	-0.0340	-0.0171	-0.0341	-0.0172	-0.0342	-0.0172	-0.0344	-0.0173	-0.0345	-0.0173	-0.0346	-0.0174	-0.0347	-0.0175	-0.0348	-0.0175	-0.0350	-0.0176	-0.0351	-0.0176
-28.	-0.0358	-0.0177	-0.0353	-0.0178	-0.0357	-0.0178	-0.0356	-0.0179	-0.0357	-0.0180	-0.0358	-0.0180	-0.0360	-0.0181	-0.0361	-0.0182	-0.0362	-0.0182	-0.0364	-0.0183
-27.	-0.0365	-0.0184	-0.0366	-0.0184	-0.0368	-0.0185	-0.0369	-0.0186	-0.0370	-0.0186	-0.0372	-0.0187	-0.0373	-0.0188	-0.0375	-0.0188	-0.0376	-0.0189	-0.0377	-0.0190
-26.	-0.0379	-0.0191	-0.0380	-0.0191	-0.0382	-0.0192	-0.0383	-0.0193	-0.0385	-0.0193	-0.0386	-0.0194	-0.0388	-0.0195	-0.0389	-0.0196	-0.0391	-0.0196	-0.0392	-0.0197
-25.	-0.0394	-0.0198	-0.0395	-0.0199	-0.0397	-0.0200	-0.0398	-0.0200	-0.0400	-0.0201	-0.0402	-0.0202	-0.0403	-0.0203	-0.0405	-0.0204	-0.0407	-0.0205	-0.0408	-0.0206
-24.	-0.0410	-0.0206	-0.0412	-0.0207	-0.0413	-0.0208	-0.0415	-0.0209	-0.0417	-0.0210	-0.0418	-0.0211	-0.0420	-0.0211	-0.0422	-0.0212	-0.0424	-0.0213	-0.0426	-0.0214
-23.	-0.0427	-0.0215	-0.0429	-0.0216	-0.0431	-0.0217	-0.0433	-0.0218	-0.0435	-0.0219	-0.0437	-0.0219	-0.0439	-0.0221	-0.0441	-0.0222	-0.0443	-0.0223	-0.0444	-0.0223
-22.	-0.0447	-0.0225	-0.0449	-0.0226	-0.0451	-0.0227	-0.0453	-0.0228	-0.0455	-0.0229	-0.0457	-0.0230	-0.0459	-0.0231	-0.0461	-0.0232	-0.0463	-0.0233	-0.0465	-0.0233
-21.	-0.0467	-0.0236	-0.0470	-0.0237	-0.0472	-0.0238	-0.0474	-0.0239	-0.0476	-0.0240	-0.0479	-0.0241	-0.0481	-0.0242	-0.0483	-0.0243	-0.0486	-0.0244	-0.0488	-0.0246
-20.X	-0.0490	-0.0247	-0.0493	-0.0248	-0.0495	-0.0250	-0.0496	-0.0251	-0.0500	-0.0252	-0.0503	-0.0253	-0.0505	-0.0255	-0.0508	-0.0256	-0.0510	-0.0257	-0.0513	-0.0259

NACA

TABLE B-IV.—VALUES OF j_{no} AND j_{no}^* USED IN EVALUATING EQUATION (26)

$$(a) -19.xx \leq \frac{x_n - x_0}{\Delta x} \leq -0.xx \quad \text{where } 99 \geq xx \geq 90$$

TABLE B-IV.—CONTINUED

$$(b) -19.XX \leq \frac{x_n - x_0}{\Delta x} \leq -0.XX \quad \text{where } 89 \geq XX \geq 80$$

	89	88	87	86	85	84	83	82	81	80
	\bar{J}_{H}	\bar{J}_{H}^*								
-19.IX	-0.0716	-0.0260	-0.0716	-0.0260	-0.0716	-0.0260	-0.0717	-0.0261	-0.0717	-0.0261
-16.	-0.0714	-0.0278	-0.0714	-0.0278	-0.0714	-0.0278	-0.0715	-0.0279	-0.0715	-0.0279
-17.	-0.0713	-0.0293	-0.0713	-0.0293	-0.0713	-0.0293	-0.0717	-0.0293	-0.0717	-0.0293
-16.	-0.0710	-0.0310	-0.0710	-0.0310	-0.0710	-0.0310	-0.0722	-0.0310	-0.0722	-0.0310
-15.	-0.0690	-0.0328	-0.0690	-0.0328	-0.0690	-0.0328	-0.0692	-0.0329	-0.0692	-0.0329
-14.	-0.0695	-0.0346	-0.0695	-0.0346	-0.0695	-0.0346	-0.0697	-0.0346	-0.0697	-0.0346
-13.	-0.0747	-0.0747	-0.0748	-0.0748	-0.0748	-0.0748	-0.0749	-0.0749	-0.0749	-0.0749
-12.	-0.0803	-0.0809	-0.0808	-0.0808	-0.0809	-0.0808	-0.0810	-0.0809	-0.0810	-0.0809
-11.	-0.0879	-0.0846	-0.0879	-0.0847	-0.0879	-0.0847	-0.0880	-0.0847	-0.0880	-0.0847
-10.	-0.0983	-0.0849	-0.0983	-0.0849	-0.0983	-0.0849	-0.0984	-0.0849	-0.0984	-0.0849
-9.	-0.0982	-0.0743	-0.0987	-0.0743	-0.0982	-0.0743	-0.0986	-0.0743	-0.0986	-0.0743
-8.	-0.1193	-0.0608	-0.1193	-0.0609	-0.1193	-0.0610	-0.1198	-0.0609	-0.1198	-0.0609
-7.	-0.1353	-0.0693	-0.1357	-0.0694	-0.1359	-0.0695	-0.1361	-0.0696	-0.1363	-0.0697
-6.	-0.1368	-0.0605	-0.1371	-0.0606	-0.1373	-0.0607	-0.1376	-0.0608	-0.1378	-0.0609
-5.	-0.1661	-0.0529	-0.1664	-0.0531	-0.1668	-0.0533	-0.1671	-0.0535	-0.1673	-0.0536
-4.	-0.2268	-0.1187	-0.2269	-0.1189	-0.2269	-0.1193	-0.2270	-0.1195	-0.2270	-0.1195
-3.	-0.2972	-0.1592	-0.2970	-0.1592	-0.2970	-0.1592	-0.2974	-0.1594	-0.2974	-0.1594
-2.	-0.4247	-0.2773	-0.4265	-0.2784	-0.4265	-0.2784	-0.4268	-0.2785	-0.4268	-0.2785
-1.	-0.7311	-0.4354	-0.7511	-0.4371	-0.7511	-0.4374	-0.7777	-0.4464	-0.7905	-0.4649
-0.IX	-0.9098	-0.8908	-0.9095	-0.8903	-0.9095	-0.8903	-0.7346	-0.4744	-0.5982	-0.3993

TABLE B-IV.—CONTINUED

$$(c) -19.xx \leq \frac{x_n - x_0}{\Delta x} \leq -0.xx \quad \text{where} \quad 79 \geq xx \geq 70$$

XX	T9	T6	T7	T6	T5	T4	T3	T2	T1	T0
zg=80	400	400*	400	400*	400	400*	400	400	400	400*
zg=80	400	400	400	400	400	400	400	400	400	400
-19.IX	-0.0519	-0.0568	-0.0519	-0.0568	-0.0519	-0.0568	-0.0519	-0.0568	-0.0519	-0.0568
-18.	-0.0517	-0.0576	-0.0517	-0.0576	-0.0517	-0.0576	-0.0517	-0.0576	-0.0517	-0.0576
-17.	-0.0579	-0.0598	-0.0579	-0.0598	-0.0579	-0.0598	-0.0579	-0.0598	-0.0579	-0.0598
-16.	-0.0514	-0.0510	-0.0514	-0.0510	-0.0514	-0.0510	-0.0514	-0.0510	-0.0514	-0.0510
-15.	-0.0514	-0.0511	-0.0514	-0.0511	-0.0514	-0.0511	-0.0514	-0.0511	-0.0514	-0.0511
-14.	-0.0700	-0.0701	-0.0700	-0.0701	-0.0700	-0.0701	-0.0700	-0.0701	-0.0700	-0.0701
-13.	-0.0729	-0.0731	-0.0729	-0.0731	-0.0729	-0.0731	-0.0729	-0.0731	-0.0729	-0.0731
-12.	-0.0714	-0.0715	-0.0714	-0.0715	-0.0714	-0.0715	-0.0714	-0.0715	-0.0714	-0.0715
-11.	-0.0885	-0.0849	-0.0885	-0.0849	-0.0885	-0.0849	-0.0885	-0.0849	-0.0885	-0.0849
-10.	-0.0713	-0.0692	-0.0713	-0.0692	-0.0713	-0.0692	-0.0713	-0.0692	-0.0713	-0.0692
-9.	-0.1076	-0.0959	-0.1076	-0.0959	-0.1076	-0.0959	-0.1076	-0.0959	-0.1076	-0.0959
-8.	-0.1006	-0.0865	-0.1006	-0.0865	-0.1006	-0.0865	-0.1006	-0.0865	-0.1006	-0.0865
-7.	-0.1374	-0.0703	-0.1374	-0.0703	-0.1374	-0.0703	-0.1374	-0.0703	-0.1374	-0.0703
-6.	-0.1523	-0.0818	-0.1523	-0.0818	-0.1523	-0.0818	-0.1523	-0.0818	-0.1523	-0.0818
-5.	-0.1808	-0.0761	-0.1808	-0.0761	-0.1808	-0.0761	-0.1808	-0.0761	-0.1808	-0.0761
-4.	-0.2342	-0.1116	-0.2342	-0.1116	-0.2342	-0.1116	-0.2342	-0.1116	-0.2342	-0.1116
-3.	-0.3065	-0.1610	-0.3065	-0.1610	-0.3065	-0.1610	-0.3065	-0.1610	-0.3065	-0.1610
-2.	-0.4403	-0.2059	-0.4403	-0.2059	-0.4403	-0.2059	-0.4403	-0.2059	-0.4403	-0.2059
-1.	-0.6179	-0.4641	-0.6179	-0.4641	-0.6179	-0.4641	-0.6179	-0.4641	-0.6179	-0.4641
0.II	-1.2049	-0.6667	-1.2049	-0.6667	-1.2049	-0.6667	-1.2049	-0.6667	-1.2049	-0.6667

TABLE B-IV.— CONTINUED

$$(d) -19.XX \leq \frac{x_n - x_0}{\Delta x} \leq -0.XX \quad \text{where } 69 \geq XX \geq 60$$

II	69		68		67		66		65		64		63		62		61		60	
III-8	Age	Sex	Age*	Sex	Age	Sex														
-19, IX	-0,0281	-0,0463	-0,0380	-0,0463	-0,0322	-0,0263	-0,0282	-0,0267	-0,0282	-0,0263	-0,0282	-0,0263	-0,0283	-0,0263	-0,0284	-0,0264	-0,0283	-0,0264	-0,0284	-0,0264
-18,	-0,0550	-0,0777	-0,0550	-0,0778	-0,0590	-0,0716	-0,0591	-0,0716	-0,0591	-0,0716	-0,0591	-0,0716	-0,0592	-0,0717	-0,0592	-0,0717	-0,0592	-0,0717	-0,0592	-0,0717
-17,	-0,0882	-0,0847	-0,0882	-0,0847	-0,0883	-0,0894	-0,0883	-0,0894	-0,0883	-0,0894	-0,0883	-0,0894	-0,0884	-0,0895	-0,0884	-0,0895	-0,0884	-0,0895	-0,0884	-0,0895
-16,	-0,0518	-0,0332	-0,0518	-0,0332	-0,0519	-0,0313	-0,0519	-0,0313	-0,0519	-0,0313	-0,0519	-0,0313	-0,0520	-0,0313	-0,0520	-0,0313	-0,0520	-0,0313	-0,0520	
-15,	-0,0599	-0,0333	-0,0599	-0,0333	-0,0600	-0,0333	-0,0600	-0,0334	-0,0600	-0,0334	-0,0600	-0,0334	-0,0601	-0,0334	-0,0601	-0,0334	-0,0601	-0,0334	-0,0601	
-14,	-0,0703	-0,0357	-0,0706	-0,0357	-0,0706	-0,0357	-0,0707	-0,0357	-0,0707	-0,0358	-0,0708	-0,0358	-0,0708	-0,0358	-0,0708	-0,0358	-0,0708	-0,0358	-0,0708	
-13,	-0,0758	-0,0364	-0,0759	-0,0364	-0,0760	-0,0365	-0,0760	-0,0365	-0,0761	-0,0365	-0,0761	-0,0366	-0,0762	-0,0366	-0,0762	-0,0366	-0,0763	-0,0366	-0,0764	
-12,	-0,0801	-0,0416	-0,0802	-0,0417	-0,0802	-0,0417	-0,0803	-0,0417	-0,0803	-0,0417	-0,0803	-0,0417	-0,0804	-0,0418	-0,0804	-0,0418	-0,0805	-0,0419	-0,0805	
-11,	-0,0854	-0,0424	-0,0855	-0,0425	-0,0856	-0,0425	-0,0857	-0,0425	-0,0857	-0,0425	-0,0858	-0,0426	-0,0858	-0,0426	-0,0858	-0,0426	-0,0859	-0,0427	-0,0859	
-10,	-0,0902	-0,0459	-0,0903	-0,0460	-0,0904	-0,0460	-0,0905	-0,0460	-0,0905	-0,0460	-0,0906	-0,0461	-0,0906	-0,0461	-0,0906	-0,0461	-0,0907	-0,0462	-0,0907	
-9,	-0,1069	-0,0554	-0,1070	-0,0555	-0,1072	-0,0556	-0,1073	-0,0556	-0,1073	-0,0556	-0,1074	-0,0557	-0,1074	-0,0557	-0,1074	-0,0557	-0,1075	-0,0558	-0,1075	
-8,	-0,1285	-0,0604	-0,1286	-0,0604	-0,1286	-0,0605	-0,1287	-0,0605	-0,1287	-0,0605	-0,1288	-0,0606	-0,1288	-0,0606	-0,1288	-0,0606	-0,1289	-0,0607	-0,1289	
-7,	-0,1393	-0,0713	-0,1393	-0,0714	-0,1397	-0,0715	-0,1399	-0,0716	-0,1401	-0,0717	-0,1403	-0,0718	-0,1403	-0,0718	-0,1403	-0,0718	-0,1404	-0,0719	-0,1404	
-6,	-0,1519	-0,0838	-0,1520	-0,0838	-0,1524	-0,0843	-0,1527	-0,0843	-0,1527	-0,0843	-0,1530	-0,0847	-0,1530	-0,0847	-0,1530	-0,0847	-0,1531	-0,0848	-0,1531	
-5,	-0,1523	-0,0906	-0,1527	-0,0907	-0,1540	-0,0908	-0,1544	-0,0909	-0,1544	-0,0909	-0,1546	-0,0910	-0,1546	-0,0910	-0,1546	-0,0910	-0,1547	-0,0911	-0,1547	
-4,	-0,2023	-0,1847	-0,2024	-0,1848	-0,2020	-0,1853	-0,2021	-0,1853	-0,2021	-0,1853	-0,2022	-0,1854	-0,2022	-0,1854	-0,2022	-0,1854	-0,2023	-0,1855	-0,2023	
-3,	-0,2161	-0,1854	-0,2172	-0,1855	-0,2171	-0,1857	-0,2172	-0,1857	-0,2172	-0,1857	-0,2173	-0,1858	-0,2173	-0,1858	-0,2173	-0,1858	-0,2174	-0,1859	-0,2174	
-2,	-0,2488	-0,1904	-0,2470	-0,1905	-0,2469	-0,1905	-0,2475	-0,1905	-0,2475	-0,1905	-0,2478	-0,1906	-0,2478	-0,1906	-0,2478	-0,1906	-0,2479	-0,1907	-0,2479	
-1,	-0,2998	-0,2139	-0,2945	-0,2145	-0,2913	-0,2145	-0,2924	-0,2145	-0,2924	-0,2145	-0,2911	-0,2146	-0,2911	-0,2146	-0,2911	-0,2146	-0,2912	-0,2147	-0,2912	
-0, IX	-0,3001	-0,2179	-0,2949	-0,2179	-0,2908	-0,2179	-0,2922	-0,2179	-0,2922	-0,2179	-0,2913	-0,2181	-0,2913	-0,2181	-0,2913	-0,2181	-0,2914	-0,2181	-0,2914	

TABLE B-IV.— CONTINUED

$$(e) -19.XX \leq \frac{x_n - x_0}{\Delta x} \leq -0.XX \quad \text{where } 59 \geq XX \geq 50$$

TABLE B-IV.— CONTINUED

$$(f) -19.XX \leq \frac{x_n - x_0}{\Delta x} \leq -0.XX \quad \text{where } .49 \geq XX \geq .40$$

TABLE B-IV.— CONTINUED

$$(i) \quad -19.XX \leq \frac{x_n - x_0}{\Delta x} \leq -0.XX \quad \text{where } 19 \geq XX \geq 10$$

$\frac{J}{2K}$	19	18	17	16	15	14	13	12	11	10
$\frac{J}{2K}$	J_{100}	J_{100}^*								
-19	-0.055	-0.0870	-0.0395	-0.0270	-0.0336	-0.0270	-0.0316	-0.0270	-0.0336	-0.0271
-18	-0.062	-0.0863	-0.0666	-0.0686	-0.0666	-0.0666	-0.0666	-0.0666	-0.0667	-0.0666
-17	-0.059	-0.0860	-0.0660	-0.0603	-0.0603	-0.0603	-0.0603	-0.0603	-0.0603	-0.0603
-16	-0.068	-0.0922	-0.0682	-0.0624	-0.0618	-0.0618	-0.0618	-0.0618	-0.0618	-0.0618
-15	-0.061	-0.0944	-0.0681	-0.0643	-0.0643	-0.0643	-0.0643	-0.0643	-0.0643	-0.0643
-14	-0.071	-0.070	-0.071	-0.070	-0.072	-0.070	-0.078	-0.072	-0.073	-0.071
-13	-0.078	-0.0599	-0.0769	-0.0600	-0.0790	-0.0600	-0.0790	-0.0600	-0.0790	-0.0600
-12	-0.066	-0.0434	-0.057	-0.0434	-0.0557	-0.0434	-0.0595	-0.0436	-0.0595	-0.0436
-11	-0.056	-0.0473	-0.057	-0.0476	-0.0585	-0.0476	-0.0593	-0.0477	-0.0590	-0.0477
-10	-1.093	-0.0523	-1.093	-0.0526	-1.093	-0.0526	-1.093	-0.0527	-1.093	-0.0527
-9	-1.153	-0.057	-1.153	-0.0588	-1.153	-0.0588	-1.153	-0.0589	-1.153	-0.0589
-8	-1.108	-0.063	-1.104	-0.0656	-1.106	-0.0656	-1.107	-0.0668	-1.109	-0.0668
-7	-1.098	-0.076	-1.100	-0.0788	-1.098	-0.0788	-1.098	-0.0790	-1.100	-0.0790
-6	-1.178	-0.097	-1.173	-0.0999	-1.178	-0.0999	-1.178	-1.077	-1.178	-1.077
-5	-2.116	-1.116	-2.116	-1.116	-2.116	-1.116	-2.116	-1.116	-2.116	-1.116
-4	-2.757	-1.462	-2.754	-1.463	-2.756	-1.464	-2.756	-1.465	-2.757	-1.464
-3	-3.702	-1.998	-3.778	-2.006	-3.790	-2.014	-3.790	-2.007	-3.819	-2.011
-2	-5.818	-3.756	-5.838	-3.761	-6.177	-3.405	-6.217	-3.428	-6.887	-3.477
-1	-1.854	-1.1653	-1.8603	-1.1618	-1.8890	-1.2059	-1.9010	-1.2080	-1.9469	-1.2139
0	1.4500	1.2753	1.5164	1.2729	1.5856	1.2656	1.6502	1.2693	1.7346	1.2602

TABLE B-IV.— CONCLUDED

$$(j) \quad -19.XX \leq \frac{X_n - X_0}{\Delta x} \leq -0.XX \quad \text{where } 09 \geq XX \geq 00$$

	09	08	07	06	05	04	03	02	01	00
	400	400*	300	300*	300	300*	300	300*	300	300*
-19. xx	-0.0538	-0.0572	-0.0539	-0.0572	-0.0539	-0.0572	-0.0539	-0.0572	-0.0540	-0.0572
-18.	-0.0509	-0.0567	-0.0569	-0.0567	-0.0569	-0.0567	-0.0570	-0.0568	-0.0570	-0.0568
-17.	-0.0504	-0.0563	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504
-16.	-0.0502	-0.0562	-0.0504	-0.0503	-0.0504	-0.0503	-0.0505	-0.0504	-0.0505	-0.0504
-15.	-0.0500	-0.0517	-0.0505	-0.0517	-0.0507	-0.0517	-0.0508	-0.0509	-0.0508	-0.0509
-14.	-0.0516	-0.0573	-0.0517	-0.0517	-0.0517	-0.0517	-0.0518	-0.0518	-0.0518	-0.0518
-13.	-0.0502	-0.0502	-0.0503	-0.0502	-0.0503	-0.0502	-0.0503	-0.0502	-0.0503	-0.0502
-12.	-0.0503	-0.0518	-0.0504	-0.0518	-0.0505	-0.0518	-0.0506	-0.0505	-0.0506	-0.0505
-11.	-0.0504	-0.0500	-0.0506	-0.0504	-0.0505	-0.0504	-0.0506	-0.0505	-0.0506	-0.0505
-10.	-0.0504	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504
-9.	-0.0504	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504
-8.	-0.0504	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504
-7.	-0.0504	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504
-6.	-0.0504	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504
-5.	-0.0504	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504
-4.	-0.0504	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504
-3.	-0.0504	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504
-2.	-0.0504	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504
-1.	-0.0504	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504
0.	-0.0504	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504	-0.0505	-0.0504

NACA TN 2451

TABLE B-V.— VALUES OF j_{no} AND j_{no}^* USED IN EVALUATING EQUATION (26)(a) $0.XX \leq \frac{x_n - x_0}{\Delta x} \leq 19.XX$ where $00 \leq XX \leq 09$

$\frac{x_n - x_0}{\Delta x}$	00		01		02		03		04		05		06		07		08		09		
	j_{no}	j_{no}^*																			
0.000	1.0000	1.0000	1.0151	0.9956	1.0218	0.9924	1.0280	0.9898	1.0351	0.9867	1.0416	0.9837	1.0481	0.9807	1.0547	0.9777	1.0605	0.9747	1.0663	0.9717	1.0714
0.001	0.9999	0.9999	1.0150	0.9955	1.0217	0.9923	1.0278	0.9897	1.0349	0.9866	1.0414	0.9836	1.0479	0.9806	1.0544	0.9774	1.0602	0.9742	1.0659	0.9712	1.0709
0.002	0.9998	0.9998	1.0149	0.9954	1.0216	0.9922	1.0277	0.9896	1.0348	0.9865	1.0413	0.9835	1.0478	0.9805	1.0543	0.9773	1.0601	0.9741	1.0658	0.9711	1.0708
0.003	0.9997	0.9997	1.0148	0.9953	1.0215	0.9921	1.0276	0.9895	1.0347	0.9864	1.0412	0.9834	1.0477	0.9804	1.0542	0.9772	1.0599	0.9740	1.0657	0.9709	1.0707
0.004	0.9996	0.9996	1.0147	0.9952	1.0214	0.9920	1.0275	0.9894	1.0346	0.9863	1.0411	0.9833	1.0476	0.9803	1.0541	0.9771	1.0598	0.9739	1.0656	0.9708	1.0706
0.005	0.9995	0.9995	1.0146	0.9951	1.0213	0.9919	1.0274	0.9893	1.0345	0.9862	1.0410	0.9832	1.0475	0.9802	1.0540	0.9770	1.0597	0.9738	1.0655	0.9707	1.0705
0.006	0.9994	0.9994	1.0145	0.9950	1.0212	0.9918	1.0273	0.9892	1.0344	0.9861	1.0409	0.9831	1.0474	0.9799	1.0539	0.9769	1.0596	0.9737	1.0654	0.9706	1.0704
0.007	0.9993	0.9993	1.0144	0.9949	1.0211	0.9917	1.0272	0.9891	1.0343	0.9860	1.0408	0.9830	1.0473	0.9798	1.0538	0.9768	1.0595	0.9736	1.0653	0.9705	1.0703
0.008	0.9992	0.9992	1.0143	0.9948	1.0210	0.9916	1.0271	0.9890	1.0342	0.9859	1.0407	0.9829	1.0472	0.9797	1.0537	0.9767	1.0594	0.9735	1.0652	0.9704	1.0702
0.009	0.9991	0.9991	1.0142	0.9947	1.0209	0.9915	1.0270	0.9889	1.0341	0.9858	1.0406	0.9828	1.0471	0.9796	1.0536	0.9766	1.0593	0.9734	1.0651	0.9703	1.0701
0.010	0.9990	0.9990	1.0141	0.9946	1.0208	0.9914	1.0269	0.9888	1.0340	0.9857	1.0405	0.9827	1.0470	0.9795	1.0535	0.9765	1.0592	0.9733	1.0650	0.9702	1.0700
0.011	0.9989	0.9989	1.0140	0.9945	1.0207	0.9913	1.0268	0.9887	1.0339	0.9856	1.0404	0.9826	1.0469	0.9794	1.0534	0.9764	1.0591	0.9732	1.0649	0.9701	1.0699
0.012	0.9988	0.9988	1.0139	0.9944	1.0206	0.9912	1.0267	0.9886	1.0338	0.9855	1.0403	0.9825	1.0468	0.9793	1.0533	0.9763	1.0590	0.9731	1.0648	0.9699	1.0698
0.013	0.9987	0.9987	1.0138	0.9943	1.0205	0.9911	1.0266	0.9885	1.0337	0.9854	1.0402	0.9824	1.0467	0.9792	1.0532	0.9762	1.0589	0.9730	1.0647	0.9698	1.0697
0.014	0.9986	0.9986	1.0137	0.9942	1.0204	0.9910	1.0265	0.9884	1.0336	0.9853	1.0401	0.9823	1.0466	0.9791	1.0531	0.9761	1.0588	0.9729	1.0646	0.9697	1.0696
0.015	0.9985	0.9985	1.0136	0.9941	1.0203	0.9909	1.0264	0.9883	1.0335	0.9852	1.0400	0.9822	1.0465	0.9790	1.0530	0.9760	1.0587	0.9728	1.0645	0.9696	1.0695
0.016	0.9984	0.9984	1.0135	0.9940	1.0202	0.9908	1.0263	0.9882	1.0334	0.9851	1.0399	0.9821	1.0464	0.9789	1.0529	0.9759	1.0586	0.9727	1.0644	0.9695	1.0694
0.017	0.9983	0.9983	1.0134	0.9939	1.0201	0.9907	1.0262	0.9881	1.0333	0.9850	1.0398	0.9820	1.0463	0.9788	1.0528	0.9758	1.0585	0.9726	1.0643	0.9694	1.0693
0.018	0.9982	0.9982	1.0133	0.9938	1.0200	0.9906	1.0261	0.9880	1.0332	0.9849	1.0397	0.9819	1.0462	0.9787	1.0527	0.9757	1.0584	0.9725	1.0642	0.9693	1.0692
0.019	0.9981	0.9981	1.0132	0.9937	1.0199	0.9905	1.0260	0.9879	1.0331	0.9848	1.0396	0.9818	1.0461	0.9786	1.0526	0.9756	1.0583	0.9724	1.0641	0.9692	1.0691
0.020	0.9980	0.9980	1.0131	0.9936	1.0198	0.9904	1.0259	0.9878	1.0330	0.9847	1.0395	0.9817	1.0460	0.9785	1.0525	0.9755	1.0582	0.9723	1.0640	0.9691	1.0690
0.021	0.9979	0.9979	1.0130	0.9935	1.0197	0.9903	1.0258	0.9877	1.0329	0.9846	1.0394	0.9816	1.0459	0.9784	1.0524	0.9754	1.0581	0.9722	1.0639	0.9690	1.0689
0.022	0.9978	0.9978	1.0129	0.9934	1.0196	0.9902	1.0257	0.9876	1.0328	0.9845	1.0393	0.9815	1.0458	0.9783	1.0523	0.9753	1.0580	0.9721	1.0638	0.9689	1.0688
0.023	0.9977	0.9977	1.0128	0.9933	1.0195	0.9901	1.0256	0.9875	1.0327	0.9844	1.0392	0.9814	1.0457	0.9782	1.0522	0.9752	1.0579	0.9720	1.0637	0.9688	1.0687
0.024	0.9976	0.9976	1.0127	0.9932	1.0194	0.9900	1.0255	0.9874	1.0326	0.9843	1.0391	0.9813	1.0456	0.9781	1.0521	0.9751	1.0578	0.9719	1.0636	0.9687	1.0686
0.025	0.9975	0.9975	1.0126	0.9931	1.0193	0.9899	1.0254	0.9873	1.0325	0.9842	1.0390	0.9812	1.0455	0.9780	1.0520	0.9750	1.0577	0.9718	1.0635	0.9686	1.0685
0.026	0.9974	0.9974	1.0125	0.9930	1.0192	0.9898	1.0253	0.9872	1.0324	0.9841	1.0389	0.9811	1.0454	0.9779	1.0519	0.9749	1.0576	0.9717	1.0634	0.9685	1.0684
0.027	0.9973	0.9973	1.0124	0.9929	1.0191	0.9897	1.0252	0.9871	1.0323	0.9840	1.0388	0.9810	1.0453	0.9778	1.0518	0.9748	1.0575	0.9716	1.0633	0.9684	1.0683
0.028	0.9972	0.9972	1.0123	0.9928	1.0190	0.9896	1.0251	0.9870	1.0322	0.9839	1.0387	0.9809	1.0452	0.9777	1.0517	0.9747	1.0574	0.9715	1.0632	0.9683	1.0682
0.029	0.9971	0.9971	1.0122	0.9927	1.0189	0.9895	1.0250	0.9869	1.0321	0.9838	1.0386	0.9808	1.0451	0.9776	1.0516	0.9746	1.0573	0.9714	1.0631	0.9682	1.0681
0.030	0.9970	0.9970	1.0121	0.9926	1.0188	0.9894	1.0249	0.9868	1.0320	0.9837	1.0385	0.9807	1.0450	0.9775	1.0515	0.9745	1.0572	0.9713	1.0630	0.9681	1.0680
0.031	0.9969	0.9969	1.0120	0.9925	1.0187	0.9893	1.0248	0.9867	1.0319	0.9836	1.0384	0.9806	1.0449	0.9774	1.0514	0.9744	1.0571	0.9712	1.0629	0.9680	1.0679
0.032	0.9968	0.9968	1.0119	0.9924	1.0186	0.9892	1.0247	0.9866	1.0318	0.9835	1.0383	0.9805	1.0448	0.9773	1.0513	0.9743	1.0570	0.9711	1.0628	0.9679	1.0678
0.033	0.9967	0.9967	1.0118	0.9923	1.0185	0.9891	1.0246	0.9865	1.0317	0.9834	1.0382	0.9804	1.0447	0.9772	1.0512	0.9742	1.0569	0.9710	1.0627	0.9678	1.0677
0.034	0.9966	0.9966	1.0117	0.9922	1.0184	0.9890	1.0245	0.9864	1.0316	0.9833	1.0381	0.9803	1.0446	0.9771	1.0511	0.9741	1.0568	0.9709	1.0626	0.9677	1.0676
0.035	0.9965	0.9965	1.0116	0.9921	1.0183	0.9889	1.0244	0.9863	1.0315	0.9832	1.0380	0.9802	1.0445	0.9770	1.0510	0.9740	1.0567	0.9708	1.0625	0.9676	1.0675
0.036	0.9964	0.9964	1.0115	0.9920	1.0182	0.9888	1.0243	0.9862	1.0314	0.9831	1.0379	0.9801	1.0444	0.9769	1.0509	0.9739	1.0566	0.9707	1.0624	0.9675	1.0674
0.037	0.9963	0.9963	1.0114	0.9919	1.0181	0.9887	1.0242	0.9861	1.0313	0.9830	1.0378	0.9800	1.0443	0.9768	1.0508	0.9738	1.0565	0.9706	1.0623	0.9674	1.0673
0.038	0.9962	0.9962	1.0113	0.9918	1.0180	0.9886	1.0241	0.9860	1.0312	0.9829	1.0377	0.9799	1.0442	0.9767	1.0507	0.9737	1.0564	0.9705	1.0622	0.9673	1.0672
0.039	0.9961	0.9961	1.0112	0.9917	1.0179	0.9885	1.0240	0.9859	1.0311	0.9828	1.0376	0.9798	1.0441	0.9766	1.0506	0.9736	1.0563	0.9704	1.0621	0.9672	1.0671
0.040	0.9960	0.9960	1.0111	0.9916	1.0178	0.9884	1.0239	0.9858	1.0310	0.9827	1.0375	0.9797	1.0440	0.9765	1.0505	0.9735	1.0562	0.9703</td			

TABLE B-V. -- CONTINUED

$$(c) 0.XX \leq \frac{x_{II}-x_0}{\Delta x} \leq 19.XX \text{ where } 20 \leq XX \leq 29$$

$\frac{x_{II}-x_0}{\Delta x}$	20		21		22		23		24		25		26		27		28		29	
	J_{n0}	J_{n0}^*																		
0.XX	1.7918	0.6406	1.7113	0.6382	1.7130	0.6397	1.6967	0.6144	1.6822	0.6079	1.6998	0.6076	1.7768	0.5977	1.5483	0.5019	1.3159	0.2743	1.4905	0.5078
1.	.7051	.6726	.6884	.5911	.5959	.5956	.5914	.5857	.5953	.5823	.5943	.5856	.5854	.5773	.5610	.5739	.5297	.5297	.5297	.5297
2.	.3747	.1777	.3732	.1751	.3719	.1744	.3703	.1738	.3691	.1723	.3577	.1726	.3564	.1720	.3550	.1724	.3537	.1708	.3623	.1703
3.	.2712	.1956	.2712	.1952	.2703	.1951	.2697	.1958	.2688	.1959	.2683	.1958	.2673	.1956	.2663	.1953	.2661	.1952	.2654	.1958
4.	.2036	.1030	.2131	.1036	.2127	.1036	.2123	.1038	.2118	.1021	.2113	.1029	.2107	.1017	.2104	.1015	.2100	.1013	.2093	.1011
5.	.1179	.0854	.1176	.0852	.1173	.0851	.1170	.0847	.1174	.0848	.1174	.0846	.1163	.0842	.1177	.0844	.1174	.0842	.1171	.0841
6.	.1143	.0729	.1143	.0738	.1151	.0727	.1149	.0746	.1152	.0752	.1145	.0744	.1142	.0733	.1140	.0728	.1140	.0721	.1142	.0720
7.	.1101	.0636	.1109	.0633	.1107	.0635	.1097	.0634	.1104	.0633	.1098	.0632	.1090	.0631	.1087	.0631	.1087	.0630	.1085	.0630
8.	.1121	.0564	.1119	.0564	.1118	.0563	.1117	.0564	.1115	.0568	.1114	.0561	.1113	.0560	.1110	.0560	.1109	.0559	.1109	.0558
9.	.1032	.0507	.1031	.0506	.1030	.0506	.1029	.0506	.1028	.0505	.1027	.0504	.1025	.0503	.1024	.0503	.1023	.0503	.1022	.0503
10.	.0935	.0460	.0934	.0460	.0936	.0460	.0935	.0460	.0934	.0459	.0933	.0459	.0931	.0459	.0930	.0458	.0928	.0457	.0927	.0457
11.	.0858	.0423	.0853	.0421	.0854	.0420	.0853	.0420	.0852	.0420	.0851	.0419	.0850	.0419	.0849	.0419	.0848	.0419	.0848	.0419
12.	.0788	.0369	.0788	.0368	.0787	.0368	.0786	.0368	.0785	.0368	.0784	.0367	.0783	.0367	.0782	.0367	.0781	.0366	.0780	.0366
13.	.0730	.0361	.0730	.0360	.0729	.0360	.0728	.0360	.0728	.0360	.0727	.0359	.0727	.0359	.0726	.0358	.0725	.0357	.0725	.0356
14.	.0681	.0336	.0680	.0336	.0680	.0336	.0679	.0336	.0678	.0336	.0678	.0335	.0678	.0335	.0677	.0335	.0677	.0335	.0676	.0335
15.	.0631	.0315	.0637	.0315	.0636	.0313	.0635	.0315	.0636	.0314	.0635	.0314	.0635	.0314	.0634	.0314	.0634	.0314	.0634	.0313
16.	.0599	.0297	.0599	.0296	.0598	.0296	.0598	.0296	.0598	.0296	.0597	.0295	.0597	.0295	.0596	.0295	.0595	.0295	.0595	.0295
17.	.0565	.0280	.0565	.0280	.0564	.0280	.0564	.0280	.0564	.0280	.0564	.0279	.0563	.0279	.0562	.0278	.0562	.0278	.0562	.0278
18.	.0535	.0269	.0535	.0269	.0534	.0269	.0534	.0269	.0534	.0269	.0533	.0269	.0533	.0269	.0533	.0268	.0533	.0268	.0533	.0268
19.	.0508	.0254	.0507	.0254	.0507	.0254	.0507	.0254	.0507	.0254	.0506	.0254	.0506	.0254	.0506	.0253	.0506	.0253	.0506	.0253

TABLE B-V. -- CONTINUED

$$(d) 0.XX \leq \frac{x_{II}-x_0}{\Delta x} \leq 19.XX \text{ where } 30 \leq XX \leq 39$$

$\frac{x_{II}-x_0}{\Delta x}$	30		31		32		33		34		35		36		37		38		39	
	J_{n0}	J_{n0}^*																		
0.XX	1.4663	0.5601	1.4418	0.5330	1.4472	0.5369	1.4567	0.5366	1.4598	0.5400	1.4715	0.5337	1.4349	0.5275	1.4361	0.5219	1.3909	0.5187	1.4709	0.5063
1.	.7050	.5933	.5922	.5922	.5921	.5921	.5920	.5920	.5920	.5920	.5919	.5919	.5918	.5918	.5917	.5917	.5916	.5916	.5915	.5915
2.	.3610	.1597	.3597	.1591	.3596	.1588	.3595	.1587	.3594	.1586	.3593	.1585	.3592	.1584	.3591	.1583	.3590	.1582	.3589	.1581
3.	.2607	.1029	.2607	.1027	.2608	.1029	.2605	.1027	.2607	.1028	.2604	.1027	.2603	.1026	.2602	.1025	.2601	.1024	.2600	.1023
4.	.2093	.0909	.2097	.0907	.2098	.0905	.2096	.0904	.2097	.0905	.2095	.0904	.2094	.0903	.2093	.0902	.2092	.0901	.2091	.0900
5.	.1728	.0859	.1729	.0858	.1728	.0857	.1729	.0857	.1728	.0857	.1727	.0856	.1727	.0855	.1726	.0854	.1726	.0853	.1725	.0852
6.	.1473	.0712	.1471	.0712	.1469	.0711	.1467	.0711	.1465	.0712	.1463	.0713	.1463	.0713	.1462	.0713	.1461	.0712	.1460	.0711
7.	.1384	.0628	.1382	.0627	.1381	.0627	.1380	.0626	.1381	.0626	.1379	.0625	.1378	.0625	.1377	.0624	.1376	.0623	.1375	.0622
8.	.1138	.0598	.1136	.0597	.1135	.0597	.1134	.0596	.1135	.0596	.1134	.0595	.1133	.0595	.1132	.0594	.1131	.0593	.1130	.0592
9.	.1021	.0508	.1020	.0508	.1019	.0507	.1018	.0507	.1017	.0507	.1016	.0506	.1015	.0506	.1014	.0505	.1013	.0504	.1012	.0503
10.	.0927	.0436	.0926	.0436	.0925	.0435	.0924	.0434	.0923	.0434	.0922	.0434	.0921	.0434	.0920	.0433	.0919	.0433	.0918	.0433
11.	.0848	.0418	.0847	.0417	.0847	.0417	.0846	.0417	.0847	.0417	.0846	.0417	.0845	.0416	.0844	.0416	.0843	.0415	.0842	.0415
12.	.0768	.0366	.0761	.0365	.0760	.0365	.0759	.0365	.0759	.0365	.0759	.0365	.0758	.0365	.0757	.0365	.0757	.0365	.0756	.0365
13.	.0725	.0258	.0724	.0258	.0724	.0258	.0723	.0257	.0723	.0257	.0722	.0257	.0722	.0257	.0721	.0257	.0721	.0256	.0720	.0256
14.	.0725	.0234	.0725	.0234	.0725	.0234	.0725	.0234	.0725	.0234	.0725	.0234	.0725	.0234	.0725	.0234	.0725	.0234	.0725	.0234
15.	.0633	.0213	.0633	.0213	.0632	.0213	.0632	.0213	.0632	.0213	.0632	.0213	.0632	.0213	.0631	.0213	.0631	.0213	.0631	.0213
16.	.0592	.0195	.0592	.0195	.0592	.0195	.0591	.0195	.0591	.0195	.0591	.0195	.0591	.0195	.0591	.0195	.0591	.0195	.0591	.0195
17.	.0582	.0186	.0582	.0186	.0582	.0186	.0581	.0186	.0581	.0186	.0581	.0186	.0581	.0186	.0580	.0186	.0580	.0186	.0580	.0186
18.	.0538	.0164	.0538	.0164	.0538	.0164	.0538	.0164	.0538	.0164	.0538	.0164	.0538	.0164	.0538	.0164	.0538	.0164	.0538	.0164
19.	.0505	.0091	.0505	.0091	.0505	.0091	.0505	.0091	.0505	.0091	.0505	.0091	.0505	.0091	.0505	.0091	.0505	.0091	.0505	.0091

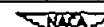


TABLE B-V. — CONTINUED

$$(e) \quad 0.XX \leq \frac{x_n - x_0}{\Delta x} \leq 19.XX \quad \text{where} \quad 40 \leq xx \leq 49$$

$\frac{x_n - x_0}{\Delta x}$	40		41		42		43		44		45		46		47		48		49	
	x_0	x_{40}																		
0.XX	1.2928	0.4989	1.2359	0.4986	1.2198	0.4984	1.2007	0.4983	1.1995	0.4983	1.1901	0.4982	1.1850	0.4987	1.1803	0.4981	1.1860	0.4985	1.1821	0.4980
1.	.5590	.3134	.5560	.3142	.5531	.3150	.5502	.3159	.5474	.3167	.5445	.3175	.5416	.3184	.5387	.3193	.5358	.3202	.5329	.3213
2.	.3449	.1641	.3471	.1652	.3492	.1660	.3447	.1665	.3433	.1671	.3403	.1679	.3371	.1689	.3339	.1694	.3308	.1700	.3276	.1703
3.	.2045	.0969	.2041	.0971	.2040	.0968	.2033	.0963	.2021	.0957	.2007	.0959	.2003	.0959	.2019	.0976	.2015	.0974	.2011	.0978
4.	.1699	.0893	.1695	.0897	.1693	.0893	.1690	.0893	.1687	.0890	.1686	.0891	.1686	.0887	.1679	.0876	.1676	.0873	.1673	.0873
5.	.1562	.0768	.1565	.0767	.1564	.0766	.1565	.0765	.1563	.0764	.1561	.0762	.1560	.0762	.1560	.0761	.1555	.0760	.1553	.0760
6.	.1503	.0690	.1506	.0690	.1504	.0691	.1503	.0691	.1501	.0691	.1500	.0692	.1500	.0694	.1500	.0694	.1503	.0694	.1504	.0694
7.	.1429	.0583	.1434	.0583	.1432	.0581	.1431	.0581	.1429	.0581	.1428	.0580	.1428	.0580	.1426	.0581	.1425	.0581	.1425	.0581
8.	.1379	.0497	.1381	.0497	.1380	.0496	.1380	.0496	.1379	.0496	.1378	.0496	.1378	.0496	.1377	.0496	.1376	.0496	.1375	.0496
9.	.1311	.0437	.1310	.0436	.1309	.0436	.1308	.0436	.1307	.0435	.1305	.0435	.1305	.0436	.1305	.0435	.1303	.0435	.1302	.0435
10.	.0918	.0422	.0917	.0424	.0916	.0421	.0915	.0421	.0914	.0419	.0913	.0418	.0912	.0418	.0911	.0418	.0910	.0418	.0909	.0418
11.	.0841	.0415	.0840	.0414	.0839	.0414	.0839	.0413	.0838	.0413	.0837	.0413	.0837	.0412	.0836	.0412	.0835	.0412	.0834	.0412
12.	.0776	.0383	.0775	.0385	.0774	.0382	.0773	.0382	.0773	.0381	.0772	.0381	.0771	.0381	.0771	.0380	.0770	.0380	.0769	.0380
13.	.0720	.0355	.0719	.0355	.0719	.0355	.0718	.0355	.0718	.0355	.0717	.0354	.0717	.0354	.0716	.0354	.0715	.0353	.0715	.0353
14.	.0671	.0332	.0671	.0332	.0670	.0331	.0670	.0331	.0670	.0331	.0669	.0331	.0669	.0331	.0668	.0330	.0668	.0330	.0667	.0330
15.	.0639	.0311	.0639	.0311	.0638	.0311	.0638	.0311	.0637	.0310	.0637	.0310	.0637	.0310	.0636	.0310	.0636	.0310	.0635	.0310
16.	.0598	.0293	.0598	.0293	.0598	.0293	.0598	.0293	.0598	.0293	.0598	.0293	.0598	.0293	.0597	.0293	.0597	.0293	.0596	.0293
17.	.0559	.0277	.0559	.0277	.0558	.0277	.0558	.0277	.0558	.0276	.0557	.0276	.0557	.0276	.0557	.0276	.0556	.0276	.0556	.0276
18.	.0529	.0261	.0529	.0261	.0528	.0261	.0528	.0261	.0528	.0260	.0527	.0260	.0527	.0260	.0527	.0260	.0527	.0260	.0526	.0260
19.XX	.0503	.0249	.0502	.0249	.0502	.0249	.0502	.0249	.0502	.0249	.0502	.0249	.0502	.0249	.0502	.0248	.0502	.0248	.0502	.0248

TABLE B-V.—CONTINUED

$$(f) \quad 0.XX \leq \frac{x_n - x_0}{\Delta x} \leq 19.XX \quad \text{where} \quad 50 \leq xx \leq 59$$

$\frac{x_n - x_0}{\Delta x}$	50		51		52		53		54		55		56		57		58		59	
	x_0	x_{50}																		
0.XX	1.0906	0.4507	1.0659	0.4454	1.0726	0.4429	1.0621	0.4381	1.0480	0.4341	1.0561	0.4301	1.0485	0.4263	1.0132	0.4225	1.0021	0.4186	0.9934	0.4151
1.	.5108	.3136	.5052	.3137	.5053	.3136	.5054	.3136	.5055	.3137	.5056	.3138	.5056	.3138	.5057	.3138	.5057	.3139	.5057	.3139
2.	.3349	.1768	.3323	.1758	.3342	.1776	.3331	.1775	.3320	.1768	.3309	.1758	.3298	.1748	.3275	.1738	.3256	.1728	.3237	.1718
3.	.2513	.1303	.2507	.1301	.2501	.1303	.2499	.1305	.2491	.1304	.2486	.1303	.2486	.1303	.2476	.1302	.2476	.1301	.2476	.1301
4.	.2007	.0970	.2003	.0968	.1999	.0966	.1993	.0964	.1991	.0963	.1987	.0961	.1987	.0960	.1987	.0957	.1973	.0953	.1971	.0953
5.	.1671	.0812	.1668	.0811	.1669	.0809	.1668	.0808	.1669	.0807	.1667	.0807	.1667	.0807	.1667	.0806	.1664	.0802	.1662	.0802
6.	.1421	.0668	.1429	.0671	.1427	.0667	.1426	.0666	.1425	.0665	.1423	.0665	.1422	.0664	.1422	.0663	.1421	.0661	.1420	.0660
7.	.1246	.0583	.1250	.0585	.1245	.0581	.1249	.0581	.1247	.0581	.1244	.0580	.1244	.0580	.1243	.0579	.1241	.0578	.1240	.0578
8.	.1118	.0494	.1111	.0494	.1115	.0494	.1109	.0494	.1107	.0494	.1104	.0493	.1104	.0493	.1102	.0492	.1101	.0491	.1101	.0491
9.	.1001	.0408	.1000	.0408	.0999	.0401	.0998	.0401	.0997	.0400	.0996	.0400	.0995	.0400	.0994	.0399	.0993	.0398	.0992	.0397
10.	.0920	.0345	.0909	.0347	.0908	.0347	.0907	.0347	.0906	.0346	.0905	.0346	.0905	.0346	.0904	.0346	.0903	.0345	.0902	.0344
11.	.0844	.0211	.0853	.0210	.0852	.0210	.0851	.0210	.0850	.0209	.0849	.0209	.0848	.0209	.0847	.0208	.0846	.0208	.0845	.0208
12.	.0770	.0160	.0769	.0160	.0768	.0161	.0768	.0161	.0767	.0161	.0767	.0161	.0767	.0161	.0766	.0161	.0765	.0161	.0764	.0161
13.	.0713	.0133	.0714	.0133	.0714	.0133	.0713	.0133	.0713	.0132	.0713	.0132	.0713	.0132	.0712	.0132	.0711	.0131	.0711	.0131
14.	.0667	.0110	.0666	.0110	.0666	.0109	.0666	.0109	.0665	.0109	.0665	.0109	.0665	.0109	.0664	.0108	.0663	.0108	.0662	.0108
15.	.0629	.0092	.0629	.0092	.0628	.0092	.0628	.0092	.0628	.0092	.0628	.0092	.0628	.0092	.0627	.0092	.0626	.0092	.0625	.0092
16.	.0598	.0091	.0598	.0091	.0598	.0091	.0597	.0091	.0597	.0091	.0597	.0091	.0597	.0091	.0596	.0091	.0596	.0091	.0595	.0091
17.	.0566	.0079	.0572	.0079	.0569	.0079	.0570	.0079	.0570	.0079	.0570	.0079	.0570	.0079	.0570	.0079	.0570	.0079	.0570	.0079
18.	.0536	.0061	.0536	.0061	.0536	.0061	.0536	.0061	.0536	.0061	.0536	.0061	.0536	.0061	.0536	.0061	.0536	.0061	.0536	.0061
19.XX	.0500	.0048	.0500	.0048	.0500	.0048	.0499	.0048	.0499	.0047	.0499	.0047	.0499	.0047	.0498	.0047	.0498	.0047	.0498	.0047

NACA

TABLE B-V. - CONTINUED

$$(g) \quad 0.XX \leq \frac{x_{II}-x_0}{\Delta x} \leq 19.XX \quad \text{where} \quad 60 \leq XX \leq 69$$

$\frac{x_{II}-x_0}{\Delta x}$	60		61		62		63		64		65		66		67		68		69	
	x_0	x_{II}																		
0.IX	0.9898	0.4315	0.9793	0.4080	0.9695	0.4043	0.9596	0.4001	0.9490	0.3978	0.9395	0.3949	0.9244	0.3912	0.9133	0.3891	0.9046	0.3869	0.8959	0.3846
1.	0.9893	0.4319	0.9791	0.4082	0.9697	0.4045	0.9598	0.4003	0.9492	0.3979	0.9397	0.3950	0.9245	0.3913	0.9138	0.3892	0.9047	0.3868	0.8958	0.3847
2.	0.9894	0.4319	0.9794	0.4084	0.9693	0.4047	0.9593	0.4005	0.9495	0.3980	0.9398	0.3951	0.9246	0.3914	0.9139	0.3893	0.9048	0.3869	0.8959	0.3848
3.	0.9895	0.4321	0.9795	0.4085	0.9695	0.4048	0.9595	0.4006	0.9497	0.3981	0.9399	0.3952	0.9247	0.3915	0.9140	0.3894	0.9049	0.3870	0.8960	0.3849
4.	0.9897	0.4321	0.9793	0.4080	0.9690	0.4042	0.9588	0.4002	0.9488	0.3974	0.9388	0.3944	0.9237	0.3904	0.9037	0.3887	0.8937	0.3857	0.8938	0.3847
5.	0.9893	0.4319	0.9790	0.4078	0.9686	0.4036	0.9583	0.4000	0.9483	0.3970	0.9383	0.3940	0.9234	0.3898	0.9034	0.3884	0.8934	0.3854	0.8935	0.3844
6.	0.9896	0.4320	0.9792	0.4079	0.9688	0.4037	0.9585	0.4001	0.9485	0.3971	0.9385	0.3941	0.9235	0.3899	0.9035	0.3885	0.8935	0.3855	0.8936	0.3845
7.	0.9896	0.4320	0.9795	0.4082	0.9692	0.4040	0.9588	0.4004	0.9488	0.3974	0.9388	0.3944	0.9237	0.3901	0.9037	0.3887	0.8937	0.3857	0.8938	0.3847
8.	0.9896	0.4320	0.9795	0.4082	0.9692	0.4040	0.9588	0.4004	0.9488	0.3974	0.9388	0.3944	0.9237	0.3901	0.9037	0.3887	0.8937	0.3857	0.8938	0.3847
9.	0.9892	0.4317	0.9790	0.4078	0.9686	0.4036	0.9583	0.4000	0.9483	0.3970	0.9383	0.3940	0.9234	0.3898	0.9034	0.3884	0.8934	0.3854	0.8935	0.3844
10.	0.9898	0.4319	0.9791	0.4081	0.9689	0.4039	0.9586	0.4003	0.9486	0.3973	0.9386	0.3943	0.9236	0.3903	0.9036	0.3886	0.8936	0.3856	0.8937	0.3846
11.	0.9897	0.4319	0.9796	0.4080	0.9688	0.4038	0.9585	0.4002	0.9485	0.3972	0.9385	0.3942	0.9235	0.3902	0.9035	0.3885	0.8935	0.3855	0.8936	0.3845
12.	0.9894	0.4317	0.9793	0.4077	0.9685	0.4035	0.9582	0.4001	0.9482	0.3970	0.9382	0.3940	0.9233	0.3900	0.9033	0.3883	0.8933	0.3853	0.8934	0.3843
13.	0.9895	0.4319	0.9795	0.4082	0.9690	0.4040	0.9588	0.4005	0.9488	0.3974	0.9388	0.3944	0.9237	0.3904	0.9037	0.3887	0.8937	0.3857	0.8938	0.3847
14.	0.9896	0.4320	0.9796	0.4083	0.9691	0.4041	0.9589	0.4006	0.9489	0.3975	0.9389	0.3945	0.9238	0.3905	0.9038	0.3888	0.8938	0.3858	0.8939	0.3848
15.	0.9896	0.4320	0.9796	0.4083	0.9691	0.4041	0.9589	0.4006	0.9489	0.3975	0.9389	0.3945	0.9238	0.3905	0.9038	0.3888	0.8938	0.3858	0.8939	0.3848
16.	0.9896	0.4320	0.9796	0.4083	0.9691	0.4041	0.9589	0.4006	0.9489	0.3975	0.9389	0.3945	0.9238	0.3905	0.9038	0.3888	0.8938	0.3858	0.8939	0.3848
17.	0.9896	0.4320	0.9796	0.4083	0.9691	0.4041	0.9589	0.4006	0.9489	0.3975	0.9389	0.3945	0.9238	0.3905	0.9038	0.3888	0.8938	0.3858	0.8939	0.3848
18.	0.9896	0.4320	0.9796	0.4083	0.9691	0.4041	0.9589	0.4006	0.9489	0.3975	0.9389	0.3945	0.9238	0.3905	0.9038	0.3888	0.8938	0.3858	0.8939	0.3848
19.IX	0.9898	0.4317	0.9797	0.4077	0.9687	0.4037	0.9587	0.4001	0.9487	0.3971	0.9387	0.3941	0.9237	0.3901	0.9037	0.3887	0.8937	0.3857	0.8938	0.3847

TABLE B-V. - CONTINUED

$$(h) \quad 0.XX \leq \frac{x_{II}-x_0}{\Delta x} \leq 19.XX \quad \text{where} \quad 70 \leq XX \leq 79$$

$\frac{x_{II}-x_0}{\Delta x}$	70		71		72		73		74		75		76		77		78		79	
	x_0	x_{II}																		
0.IX	0.9873	0.3789	0.9790	0.3772	0.9793	0.3780	0.9693	0.3770	0.9590	0.3760	0.9493	0.3753	0.9390	0.3749	0.9298	0.3742	0.9191	0.3731	0.9094	0.3726
1.	0.9868	0.3739	0.9781	0.3726	0.9683	0.3717	0.9582	0.3706	0.9481	0.3699	0.9380	0.3690	0.9281	0.3682	0.9181	0.3672	0.9082	0.3663	0.8966	0.3656
2.	0.9864	0.3739	0.9781	0.3726	0.9683	0.3717	0.9581	0.3706	0.9481	0.3699	0.9380	0.3690	0.9281	0.3682	0.9181	0.3672	0.9082	0.3663	0.8966	0.3656
3.	0.9869	0.3743	0.9785	0.3731	0.9687	0.3724	0.9585	0.3713	0.9485	0.3703	0.9385	0.3703	0.9285	0.3693	0.9185	0.3685	0.9085	0.3675	0.8965	0.3668
4.	0.9869	0.3743	0.9785	0.3731	0.9687	0.3724	0.9585	0.3713	0.9485	0.3703	0.9385	0.3703	0.9285	0.3693	0.9185	0.3685	0.9085	0.3675	0.8965	0.3668
5.	0.9866	0.3740	0.9785	0.3731	0.9687	0.3724	0.9585	0.3713	0.9485	0.3703	0.9385	0.3703	0.9285	0.3693	0.9185	0.3685	0.9085	0.3675	0.8965	0.3668
6.	0.9866	0.3740	0.9785	0.3731	0.9687	0.3724	0.9585	0.3713	0.9485	0.3703	0.9385	0.3703	0.9285	0.3693	0.9185	0.3685	0.9085	0.3675	0.8965	0.3668
7.	0.9861	0.3736	0.9780	0.3724	0.9682	0.3714	0.9578	0.3704	0.9478	0.3694	0.9378	0.3684	0.9278	0.3674	0.9178	0.3664	0.9078	0.3654	0.8958	0.3647
8.	0.9868	0.3734	0.9783	0.3721	0.9685	0.3712	0.9581	0.3701	0.9481	0.3690	0.9381	0.3680	0.9281	0.3671	0.9181	0.3661	0.9081	0.3651	0.8961	0.3644
9.	0.9861	0.3734	0.9783	0.3721	0.9685	0.3712	0.9581	0.3701	0.9481	0.3690	0.9381	0.3680	0.9281	0.3671	0.9181	0.3661	0.9081	0.3651	0.8961	0.3644
10.	0.9863	0.3734	0.9783	0.3721	0.9685	0.3712	0.9581	0.3701	0.9481	0.3690	0.9381	0.3680	0.9281	0.3671	0.9181	0.3661	0.9081	0.3651	0.8961	0.3644
11.	0.9860	0.3734	0.9783	0.3721	0.9685	0.3712	0.9581	0.3701	0.9481	0.3690	0.9381	0.3680	0.9281	0.3671	0.9181	0.3661	0.9081	0.3651	0.8961	0.3644
12.	0.9858	0.3734	0.9783	0.3721	0.9685	0.3712	0.9581	0.3701	0.9481	0.3690	0.9381	0.3680	0.9281	0.3671	0.9181	0.3661	0.9081	0.3651	0.8961	0.3644
13.	0.9859	0.3734	0.9784	0.3721	0.9686	0.3712	0.9582	0.3701	0.9482	0.3691	0.9382	0.3681	0.9282	0.3672	0.9182	0.3662	0.9082	0.3652	0.8962	0.3645
14.	0.9859	0.3734	0.9784	0.3721	0.9686	0.3712	0.9582	0.3701	0.9482	0.3691	0.9382	0.3681	0.9282	0.3672	0.9182	0.3662	0.9082	0.3652	0.8962	0.3645
15.	0.9857	0.3734	0.9784	0.3721	0.9686	0.3712	0.9582	0.3701	0.9482	0.3691	0.9382	0.3681	0.9282	0.3672	0.9182	0.3662	0.9082	0.3652	0.8962	0.3645
16.	0.9856	0.3734	0.9784	0.3721	0.9686	0.3712	0.9582	0.3701	0.9482	0.3691	0.9382	0.3681	0.9282	0.3672	0.9182	0.3662	0.9082	0.3652	0.8962	0.3645
17.	0.9856	0.3734	0.9784	0.3721	0.9686	0.3712	0.9582	0.3701	0.9482	0.3691	0.9382	0.3681	0.9282	0.3672	0.9182	0.3662	0.9082	0.3652	0.8962	0.3645
18.	0.9856	0.3734	0.9784	0.3721	0.968															

TABLE B-V. - CONTINUED

$$(i) 0.XX \leq \frac{x_n - x_0}{\Delta x} \leq 19.XX \text{ where } 80 \leq XX \leq 89$$

$\frac{x_n - x_0}{\Delta x}$	80		81		82		83		84		85		86		87		88		89	
	x_0	x_{n0}^*																		
0.XX	0.8109	0.3513	0.8041	0.3487	0.7973	0.3462	0.7906	0.3438	0.7841	0.3413	0.7777	0.3389	0.7714	0.3366	0.7652	0.3313	0.7591	0.3280	0.7511	0.3257
1.	0.8118	0.3517	0.8049	0.3493	0.7979	0.3469	0.7920	0.3440	0.7840	0.3414	0.7771	0.3395	0.7710	0.3374	0.7658	0.3321	0.7580	0.3287	0.7516	0.3254
2.	0.8054	0.3449	0.8044	0.3445	0.7953	0.3411	0.7865	0.3387	0.7737	0.3343	0.7688	0.3308	0.7628	0.3284	0.7568	0.3248	0.7503	0.3203	0.7447	0.3174
3.	0.8135	0.3523	0.8053	0.3491	0.7980	0.3478	0.7958	0.3450	0.7878	0.3425	0.7818	0.3398	0.7751	0.3366	0.7683	0.3323	0.7603	0.3263	0.7538	0.3238
4.	0.8058	0.3507	0.8059	0.3485	0.7989	0.3472	0.7968	0.3455	0.7881	0.3428	0.7821	0.3391	0.7754	0.3369	0.7686	0.3326	0.7603	0.3263	0.7538	0.3238
5.	0.8063	0.3501	0.8059	0.3485	0.7989	0.3472	0.7968	0.3455	0.7881	0.3428	0.7821	0.3391	0.7754	0.3369	0.7686	0.3326	0.7603	0.3263	0.7538	0.3238
6.	0.8076	0.3528	0.8073	0.3474	0.7988	0.3471	0.7971	0.3473	0.7973	0.3437	0.7868	0.3393	0.7756	0.3371	0.7696	0.3337	0.7653	0.3293	0.7568	0.3268
7.	0.8078	0.3528	0.8073	0.3474	0.7988	0.3471	0.7971	0.3473	0.7973	0.3437	0.7868	0.3393	0.7756	0.3371	0.7696	0.3337	0.7653	0.3293	0.7568	0.3268
8.	0.8079	0.3528	0.8073	0.3474	0.7988	0.3471	0.7971	0.3473	0.7973	0.3437	0.7868	0.3393	0.7756	0.3371	0.7696	0.3337	0.7653	0.3293	0.7568	0.3268
9.	0.8079	0.3528	0.8073	0.3474	0.7988	0.3471	0.7971	0.3473	0.7973	0.3437	0.7868	0.3393	0.7756	0.3371	0.7696	0.3337	0.7653	0.3293	0.7568	0.3268
10.	0.8079	0.3528	0.8073	0.3474	0.7988	0.3471	0.7971	0.3473	0.7973	0.3437	0.7868	0.3393	0.7756	0.3371	0.7696	0.3337	0.7653	0.3293	0.7568	0.3268
11.	0.8081	0.3501	0.8013	0.3401	0.8013	0.3401	0.8011	0.3401	0.8011	0.3401	0.8011	0.3401	0.8011	0.3401	0.8011	0.3401	0.8011	0.3401	0.8011	0.3401
12.	0.8082	0.3517	0.8016	0.3401	0.8017	0.3401	0.8011	0.3401	0.8017	0.3401	0.8016	0.3401	0.8016	0.3401	0.8016	0.3401	0.8016	0.3401	0.8016	0.3401
13.	0.8090	0.3516	0.8059	0.3443	0.8049	0.3443	0.8048	0.3443	0.8049	0.3443	0.8048	0.3443	0.8049	0.3443	0.8048	0.3443	0.8048	0.3443	0.8048	0.3443
14.	0.8094	0.3523	0.8053	0.3443	0.8049	0.3443	0.8048	0.3443	0.8049	0.3443	0.8048	0.3443	0.8049	0.3443	0.8048	0.3443	0.8048	0.3443	0.8048	0.3443
15.	0.8094	0.3523	0.8053	0.3443	0.8049	0.3443	0.8048	0.3443	0.8049	0.3443	0.8048	0.3443	0.8049	0.3443	0.8048	0.3443	0.8048	0.3443	0.8048	0.3443
16.	0.8094	0.3523	0.8053	0.3443	0.8049	0.3443	0.8048	0.3443	0.8049	0.3443	0.8048	0.3443	0.8049	0.3443	0.8048	0.3443	0.8048	0.3443	0.8048	0.3443
17.	0.8094	0.3523	0.8053	0.3443	0.8049	0.3443	0.8048	0.3443	0.8049	0.3443	0.8048	0.3443	0.8049	0.3443	0.8048	0.3443	0.8048	0.3443	0.8048	0.3443
18.	0.8094	0.3523	0.8053	0.3443	0.8049	0.3443	0.8048	0.3443	0.8049	0.3443	0.8048	0.3443	0.8049	0.3443	0.8048	0.3443	0.8048	0.3443	0.8048	0.3443
19.	0.8093	0.3523	0.8053	0.3443	0.8049	0.3443	0.8048	0.3443	0.8049	0.3443	0.8048	0.3443	0.8049	0.3443	0.8048	0.3443	0.8048	0.3443	0.8048	0.3443

TABLE B-V. - CONCLUDED

$$(j) 0.XX \leq \frac{x_n - x_0}{\Delta x} \leq 19.XX \text{ where } 90 \leq XX \leq 99$$

$\frac{x_n - x_0}{\Delta x}$	90		91		92		93		94		95		96		97		98		99	
	x_0	x_{n0}^*																		
0.XX	0.7472	0.3273	0.7424	0.3253	0.7327	0.3231	0.7301	0.3210	0.7243	0.3189	0.7191	0.3168	0.7138	0.3148	0.7085	0.3188	0.7031	0.3106	0.6988	0.3088
1.	0.8029	0.3626	0.8011	0.3598	0.8029	0.3563	0.8011	0.3535	0.8011	0.3507	0.8011	0.3475	0.8011	0.3447	0.8011	0.3418	0.8011	0.3388	0.8011	0.3358
2.	0.8098	0.3503	0.8054	0.3484	0.8054	0.3461	0.8054	0.3443	0.8054	0.3421	0.8054	0.3401	0.8054	0.3381	0.8054	0.3361	0.8054	0.3341	0.8054	0.3321
3.	0.8028	0.3698	0.8027	0.3665	0.8027	0.3634	0.8027	0.3603	0.8027	0.3571	0.8027	0.3541	0.8027	0.3511	0.8027	0.3481	0.8027	0.3451	0.8027	0.3421
4.	0.8027	0.3698	0.8027	0.3665	0.8027	0.3634	0.8027	0.3603	0.8027	0.3571	0.8027	0.3541	0.8027	0.3511	0.8027	0.3481	0.8027	0.3451	0.8027	0.3421
5.	0.8027	0.3698	0.8027	0.3665	0.8027	0.3634	0.8027	0.3603	0.8027	0.3571	0.8027	0.3541	0.8027	0.3511	0.8027	0.3481	0.8027	0.3451	0.8027	0.3421
6.	0.8027	0.3698	0.8027	0.3665	0.8027	0.3634	0.8027	0.3603	0.8027	0.3571	0.8027	0.3541	0.8027	0.3511	0.8027	0.3481	0.8027	0.3451	0.8027	0.3421
7.	0.8027	0.3698	0.8027	0.3665	0.8027	0.3634	0.8027	0.3603	0.8027	0.3571	0.8027	0.3541	0.8027	0.3511	0.8027	0.3481	0.8027	0.3451	0.8027	0.3421
8.	0.8027	0.3698	0.8027	0.3665	0.8027	0.3634	0.8027	0.3603	0.8027	0.3571	0.8027	0.3541	0.8027	0.3511	0.8027	0.3481	0.8027	0.3451	0.8027	0.3421
9.	0.8027	0.3698	0.8027	0.3665	0.8027	0.3634	0.8027	0.3603	0.8027	0.3571	0.8027	0.3541	0.8027	0.3511	0.8027	0.3481	0.8027	0.3451	0.8027	0.3421
10.	0.8076	0.3473	0.8077	0.3453	0.8076	0.3433	0.8076	0.3413	0.8076	0.3393	0.8076	0.3373	0.8076	0.3353	0.8076	0.3333	0.8076	0.3313	0.8076	0.3293
11.	0.8077	0.3498	0.8066	0.3478	0.8066	0.3456	0.8066	0.3436	0.8066	0.3416	0.8066	0.3396	0.8066	0.3376	0.8066	0.3356	0.8066	0.3336	0.8066	0.3316
12.	0.8077	0.3498	0.8066	0.3478	0.8066	0.3456	0.8066	0.3436	0.8066	0.3416	0.8066	0.3396	0.8066	0.3376	0.8066	0.3356	0.8066	0.3336	0.8066	0.3316
13.	0.8077	0.3498	0.8066	0.3478	0.8066	0.3456	0.8066	0.3436	0.8066	0.3416	0.8066	0.3396	0.8066	0.3376	0.8066	0.3356	0.8066	0.3336	0.8066	0.3316
14.	0.8077	0.3498	0.8066	0.3478	0.8066	0.3456	0.8066	0.3436	0.8066	0.3416	0.8066	0.3396	0.8066	0.3376	0.8066	0.3356	0.8066	0.3336	0.8066	0.3316
15.	0.8077	0.3498	0.8066	0.3478	0.8066	0.3456	0.8066	0.3436	0.8066	0.3416	0.8066	0.3396	0.8066	0.3376	0.8066	0.3356	0.8066	0.3336	0.8066	0.3316
16.	0.8077	0.3498	0.8066	0.3478	0.8066	0.3456	0.8066	0.3436	0.8066	0.3416	0.8066	0.3396	0.8066	0.3376	0.8066	0.3356	0.8066	0.3336	0.8066	0.3316
17.	0.8077	0.3498	0.8066	0.3478	0.8066	0.3456	0.8066	0.3436	0.8066	0.3416	0.8066	0.3396	0.8066							

TABLE B-VI.— VALUES OF j_{no} AND j_{no}^* USED IN EVALUATING EQUATION (26)

$$20.0 \leq \frac{x_{H+} - x_0}{\Delta x} \leq 39.9$$

$\frac{x_{H+} - x_0}{\Delta x}$	0	1	2	3	4	5	6	7	8	9
	j_{no}	j_{no}^*								
20.1	0.0488	0.0442	0.0486	0.0441	0.0483	0.0441	0.0481	0.0439	0.0478	0.0437
21.	.0469	.0431	.0463	.0430	.0461	.0429	.0459	.0427	.0457	.0426
22.	.0444	.0421	.0443	.0420	.0441	.0419	.0439	.0418	.0437	.0435
23.	.0426	.0411	.0424	.0410	.0422	.0410	.0420	.0409	.0418	.0408
24.	.0408	.0403	.0407	.0402	.0405	.0401	.0403	.0400	.0409	.0402
25.	.0392	.0393	.0391	.0394	.0389	.0393	.0388	.0392	.0386	.0385
26.	.0377	.0387	.0376	.0387	.0375	.0386	.0373	.0387	.0372	.0385
27.	.0364	.0381	.0362	.0380	.0361	.0379	.0360	.0379	.0358	.0378
28.	.0351	.0373	.0350	.0374	.0348	.0373	.0347	.0373	.0346	.0345
29.	.0339	.0368	.0338	.0368	.0337	.0367	.0336	.0367	.0334	.0333
30.	.0328	.0363	.0347	.0362	.0326	.0362	.0325	.0361	.0324	.0321
31.	.0317	.0358	.0316	.0357	.0315	.0357	.0315	.0356	.0314	.0313
32.	.0306	.0353	.0307	.0352	.0306	.0352	.0305	.0351	.0304	.0351
33.	.0299	.0349	.0298	.0348	.0297	.0348	.0296	.0347	.0295	.0347
34.	.0290	.0344	.0289	.0344	.0288	.0343	.0287	.0343	.0286	.0343
35.	.0282	.0341	.0281	.0340	.0280	.0339	.0279	.0339	.0279	.0338
36.	.0274	.0336	.0273	.0336	.0273	.0336	.0272	.0335	.0271	.0334
37.	.0267	.0333	.0266	.0332	.0265	.0332	.0265	.0332	.0264	.0331
38.	.0260	.0329	.0259	.0329	.0258	.0329	.0258	.0327	.0257	.0325
39.1	.0253	.0326	.0253	.0326	.0252	.0326	.0251	.0325	.0251	.0324

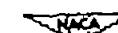


TABLE B-VII.— VALUES OF j_{no} AND j_{no}^* USED IN EVALUATING EQUATION (26)

$$40.0 \leq \frac{x_n - x_o}{\Delta x} \leq 89.5$$

$\frac{x_n - x_o}{\Delta x}$	4x.0		4x.5		5x.0		5x.5		6x.0		6x.5		7x.0		7x.5		8x.0		8x.5	
X	j_{no}	j_{no}^*																		
0	0.0247	0.0123	0.0244	0.0122	0.0198	0.0099	0.0196	0.0097	0.0165	0.0082	0.0164	0.0082	0.0142	0.0071	0.0141	0.0071	0.0134	0.0062	0.0123	0.0061
1	.0241	.0120	.0238	.0118	.0194	.0097	.0192	.0096	.0163	.0081	.0161	.0081	.0140	.0069	.0139	.0069	.0123	.0061	.0122	.0061
2	.0235	.0117	.0233	.0116	.0190	.0095	.0189	.0094	.0160	.0080	.0159	.0079	.0138	.0068	.0137	.0068	.0121	.0061	.0120	.0060
3	.0230	.0114	.0227	.0113	.0184	.0091	.0182	.0090	.0155	.0077	.0154	.0077	.0134	.0066	.0133	.0066	.0118	.0059	.0119	.0059
4	.0225	.0112	.0222	.0110	.0180	.0089	.0179	.0089	.0153	.0076	.0152	.0075	.0132	.0066	.0132	.0066	.0117	.0058	.0116	.0058
5	.0220	.0109	.0217	.0108	.0177	.0089	.0175	.0088	.0150	.0075	.0149	.0074	.0131	.0065	.0130	.0065	.0116	.0058	.0115	.0058
6	.0215	.0107	.0213	.0106	.0177	.0089	.0172	.0087	.0148	.0074	.0147	.0073	.0129	.0064	.0128	.0064	.0114	.0057	.0114	.0056
7	.0211	.0105	.0208	.0105	.0174	.0087	.0172	.0086	.0145	.0074	.0145	.0072	.0127	.0063	.0127	.0063	.0113	.0056	.0112	.0056
8	.0206	.0103	.0204	.0101	.0171	.0085	.0169	.0089	.0146	.0072	.0145	.0072	.0126	.0063	.0125	.0062	.0112	.0055	.0111	.0055
9	.0202	.0101	.0200	.0100	.0168	.0084	.0167	.0083	.0144	.0072	.0143	.0072	.0125	.0062	.0125	.0062	.0112	.0055	.0111	.0055

TABLE B-VIII.— VALUES OF j_{no} AND j_{no}^* USED IN EVALUATING EQUATION (26)

$$90 \leq \frac{x_n - x_o}{\Delta x} \leq 189$$

$\frac{x_n - x_o}{\Delta x}$	9x.0		10x.0		11x.0		12x.0		13x.0		14x.0		15x.0		16x.0		17x.0		18x.0	
X	j_{no}	j_{no}^*																		
0	0.0111	0.0053	0.0100	0.0050	0.0091	0.0045	0.0083	0.0042	0.0077	0.0038	0.0071	0.0036	0.0067	0.0033	0.0063	0.0031	0.0059	0.0029	0.0056	0.0028
1	.0109	.0054	.0099	.0050	.0090	.0045	.0083	.0041	.0076	.0038	.0071	.0035	.0066	.0033	.0062	.0031	.0058	.0029	.0055	.0027
2	.0108	.0054	.0098	.0049	.0089	.0045	.0082	.0041	.0076	.0038	.0070	.0035	.0066	.0033	.0061	.0031	.0058	.0029	.0055	.0027
3	.0107	.0054	.0097	.0049	.0088	.0044	.0081	.0041	.0075	.0038	.0070	.0035	.0065	.0033	.0061	.0031	.0057	.0029	.0054	.0027
4	.0106	.0053	.0096	.0048	.0088	.0044	.0081	.0040	.0074	.0037	.0069	.0035	.0065	.0032	.0061	.0030	.0057	.0029	.0054	.0027
5	.0105	.0053	.0095	.0048	.0087	.0043	.0080	.0040	.0074	.0037	.0069	.0034	.0065	.0032	.0061	.0030	.0057	.0028	.0054	.0027
6	.0104	.0052	.0094	.0047	.0086	.0043	.0079	.0040	.0074	.0037	.0068	.0034	.0064	.0032	.0060	.0029	.0056	.0028	.0053	.0027
7	.0103	.0052	.0093	.0047	.0085	.0043	.0079	.0039	.0073	.0036	.0068	.0034	.0064	.0032	.0060	.0029	.0056	.0028	.0053	.0027
8	.0102	.0051	.0093	.0046	.0085	.0042	.0078	.0039	.0072	.0036	.0068	.0034	.0063	.0032	.0059	.0030	.0056	.0028	.0053	.0026
9	.0101	.0051	.0092	.0046	.0084	.0042	.0078	.0039	.0072	.0036	.0067	.0034	.0063	.0031	.0059	.0030	.0056	.0028	.0053	.0026

NACA

TABLE B-IX.— VALUES OF j_{no} AND j_{no}^* USED IN EVALUATING EQUATION (26)

$$(a) \quad -0.999 \leq \frac{x_1 - x_0}{\Delta x} \leq -0.750$$

$\frac{x_1 - x_0}{\Delta x}$	9		8		7		6		5		4		3		2		1		0	
	j_{no}	j_{no}^*																		
-0.999	-6.9068	-5.8998	-6.9126	-5.8003	-5.8061	-4.7887	-5.5175	-4.4954	-5.2933	-4.2668	-5.1100	-4.0793	-4.9548	-3.9202	-4.8203	-3.7617	-4.7015	-3.6992	-4.5931	-3.5492
-0.98	-1.4088	-3.4493	-1.4108	-3.3578	-4.3297	-3.2734	-4.2586	-3.1753	-4.1846	-3.1218	-4.1190	-3.0531	-4.0574	-2.9884	-3.9992	-2.9272	-3.9441	-2.8692	-3.8918	-2.8140
-0.97	-3.8420	-2.7613	-3.7945	-2.7110	-3.7489	-2.6627	-3.7024	-2.6163	-3.6636	-2.5720	-3.6833	-2.5891	-3.5845	-2.4878	-3.5473	-2.4480	-3.5110	-2.4092	-3.4761	-2.3718
-0.96	-3.4423	-2.3356	-3.4095	-2.3004	-3.3777	-2.2666	-3.3468	-2.2330	-3.3168	-2.2007	-3.2876	-2.1692	-3.2891	-2.1385	-3.2310	-2.1086	-3.2044	-2.0794	-3.1761	-2.0509
-0.95	-3.1583	-2.0231	-3.1272	-1.9959	-3.1026	-1.9692	-3.0766	-1.9431	-3.0550	-1.9176	-3.0320	-1.8925	-3.0093	-1.8680	-3.9673	-1.8440	-2.9657	-1.8204	-2.9444	-1.7972
-0.94	-2.9236	-1.7745	-2.9031	-1.7522	-2.8830	-1.7304	-2.8532	-1.7086	-2.8439	-1.6875	-2.8248	-1.6666	-2.8060	-1.6461	-2.7875	-1.6259	-2.7694	-1.6060	-2.7516	-1.5863
-0.93	-2.7339	-1.5671	-2.7167	-1.5488	-2.6995	-1.5695	-2.6827	-1.5110	-2.6666	-1.4729	-2.6499	-1.4750	-2.6337	-1.4572	-2.6178	-1.4398	-2.6022	-1.4226	-2.5867	-1.4056
-0.92	-2.5715	-1.3889	-2.5564	-1.3783	-2.5413	-1.3560	-2.5268	-1.3399	-2.5123	-1.3239	-2.4980	-1.3081	-2.4838	-1.2986	-2.4699	-1.2772	-2.4560	-1.2620	-2.4423	-1.2470
-0.91	-2.4289	-1.2321	-2.4155	-1.2174	-2.4028	-1.2029	-2.3892	-1.1882	-2.3763	-1.1743	-2.3635	-1.1602	-2.3508	-1.1463	-2.3363	-1.1326	-2.3259	-1.1182	-2.3136	-1.1054
-0.90	-2.3023	-1.0920	-2.2892	-1.0768	-2.2773	-1.0657	-2.2557	-1.0568	-2.2341	-1.0399	-2.2165	-1.0272	-2.2110	-1.0146	-2.2196	-1.0021	-2.2084	-9.998	-2.1972	-9.7772
-0.89	-2.1862	-9.6934	-2.1792	-9.5933	-2.1643	-9.414	-2.1536	-9.2956	-2.1429	-9.179	-2.1323	-9.063	-2.1218	-8.947	-2.1113	-8.833	-2.1010	-8.720	-2.0908	-8.6068
-0.88	-2.0806	-8.4946	-2.0702	-8.3936	-2.0607	-8.276	-2.0507	-8.168	-2.0407	-8.060	-2.0309	-7.953	-2.0212	-7.847	-2.0115	-7.746	-2.0019	-7.637	-1.9984	-7.533
-0.87	-1.9630	-7.431	-1.9736	-7.328	-1.9643	-7.227	-1.9551	-7.127	-1.9459	-7.027	-1.9368	-6.9268	-1.9277	-6.829	-1.9188	-6.732	-1.9098	-6.633	-1.9010	-6.538
-0.86	-1.8921	-6.643	-1.8834	-6.548	-1.8747	-6.454	-1.8660	-6.160	-1.8575	-6.067	-1.8489	-5.975	-1.8404	-5.883	-1.8320	-5.792	-1.8236	-5.701	-1.8153	-5.612
-0.85	-1.8070	-5.922	-1.7988	-5.843	-1.7906	-5.743	-1.7823	-5.728	-1.7744	-5.717	-1.7663	-5.684	-1.7583	-5.499	-1.7504	-4.913	-1.7425	-4.628	-1.7346	-4.714
-0.84	-1.7268	-4.660	-1.7190	-4.577	-1.7113	-4.495	-1.7036	-4.412	-1.6959	-4.330	-1.6833	-4.249	-1.6607	-4.168	-1.6732	-4.068	-1.6657	-4.008	-1.6582	-3.929
-0.83	-1.6508	-3.890	-1.6434	-3.772	-1.6361	-3.569	-1.6208	-3.467	-1.6215	-3.339	-1.6182	-3.463	-1.6070	-3.387	-1.5999	-3.311	-1.5927	-3.244	-1.5856	-3.161
-0.82	-1.5786	-3.086	-1.5715	-3.012	-1.5645	-2.938	-1.5575	-2.867	-1.5506	-2.792	-1.5437	-2.720	-1.5368	-2.648	-1.5200	-2.576	-1.5231	-2.505	-1.5154	-2.434
-0.81	-1.5096	-2.236	-1.5029	-2.293	-1.4962	-2.228	-1.4895	-2.154	-1.4868	-2.065	-1.4762	-2.016	-1.4696	-1.948	-1.4650	-1.880	-1.4569	-1.812	-1.4500	-1.745
-0.80	-1.4435	-1.676	-1.4371	-1.611	-1.4306	-1.545	-1.4242	-1.479	-1.4178	-1.414	-1.4115	-1.348	-1.4051	-1.283	-1.3988	-1.219	-1.3926	-1.154	-1.3863	-1.090
-0.79	-1.3801	-1.027	-1.3736	-0.963	-1.3676	-0.900	-1.3615	-0.837	-1.3553	-0.773	-1.3498	-0.713	-1.3431	-0.651	-1.3370	-0.589	-1.3310	-0.528	-1.3249	-0.467
-0.78	-1.3189	-0.406	-1.3129	-0.346	-1.3069	-0.286	-1.3010	-0.226	-1.2951	-0.166	-1.2891	-0.107	-1.2832	-0.048	-1.2774	.0011	-1.2715	.0070	-1.2697	.0128
-0.77	-1.2599	.0186	-1.2540	.0244	-1.2483	.0301	-1.2425	.0358	-1.2368	.0413	-1.2310	.0472	-1.2223	.0528	-1.2196	.0584	-1.2140	.0640	-1.2083	.0696
-0.76	-1.2087	.0751	-1.1970	.0807	-1.1914	.0862	-1.1859	.0916	-1.1803	.0971	-1.1747	.1035	-1.1698	.1079	-1.1687	.1133	-1.1582	.1186	-1.1527	.1240
-0.75	-1.1472	.1293	-1.1417	.1346	-1.1363	.1398	-1.1309	.1451	-1.1254	.1503	-1.1200	.1555	-1.1147	.1606	-1.1093	.1658	-1.1040	.1709	-1.0966	.1760

NACA

TABLE B-IX.— CONTINUED

$$(b) \quad -0.749 \leq \frac{x_n - x_0}{\Delta x} \leq -0.500$$

$\frac{x}{x_n - x_0}$	9		8		7		6		5		4		3		2		1		0	
Δx	j_{no}	j_{no}^*																		
-749	-1.0933	0.1811	-1.0860	0.1862	-1.0827	0.1912	-1.0774	0.1963	-1.0721	0.2013	-1.0669	0.2062	-1.0616	0.2112	-1.0564	0.2162	-1.0512	0.2211	-1.0460	0.2260
-748	-1.0408	.2309	-1.0356	.2357	-1.0304	.2406	-1.0253	.2454	-1.0201	.2504	-1.0150	.2550	-1.0099	.2598	-1.0048	.2645	-9997	.2692	-9946	.2739
-747	-9895	.2786	-9845	.2833	-9795	.2879	-9744	.2926	-9694	.2972	-9644	.3018	-9594	.3064	-9544	.3109	-9494	.3155	-9445	.3200
-746	-9395	.3245	-9346	.3290	-9296	.3334	-9247	.3379	-9196	.3423	-9149	.3468	-9100	.3512	-9051	.3556	-9002	.3599	-8954	.3643
-745	-8905	.3686	-8857	.3729	-8809	.3772	-8761	.3815	-8718	.3858	-8664	.3900	-8616	.3943	-8568	.3983	-8521	.4020	-8473	.4069
-744	-8486	.4111	-8378	.4158	-8330	.4194	-8283	.4235	-8236	.4276	-8189	.4317	-8142	.4358	-8093	.4398	-8048	.4439	-8001	.4479
-743	-7954	.4519	-7908	.4559	-7861	.4599	-7815	.4639	-7768	.4679	-7722	.4718	-7676	.4757	-7630	.4796	-7584	.4835	-7538	.4874
-742	-7492	.4913	-7446	.4958	-7400	.4990	-7354	.5028	-7309	.5057	-7263	.5104	-7218	.5142	-7173	.5180	-7127	.5218	-7062	.5253
-741	-7036	.5293	-6991	.5330	-6946	.5367	-6901	.5404	-6857	.5440	-6812	.5477	-6767	.5513	-6722	.5550	-6678	.5586	-6633	.5622
-740	-6589	.5698	-6544	.5694	-6500	.5730	-6455	.5765	-6411	.5801	-6367	.5836	-6322	.5872	-6278	.5914	-6834	.5922	-6191	.5976
-739	-6146	.6011	-6103	.6016	-6059	.6080	-6013	.6114	-5971	.6149	-5928	.6183	-5884	.6217	-5841	.6250	-5797	.6284	-5754	.6318
-738	-5710	.6351	-5667	.6385	-5624	.6418	-5581	.6451	-5537	.6484	-5494	.6517	-5451	.6549	-5408	.6582	-5365	.6615	-5322	.6647
-737	-5279	.6679	-5237	.6711	-5194	.6743	-5151	.6776	-5108	.6807	-5066	.6839	-5023	.6871	-4980	.6908	-4938	.6934	-4896	.6965
-736	-4853	.6996	-4811	.7027	-4769	.7058	-4726	.7089	-4684	.7119	-4642	.7150	-4600	.7180	-4557	.7211	-4515	.7241	-4473	.7271
-735	-4431	.7302	-4369	.7331	-4347	.7361	-4305	.7391	-4264	.7420	-4222	.7450	-4180	.7480	-4138	.7509	-4097	.7538	-4055	.7567
-734	-4013	.7596	-3972	.7625	-3930	.7654	-3888	.7683	-3847	.7711	-3806	.7739	-3764	.7768	-3723	.7796	-3680	.7804	-3639	.7853
-733	-3598	.7881	-3577	.7908	-3516	.7936	-3473	.7964	-3433	.7993	-3392	.8019	-3351	.8046	-3310	.8074	-3269	.8101	-3228	.8128
-732	-3187	.8155	-3146	.8182	-3105	.8209	-3064	.8235	-3023	.8262	-2982	.8288	-2941	.8315	-2900	.8341	-2859	.8367	-2818	.8393
-731	-2778	.8419	-2737	.8449	-2696	.8471	-2656	.8497	-2604	.8529	-2574	.8548	-2533	.8574	-2533	.8599	-2452	.8624	-2412	.8649
-730	-2371	.8673	-2331	.8700	-2290	.8724	-2249	.8749	-2209	.8774	-2169	.8799	-2128	.8823	-2088	.8848	-2047	.8873	-2007	.8896
-729	-1966	.8920	-1926	.8945	-1886	.8969	-1845	.8993	-1805	.9016	-1765	.9040	-1724	.9064	-1684	.9087	-1644	.9111	-1603	.9134
-728	-1563	.9197	-1523	.9181	-1483	.9204	-1443	.9227	-1402	.9250	-1362	.9273	-1322	.9295	-1282	.9318	-1242	.9341	-1201	.9363
-727	-1161	.9386	-1121	.9408	-1081	.9430	-1041	.9452	-1001	.9475	-961	.9497	-921	.9519	-881	.9540	-840	.9562	-800	.9584
-726	-726	-0.0760	-0.0720	-0.0687	-0.0680	-0.0688	-0.0640	-0.0670	-0.0600	-0.0691	-0.0560	-0.0712	-0.0200	-0.0733	-0.0480	-0.0754	-0.0440	-0.0773	-0.0400	-0.0796
-725	-725	-0.0360	-0.0320	-0.0387	-0.0280	-0.0358	-0.0240	-0.0379	-0.0200	-0.0399	-0.0160	-0.0919	-0.0120	-0.0940	-0.0080	-0.0960	-0.0040	-0.0980	0	1.0000



TABLE B-IX.-- CONTINUED

$$(c) \quad -0.499 \leq \frac{x_{11}-x_0}{\Delta x} \leq -0.250$$

$\frac{x_{11}-x_0}{\Delta x}$	9		8		7		6		5		4		3		2		1		0	
	j_{10}	j_{10}^*																		
-4.94	0.0040	1.0020	0.0080	1.0040	0.0120	1.0060	0.0160	1.0079	0.0200	1.0099	0.0240	1.0119	0.0280	1.0138	0.0320	1.0157	0.0360	1.0177	0.0400	1.0196
-4.85	.0440	1.0315	.0480	1.0334	.0520	1.0353	.0560	1.0372	.0601	1.0391	.0640	1.0310	.0680	1.0389	.0720	1.0347	.0760	1.0366	.0800	1.0384
-4.7	.0842	1.0403	.0881	1.0421	.0920	1.0439	.0960	1.0457	.1001	1.0476	.1041	1.0493	.1081	1.0511	.1121	1.0529	.1161	1.0547	.1202	1.0565
-4.6	.1243	1.0502	.1282	1.0600	.1322	1.0617	.1362	1.0635	.1402	1.0672	.1443	1.0669	.1482	1.0686	.1523	1.0704	.1563	1.0741	.1603	1.0738
-4.5	.1643	1.0754	.1684	1.0771	.1724	1.0788	.1763	1.0805	.1807	1.0821	.1843	1.0838	.1886	1.0854	.1926	1.0871	.1966	1.0887	.2007	1.0903
-4.4	.2047	1.0919	.2087	1.0935	.2128	1.0951	.2169	1.0967	.2209	1.0985	.2250	1.0999	.2290	1.1014	.2330	1.1030	.2371	1.1046	.2411	1.1061
-4.3	.2452	1.1077	.2493	1.1092	.2533	1.1107	.2574	1.1122	.2613	1.1138	.2655	1.1152	.2696	1.1168	.2737	1.1186	.2778	1.1197	.2819	1.1212
-4.2	.2899	1.1227	.2900	1.1241	.2941	1.1256	.2982	1.1270	.3023	1.1285	.3064	1.1299	.3105	1.1313	.3146	1.1328	.3187	1.1342	.3227	1.1355
-4.1	.3269	1.1370	.3310	1.1383	.3351	1.1397	.3392	1.1411	.3433	1.1425	.3472	1.1439	.3516	1.1452	.3557	1.1466	.3598	1.1479	.3639	1.1492
-4.0	.3681	1.1506	.3783	1.1519	.3764	1.1538	.3806	1.1555	.3847	1.1578	.3888	1.1591	.3930	1.1584	.3972	1.1597	.4013	1.1609	.4059	1.1622
-3.9	.4097	1.1633	.4138	1.1647	.4180	1.1659	.4222	1.1672	.4264	1.1684	.4305	1.1696	.4347	1.1708	.4389	1.1720	.4431	1.1732	.4473	1.1745
-3.8	.4515	1.1756	.4557	1.1768	.4600	1.1780	.4642	1.1792	.4681	1.1803	.4726	1.1815	.4769	1.1826	.4811	1.1838	.4853	1.1849	.4896	1.1860
-3.7	.4938	1.1871	.4980	1.1883	.5023	1.1894	.5066	1.1905	.5108	1.1916	.5151	1.1926	.5194	1.1937	.5237	1.1948	.5279	1.1959	.5322	1.1969
-3.6	.5369	1.1980	.5408	1.1990	.5451	1.2001	.5494	1.2011	.5537	1.2021	.5581	1.2031	.5624	1.2041	.5667	1.2051	.5710	1.2061	.5754	1.2071
-3.5	.5797	1.2081	.5841	1.2091	.5884	1.2101	.5927	1.2110	.5971	1.2120	.6015	1.2129	.6059	1.2139	.6103	1.2148	.6146	1.2157	.6191	1.2167
-3.4	.6234	1.2176	.6278	1.2185	.6322	1.2194	.6367	1.2203	.6411	1.2212	.6455	1.2221	.6500	1.2229	.6544	1.2238	.6589	1.2247	.6633	1.2255
-3.3	.6678	1.2264	.6702	1.2272	.6757	1.2281	.6812	1.2289	.6857	1.2297	.6901	1.2305	.6946	1.2313	.6991	1.2321	.7036	1.2329	.7082	1.2337
-3.2	.7127	1.2345	.7173	1.2353	.7218	1.2360	.7263	1.2368	.7309	1.2375	.7354	1.2385	.7400	1.2390	.7446	1.2398	.7492	1.2403	.7538	1.2412
-3.1	.7584	1.2419	.7630	1.2426	.7676	1.2433	.7722	1.2440	.7769	1.2447	.7813	1.2454	.7861	1.2461	.7908	1.2467	.7954	1.2474	.8001	1.2480
-3.0	.8048	1.2487	.8093	1.2493	.8143	1.2500	.8189	1.2506	.8236	1.2512	.8283	1.2518	.8330	1.2524	.8378	1.2530	.8426	1.2536	.8473	1.2542
-2.9	.8521	1.2548	.8568	1.2553	.8616	1.2559	.8664	1.2565	.8712	1.2570	.8761	1.2576	.8809	1.2581	.8857	1.2586	.8905	1.2591	.8954	1.2597
-2.8	.9002	1.2602	.9051	1.2607	.9100	1.2612	.9149	1.2617	.9198	1.2624	.9247	1.2666	.9295	1.2631	.9346	1.2683	.9395	1.2640	.9445	1.2664
-2.7	.9494	1.2649	.9544	1.2653	.9594	1.2658	.9644	1.2662	.9694	1.2666	.9744	1.2670	.9795	1.2674	.9845	1.2678	.9895	1.2682	.9946	1.2687
-2.6	.9997	1.2689	1.0048	1.2693	1.0099	1.2696	1.0150	1.2700	1.0201	1.2703	1.0253	1.2707	1.0304	1.2710	1.0356	1.2713	1.0408	1.2716	1.0460	1.2720
-2.5	1.0532	1.2723	1.0584	1.2726	1.0616	1.2729	1.0669	1.2731	1.0721	1.2734	1.0774	1.2737	1.0827	1.2739	1.0880	1.2742	1.0933	1.2744	1.0986	1.2747



TABLE B-IX.—CONCLUDED

$$(d) \quad -0.249 \leq \frac{x_n - x_0}{\Delta x} \leq 0.000$$

X	9	8		7		6		5		4		3		2		1		0		
$\frac{J_{no}}{\Delta x}$	J _{no}	J _{no} *																		
-241	1.1040	1.2749	1.1093	1.2751	1.1147	1.2753	1.1200	1.2755	1.1194	1.2757	1.1309	1.2759	1.1363	1.2761	1.1417	1.2763	1.1472	1.2765	1.1527	1.2766
-23	1.1582	1.2768	1.1637	1.2770	1.1692	1.2771	1.1747	1.2772	1.1803	1.2774	1.1889	1.2775	1.1914	1.2776	1.1970	1.2777	1.2027	1.2778	1.2063	1.2779
-22	1.2140	1.2780	1.2196	1.2781	1.2223	1.2782	1.2310	1.2784	1.2368	1.2783	1.2439	1.2783	1.2483	1.2784	1.2540	1.2784	1.2599	1.2784	1.2657	1.2785
-21	1.2715	1.2785	1.2774	1.2785	1.2832	1.2787	1.2891	1.2785	1.2951	1.2787	1.3010	1.2784	1.3069	1.2788	1.3129	1.2783	1.3189	1.2783	1.3249	1.2782
-20	1.3310	1.2788	1.3370	1.2791	1.3431	1.2793	1.3498	1.2799	1.3593	1.2798	1.3615	1.2777	1.3676	1.2776	1.3738	1.2773	1.3801	1.2774	1.3863	1.2775
-19	1.3956	1.2771	1.3993	1.2770	1.4051	1.2768	1.4113	1.2766	1.4178	1.2765	1.4242	1.2763	1.4306	1.2761	1.4371	1.2759	1.4435	1.2757	1.4500	1.2755
-18	1.4555	1.2753	1.4530	1.2751	1.4696	1.2748	1.4762	1.2745	1.4828	1.2743	1.4895	1.2741	1.4962	1.2738	1.5029	1.2735	1.5096	1.2732	1.5164	1.2729
-17	1.5231	1.2726	1.5300	1.2723	1.5368	1.2720	1.5437	1.2717	1.5506	1.2714	1.5573	1.2710	1.5645	1.2707	1.5715	1.2703	1.5786	1.2699	1.5856	1.2696
-16	1.5927	1.2692	1.5999	1.2688	1.6070	1.2684	1.6142	1.2680	1.6215	1.2675	1.6288	1.2671	1.6361	1.2667	1.6434	1.2662	1.6508	1.2658	1.6582	1.2655
-15	1.6657	1.2648	1.6732	1.2644	1.6807	1.2639	1.6883	1.2634	1.6999	1.2629	1.7036	1.2683	1.7113	1.2618	1.7190	1.2613	1.7268	1.2607	1.7346	1.2602
-14	1.7425	1.2596	1.7504	1.2591	1.7583	1.2595	1.7663	1.2579	1.7744	1.2573	1.7803	1.2567	1.7906	1.2561	1.7988	1.2557	1.8070	1.2548	1.8153	1.2541
-13	1.8236	1.2535	1.8320	1.2528	1.8404	1.2521	1.8489	1.2513	1.8575	1.2508	1.8660	1.2501	1.8747	1.2493	1.8834	1.2486	1.8921	1.2479	1.9010	1.2471
-12	1.9050	1.2447	1.9188	1.2456	1.9277	1.2448	1.9348	1.2440	1.9459	1.2432	1.9551	1.2424	1.9643	1.2416	1.9736	1.2408	1.9830	1.2399	1.9944	1.2393
-11	2.0019	1.2392	2.0115	1.2374	2.0212	1.2365	2.0309	1.2356	2.0407	1.2347	2.0505	1.2338	2.0605	1.2328	2.0705	1.2319	2.0806	1.2309	2.0908	1.2300
-10	2.1010	1.2290	2.1113	1.2280	2.1218	1.2270	2.1323	1.2260	2.1429	1.2250	2.1536	1.2240	2.1643	1.2229	2.1752	1.2219	2.1862	1.2209	2.1972	1.2197
-09	2.2084	1.2186	2.2196	1.2175	2.2310	1.2164	2.2425	1.2153	2.2541	1.2141	2.2657	1.2130	2.2775	1.2118	2.2893	1.2106	2.3015	1.2094	2.3136	1.2082
-08	2.3259	1.2070	2.3383	1.2058	2.3509	1.2045	2.3635	1.2033	2.3763	1.2020	2.3892	1.2007	2.4022	1.1994	2.4155	1.1981	2.4289	1.1967	2.4423	1.1947
-07	2.4360	1.1940	2.4493	1.1927	2.4638	1.1913	2.4760	1.1898	2.5123	1.1884	2.5268	1.1870	2.5415	1.1859	2.5564	1.1841	2.5715	1.1826	2.5867	1.1811
-06	2.6023	1.1756	2.6178	1.1760	2.6337	1.1763	2.6459	1.1749	2.6662	1.1733	2.6827	1.1717	2.6995	1.1701	2.7166	1.1684	2.7339	1.1668	2.7516	1.1651
-05	2.7654	1.1584	2.7876	1.1617	2.8060	1.1599	2.8248	1.1582	2.8439	1.1564	2.8632	1.1545	2.8830	1.1528	2.9031	1.1510	2.9236	1.1491	2.9444	1.1472
-04	2.9657	1.1453	2.9873	1.1434	3.0095	1.1414	3.0320	1.1395	3.0590	1.1375	3.0786	1.1355	3.1086	1.1334	3.1272	1.1313	3.1823	1.1292	3.1781	1.1271
-03	3.2044	1.1850	3.2314	1.1828	3.2591	1.1806	3.2876	1.1814	3.3168	1.1816	3.3468	1.1818	3.3777	1.1815	3.4093	1.1801	3.4423	1.1807	3.4761	1.1803
-02	3.5110	1.1018	3.5473	1.0993	3.5845	1.0968	3.6033	1.0942	3.6363	1.0916	3.7054	1.0889	3.7489	1.0862	3.7945	1.0835	3.8480	1.0807	3.8918	1.0778
-01	3.9441	1.0749	3.9992	1.0720	4.0574	1.0690	4.1190	1.0659	4.1846	1.0628	4.2846	1.0596	4.3897	1.0563	4.4108	1.0529	4.4988	1.0495	4.5951	1.0460
-00	4.7015	1.0423	4.8203	1.0386	4.9548	1.0347	5.1100	1.0307	5.2933	1.0269	5.5173	1.0221	5.8061	1.0174	6.2126	1.0124	6.9068	1.0069	**	1.0000



APPENDIX C

DETAILS OF SOLUTION OF INTEGRAL (36)

$$F_1 = \int_0^{\epsilon_1} \frac{\frac{\Delta v}{v_o}}{\sqrt{x(c-x)}} \frac{dx}{x-x_o} = \frac{1}{c} \int_0^{\epsilon_1} \frac{\Delta v}{v_o} \frac{1}{\sqrt{\frac{x}{c}}} \frac{1}{\sqrt{1-\frac{x}{c}}} \frac{d(\frac{x}{c})}{\frac{x}{c}-\frac{x_o}{c}} \quad (C1)$$

Introduce $\xi = \frac{x}{c}$ and find

$$F_1 = \frac{1}{c} \int_0^{\epsilon_1/c} \frac{\Delta v}{v_o} \frac{1}{\sqrt{\xi}} \left(1 + \frac{1}{2} \xi + \frac{3}{8} \xi^2 + \dots \right) \frac{d\xi}{\xi - \xi_o} \quad (C2)$$

With the expansion (see equation (37))

$$\begin{aligned} \frac{\Delta v}{v_o} \left(1 + \frac{1}{2} \xi + \frac{3}{8} \xi^2 + \dots \right) &= a_0 + \left(a_1 + \frac{1}{2} a_0 \right) \xi + \left(a_2 + \frac{1}{2} a_1 + \frac{3}{8} a_0 \right) \xi^2 \\ &= a_0 + a_1^* \xi + a_2^* \xi^2 + \dots \end{aligned} \quad (C3)$$

Hence,

$$\begin{aligned} F_1 &= \frac{1}{c} \int_0^{\epsilon_1/c} \frac{a_0 + a_1^* \xi + a_2^* \xi^2}{\sqrt{\xi} (\xi - \xi_o)} d\xi \\ &= \frac{1}{c} \left[a_0 \int_0^{\epsilon_1/c} \frac{d\xi}{\sqrt{\xi} (\xi - \xi_o)} + \right. \\ &\quad a_1^* \int_0^{\epsilon_1/c} \frac{\xi d\xi}{\sqrt{\xi} (\xi - \xi_o)} + \\ &\quad \left. a_2^* \int_0^{\epsilon_1/c} \frac{\xi^2 d\xi}{\sqrt{\xi} (\xi - \xi_o)} \right]. \end{aligned} \quad (C4)$$

As the occurring integrals are all of the same type, define

$$L_n = \int_0^{\epsilon_1/c} \frac{\xi^n d\xi}{\sqrt{\xi} (\xi - \xi_0)} \quad (C5)$$

These integrals L_n are easily solved by recurrence.

$$L_n = \xi_0 L_{n-1} + \frac{\left(\frac{\epsilon_1}{c}\right)^{n-\frac{1}{2}}}{n - \frac{1}{2}} \quad (C6)$$

with

$$L_0 = \frac{1}{\sqrt{\xi_0}} \log_e \frac{1 - \sqrt{\frac{\epsilon_1}{x_0}}}{1 + \sqrt{\frac{\epsilon_1}{x_0}}} \quad \text{for } x_0 > \epsilon_1 \quad (C7)$$

and

$$L_0 = \frac{1}{\sqrt{\xi_0}} \log_e \frac{1 - \sqrt{\frac{x_0}{\epsilon_1}}}{1 + \sqrt{\frac{x_0}{\epsilon_1}}} \quad \text{for } x_0 < \epsilon_1 \quad (C8)$$

The function

$$M_0 = \log_e \frac{1 - \sqrt{\frac{\epsilon_1}{x_0}}}{1 + \sqrt{\frac{\epsilon_1}{x_0}}} \quad \text{and} \quad \log_e \frac{1 - \sqrt{\frac{x_0}{\epsilon_1}}}{1 + \sqrt{\frac{x_0}{\epsilon_1}}}$$

is given in figure 2 in order to provide a more rapid computation in the event that $\frac{x_0}{\epsilon_1}$ or $\frac{\epsilon_1}{x_0}$ is not very small.

If $\frac{\epsilon_1}{x_0} \ll 1$,

$$M_0 = -2 \left(\sqrt{\frac{\epsilon_1}{x_0}} + \frac{1}{3} \sqrt{\frac{\epsilon_1}{x_0}}^3 + \frac{1}{5} \sqrt{\frac{\epsilon_1}{x_0}}^5 + \dots \right) \quad (C9)$$

The integrals L_0 , L_1 , and L_2 are needed; these are given by

$$\left. \begin{aligned} L_0 &= \frac{1}{\sqrt{\xi_0}} M_0 \\ L_1 &= \sqrt{\xi_0} M_0 + 2 \sqrt{\frac{\epsilon_1}{c}} \\ L_2 &= \xi_0 L_1 + \frac{2}{3} \sqrt{\frac{\epsilon_1}{c}}^3 \\ &= \xi_0^{3/2} M_0 + 2 \xi_0 \sqrt{\frac{\epsilon_1}{c}} + \frac{2}{3} \sqrt{\frac{\epsilon_1}{c}}^3 \end{aligned} \right\} \quad (C10)$$

If $\frac{\epsilon_1}{x_0} \ll 1$,

$$\left. \begin{aligned} L_0 &= -\frac{2}{\sqrt{\xi_0}} \left(\sqrt{\frac{\epsilon_1}{x_0}} + \frac{1}{3} \sqrt{\frac{\epsilon_1}{x_0}}^3 + \frac{1}{5} \sqrt{\frac{\epsilon_1}{x_0}}^5 + \dots \right) \\ L_1 &= -2 \sqrt{\xi_0} \left(\frac{1}{3} \sqrt{\frac{\epsilon_1}{x_0}}^3 + \frac{1}{5} \sqrt{\frac{\epsilon_1}{x_0}}^5 + \dots \right) \\ L_2 &= -2 \sqrt{\xi_0}^3 \left(\frac{1}{5} \sqrt{\frac{\epsilon_1}{x_0}}^5 + \dots \right) \end{aligned} \right\} \quad (C11)$$

With these expressions the integral F_1 is as follows:

$$\begin{aligned}
 F_1 &= \frac{1}{c} \left(a_0 L_0 + a_1^* L_1 + a_2^* L_2 \right) \\
 &= \frac{1}{c} \left[\frac{a_0}{\sqrt{\xi_0}} M_0 + a_1^* \left(\sqrt{\xi_0} M_0 + 2\sqrt{\frac{\epsilon_1}{c}} \right) + a_2^* \left(\sqrt{\xi_0}^3 M_0 + \right. \right. \\
 &\quad \left. \left. 2\xi_0 \sqrt{\frac{\epsilon_1}{c}} + \frac{2}{3} \sqrt{\frac{\epsilon_1}{c}}^3 \right) \right] \\
 &= \frac{1}{c} \left[M_0 \left(\frac{a_0}{\sqrt{\xi_0}} + a_1^* \sqrt{\xi_0} + a_2^* \sqrt{\xi_0}^3 \right) + \right. \\
 &\quad \left. 2\sqrt{\frac{\epsilon_1}{c}} (a_1^* + \xi_0 a_2^*) + \frac{2}{3} a_2^* \sqrt{\frac{\epsilon_1}{c}}^3 \right] . \tag{C12}
 \end{aligned}$$

The coefficients a_0 , a_1 , and a_2 of the expansion of $\frac{\Delta v}{V_0}$ are given by

$$\left. \begin{aligned}
 a_0 &= \left(\frac{\Delta v}{V_0} \right)_{x=0} \\
 a_1 &= \frac{c}{2\epsilon_1} \left[-3 \left(\frac{\Delta v}{V_0} \right)_{x=0} + 4 \left(\frac{\Delta v}{V_0} \right)_{x=\epsilon_1} - \left(\frac{\Delta v}{V_0} \right)_{x=2\epsilon_1} \right] \\
 a_2 &= \frac{c^2}{2\epsilon_1^2} \left[\left(\frac{\Delta v}{V_0} \right)_{x=0} - 2 \left(\frac{\Delta v}{V_0} \right)_{x=\epsilon_1} + \left(\frac{\Delta v}{V_0} \right)_{x=2\epsilon_1} \right]
 \end{aligned} \right\} \tag{C13}$$

REFERENCES

1. Allen, H. Julian: General Theory of Airfoil Sections Having Arbitrary Shape or Pressure Distribution. NACA Rep. 833, 1945.
2. Naiman, Irven: Numerical Evaluation of the ϵ -Integral Occurring in the Theodorsen Arbitrary Airfoil Potential Theory. NACA ARR L4D27a, 1944.
3. Naiman, Irven: Numerical Evaluation by Harmonic Analysis of the ϵ -Function of the Theodorsen Arbitrary-Airfoil Potential Theory. NACA ARR L5H18, 1945.
4. Multhopp, H.: Die Berechnung der Auftriebsverteilung von Tragflügeln. Luftfahrtforschung, Bd. 15, Nr. 4, April 6, 1938, pp. 153-169.
5. Timman, R.: The Numerical Evaluation of the Poisson Integral. Rapport F.32, Nationaal Luchtvaartlaboratorium, June 16, 1948. (English)
6. Schoenberg, I. J.: Contributions to the Problem of Approximation of Equidistant Data by Analytic Functions. Part A.- On the Problem of Smoothing or Graduation. A First Class of Analytic Approximation Formulae. Quart. Appl. Math., vol. IV, no. 1, April 1946, pp. 45-99; Part B.- On the Problem of Osculatory Interpolation. A Second Class of Analytic Approximation Formulae. Quart. Appl. Math., vol. IV, no. 2, July 1946, pp. 112-141.

TABLE I.- VALUES OF j_{no} AND j_{no}^* FOR $-49.5 < \frac{x_n - x_0}{\Delta x} < 49.5$

$\frac{x_n - x_0}{\Delta x}$	j_{no}	j_{no}^*	$\frac{x_n - x_0}{\Delta x}$	j_{no}	j_{no}^*
-49.5	-0.0204	-0.0102	0.5	1.0986	0.4507
-48.5	-.0208	-.0104	1.5	.5108	.2338
-47.5	-.0213	-.0107	2.5	.3365	.1588
-46.5	-.0217	-.0109	3.5	.2513	.1204
-45.5	-.0222	-.0112	4.5	.2007	.0970
-44.5	-.0227	-.0114	5.5	.1671	.0812
-43.5	-.0233	-.0117	6.5	.1431	.0698
-42.5	-.0238	-.0120	7.5	.1252	.0613
-41.5	-.0244	-.0122	8.5	.1112	.0546
-40.5	-.0250	-.0125	9.5	.1001	.0492
-39.5	-.0256	-.0129	10.5	.0910	.0448
-38.5	-.0263	-.0132	11.5	.0834	.0411
-37.5	-.0270	-.0136	12.5	.0770	.0380
-36.5	-.0278	-.0139	13.5	.0715	.0353
-35.5	-.0286	-.0143	14.5	.0667	.0330
-34.5	-.0294	-.0148	15.5	.0625	.0309
-33.5	-.0303	-.0153	16.5	.0588	.0291
-32.5	-.0313	-.0157	17.5	.0556	.0275
-31.5	-.0323	-.0162	18.5	.0526	.0261
-30.5	-.0333	-.0167	19.5	.0500	.0248
-29.5	-.0345	-.0173	20.5	.0476	.0236
-28.5	-.0357	-.0180	21.5	.0455	.0226
-27.5	-.0370	-.0186	22.5	.0435	.0216
-26.5	-.0385	-.0193	23.5	.0417	.0207
-25.5	-.0400	-.0201	24.5	.0400	.0199
-24.5	-.0417	-.0210	25.5	.0385	.0191
-23.5	-.0435	-.0219	26.5	.0370	.0184
-22.5	-.0455	-.0229	27.5	.0357	.0178
-21.5	-.0476	-.0240	28.5	.0345	.0172
-20.5	-.0500	-.0252	29.5	.0333	.0166
-19.5	-.0526	-.0266	30.5	.0323	.0160
-18.5	-.0556	-.0280	31.5	.0313	.0155
-17.5	-.0588	-.0297	32.5	.0303	.0151
-16.5	-.0625	-.0316	33.5	.0294	.0146
-15.5	-.0667	-.0337	34.5	.0286	.0142
-14.5	-.0715	-.0362	35.5	.0278	.0138
-13.5	-.0770	-.0390	36.5	.0270	.0134
-12.5	-.0834	-.0423	37.5	.0263	.0131
-11.5	-.0910	-.0462	38.5	.0256	.0127
-10.5	-.1001	-.0509	39.5	.0250	.0125
-9.5	-.1112	-.0567	40.5	.0244	.0122
-8.5	-.1252	-.0639	41.5	.0238	.0118
-7.5	-.1431	-.0733	42.5	.0233	.0116
-6.5	-.1671	-.0859	43.5	.0227	.0113
-5.5	-.2007	-.1037	44.5	.0222	.0111
-4.5	-.2513	-.1309	45.5	.0217	.0108
-3.5	-.3365	-.1777	46.5	.0213	.0106
-2.5	-.5108	-.2771	47.5	.0208	.0103
-1.5	-.1.0986	-.6479	48.5	.0204	.0101
-.5	0	1.0	49.5	.0200	.0100



TABLE II.- COMPUTATION BY UNEQUAL INTERVALS, TRANSITION FROM
ONE INTERVAL SIZE TO ANOTHER

(a) $\overline{\Delta x} = 0.002$.

$\frac{x}{c}$	σ_n	$\sigma_{n+1} - \sigma_n$	$\frac{x_n - x_0}{\Delta x}$	j_{no}	j_{no}^*
0	σ_0	$\sigma_1 - \sigma_0$	-4.5	-0.2513	-0.1309
.002	σ_1	$\sigma_2 - \sigma_1$	-3.5	-.3365	-.1777
.004	σ_2	$\sigma_3 - \sigma_2$	-2.5	-.5108	-.2771
.006	σ_3	$\sigma_4 - \sigma_3$	-1.5	-.10986	-.6479
.008	σ_4	$\sigma_5 - \sigma_4$	-.5	0	1.0
.010	σ_5	$\sigma_6 - \sigma_5$.5	1.0986	.4507
.012	σ_6	$\sigma_7 - \sigma_6$	1.5	.5108	.2338
.014	.	.	2.5	.3365	.1588
.016	.	.	3.5	.2513	.1204
.018	.	.	4.5	.2007	.0970
.020	.	.	5.5	.1671	.0812
.022	.	.	6.5	.1431	.0698
.024	.	.	7.5	.1252	.0613
.026	.	.	8.5	.1112	.0546
.028	σ_{14}	$\sigma_{15} - \sigma_{14}$	9.5	.1001	.0492
.030	σ_{15}		10.5		

(b) $\overline{\Delta x} = 0.006$.

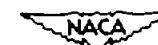
$\frac{x}{c}$	σ_n	$\sigma_{n+1} - \sigma_n$	$\frac{x_n - x_0}{\Delta x}$	j_{no}	j_{no}^*
0	σ_0	$\sigma_3 - \sigma_0$	-1.5	-1.0986	-0.6479
.006	σ_3	$\sigma_6 - \sigma_3$	-.5	0	1.0
.012	σ_6	$\sigma_9 - \sigma_6$.5	1.0986	.4507
.018	σ_9	$\sigma_{12} - \sigma_9$	1.5	.5108	.2338
.024	σ_{12}	$\sigma_{15} - \sigma_{12}$	2.5	.3365	.1588
<hr/>					
.030	σ_{15}	$\sigma_{16} - \sigma_{15}$	3.5	.2513	.1204
.036	σ_{16}	$\sigma_{17} - \sigma_{16}$	4.5	.2007	.0970
.042	σ_{17}	$\sigma_{18} - \sigma_{17}$	5.5	.1671	.0812
.048	σ_{18}	$\sigma_{19} - \sigma_{18}$	6.5	.1431	.0698
.054	.	.	7.5	.1252	.0613
.060	.	.	8.5	.1112	.0546
.066	.	.	9.5	.1001	.0492
.072	.	.	10.5	.0910	.0448
.078	.	.	11.5	.0834	.0411
.084	.	.	12.5	.0770	.0380
.090	σ_{25}	$\sigma_{26} - \sigma_{25}$	13.5	.0715	.0353
.096	σ_{26}	$\sigma_{27} - \sigma_{26}$	14.5	.0667	.0330



TABLE III.- COMPUTATION FOR $x_0 = 0.065$ BY UNEQUAL INTERVALS

[Example, fig. 18]

x_n	σ_n	$\sigma_{n+1} - \sigma_n$	$\frac{x_n - x_0}{\bar{\Delta}x_n}$	$\frac{x_n - x_0}{\overline{\Delta}x_n}$	$\frac{x_n - x_0}{\overline{\overline{\Delta}x}_n}$	j_{no}	j_{no}^*
0.060	0	0.005	-1.5			-1.099	-0.648
.0633	.005	.010	-.5			0	1.0
.0667	.015	.021	.5			1.099	.451
.070	.036	.0565		1.0		.693	.307
.075	.0925	.1075		2.0		.406	.189
.080	.2000	-.1000		3.0		.288	.137
.085	.1000	-.094		4.0		.223	.107
.090	.006	-.0087			2.5	.336	.159
.100	-.0027	.0011			3.5	.251	.120
.110	-.0016	.0016			4.5	.201	.097
.120	0	0			5.5	.167	.081
			$\bar{\Delta}x = 0.0033$	$\overline{\Delta}x = 0.005$	$\overline{\overline{\Delta}x} = 0.010$		



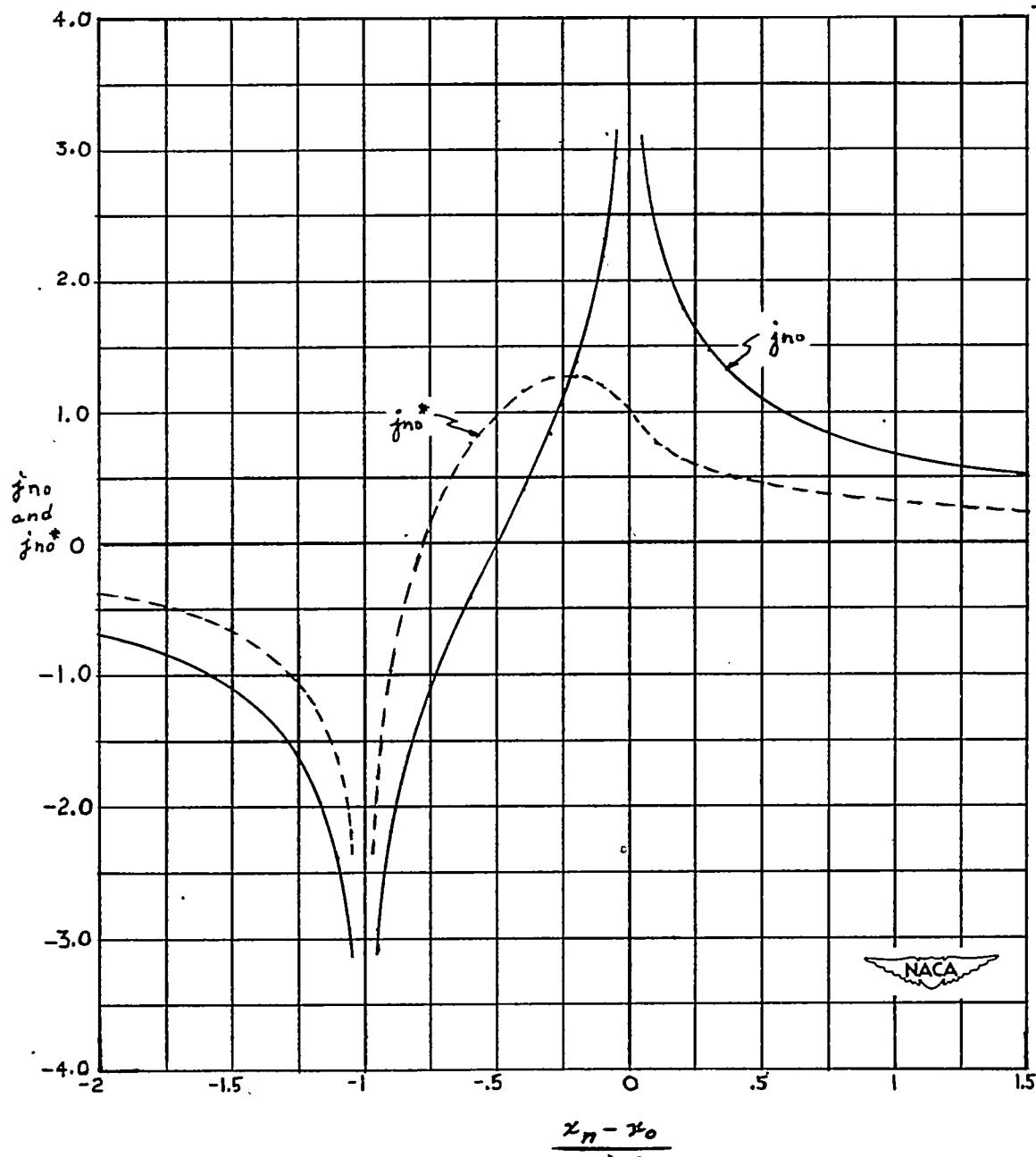


Figure 1.- Characteristic qualities of j_{no} and j_{no}^* as functions

$$\text{of } \frac{x_n - x_o}{\Delta x}.$$

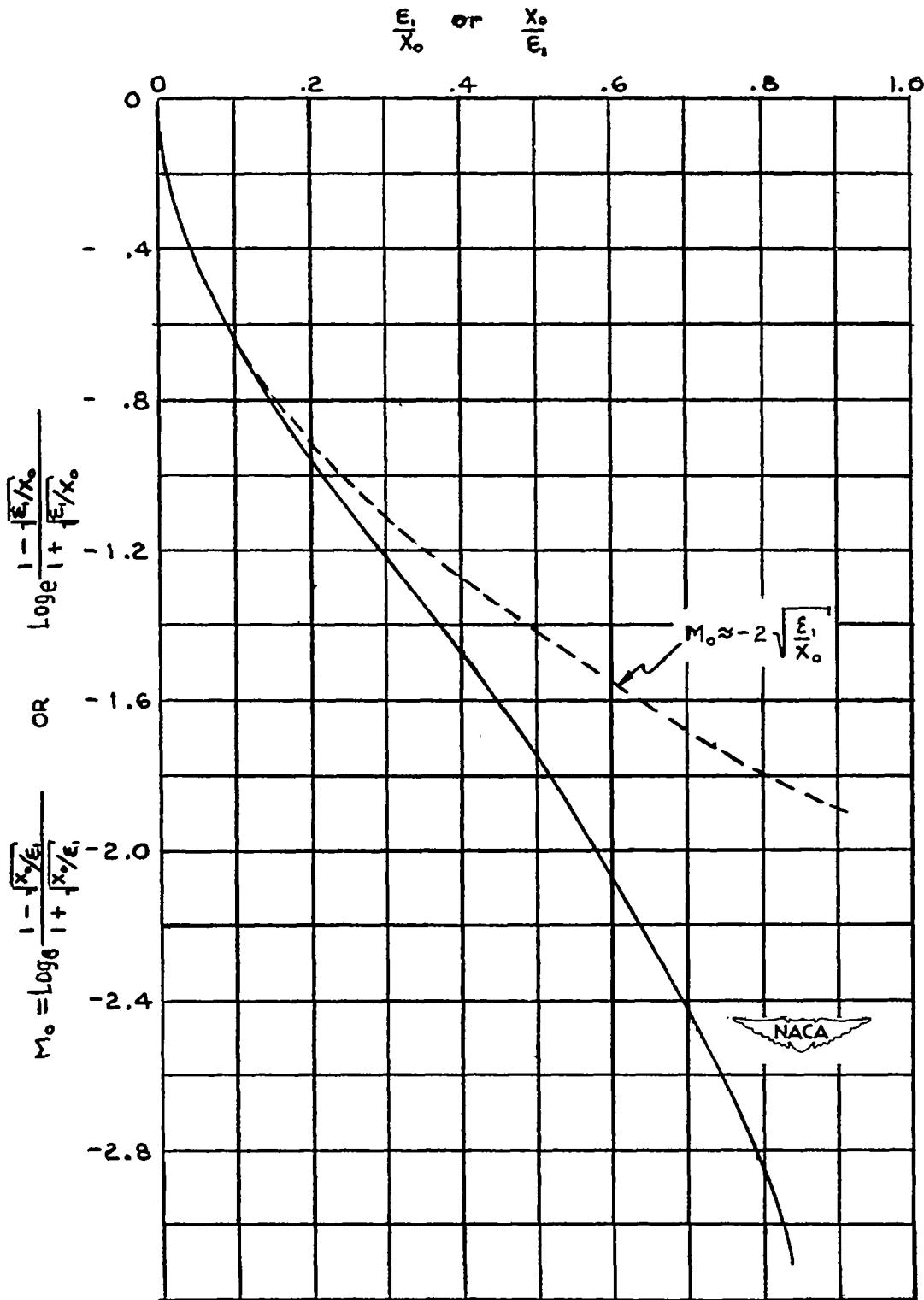


Figure 2.- Function M_0 for computation when x_0/ϵ_1 or ϵ_1/x_0 is not small.

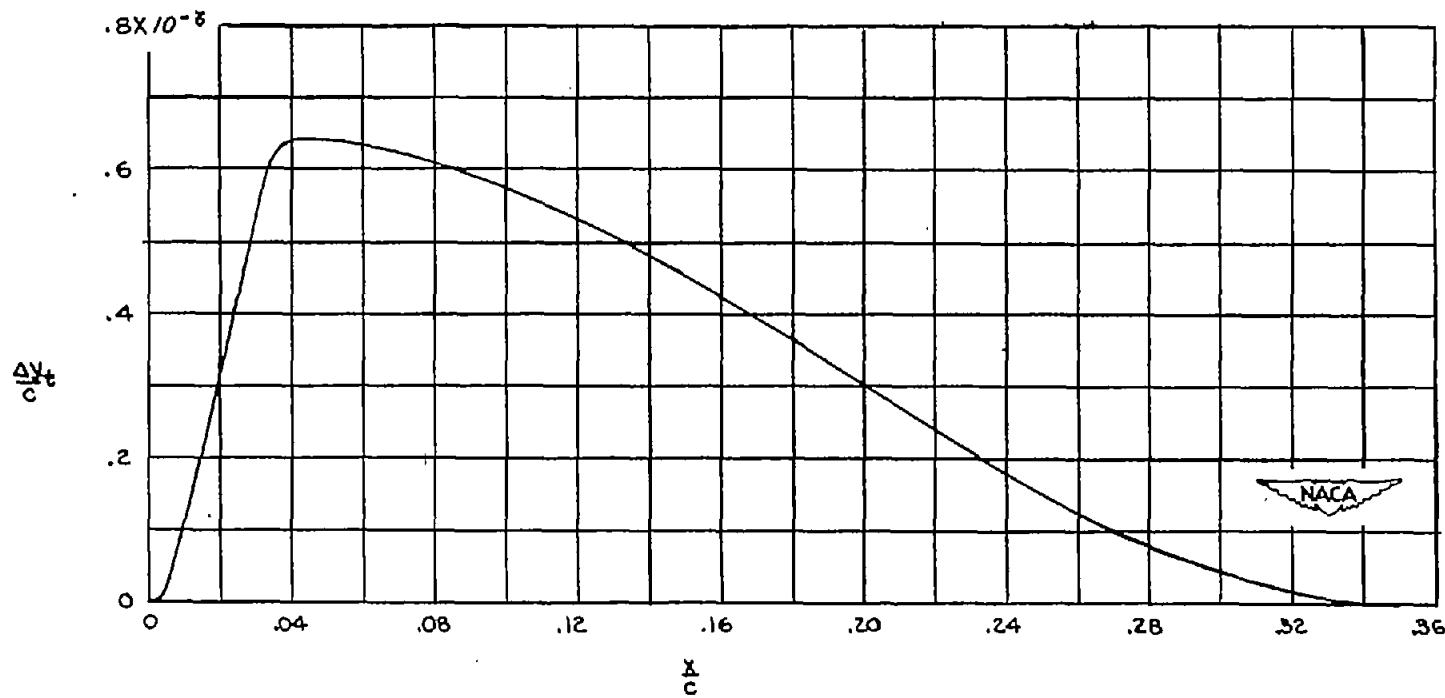
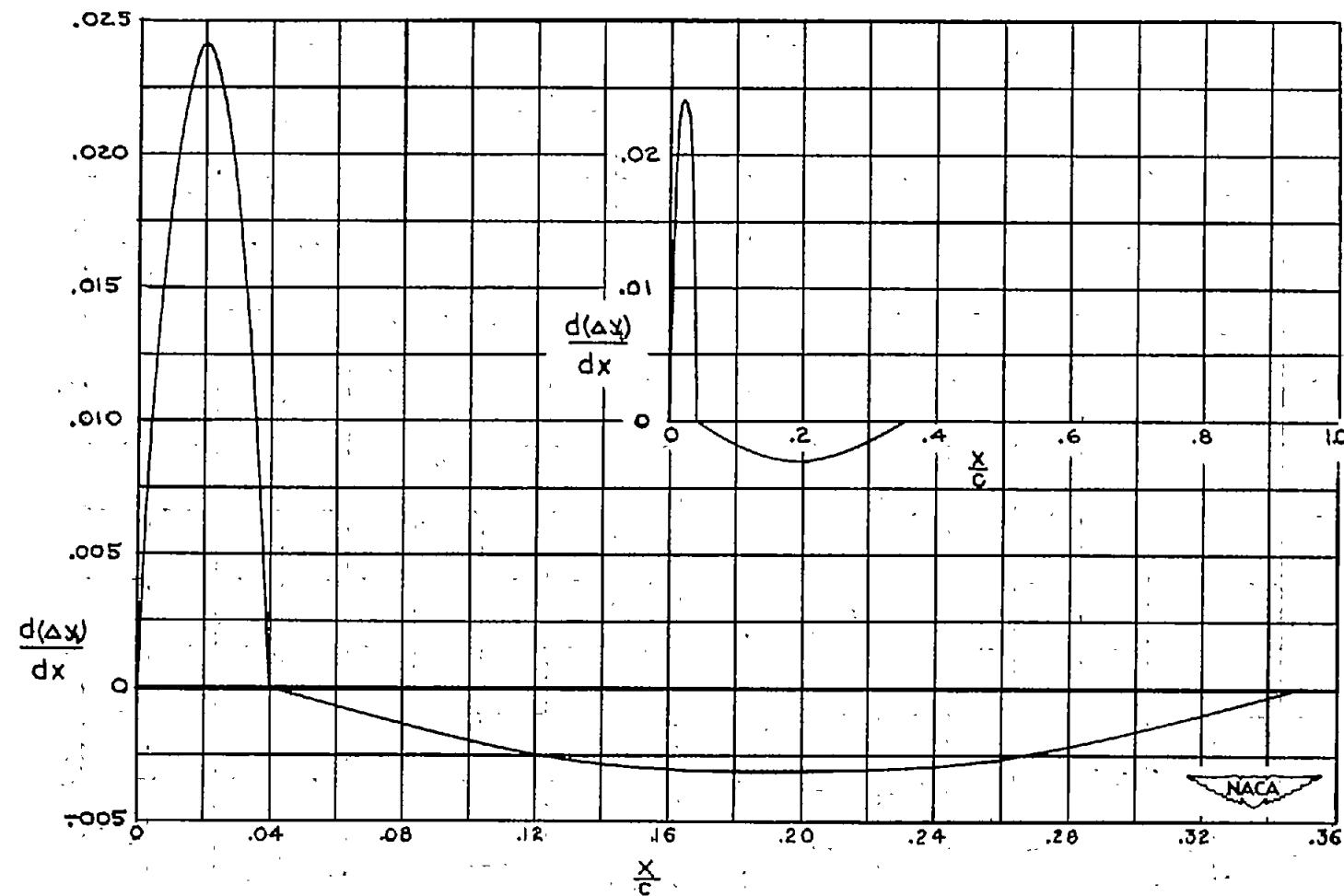
(a) Function ΔY_t .

Figure 3.- Analytical example for testing accuracy of method.



(b) Function $\frac{d(\Delta y_t)}{dx}$.

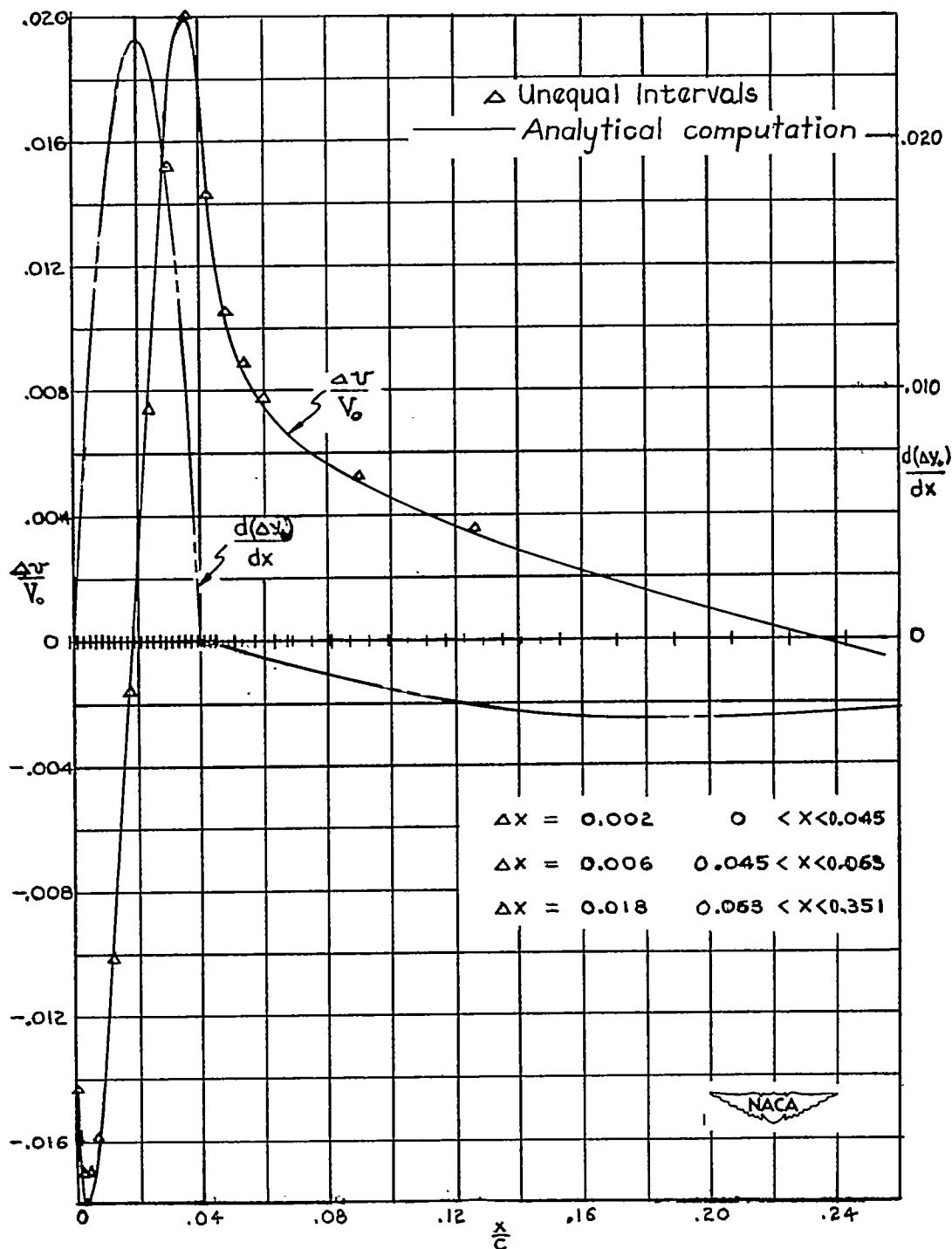
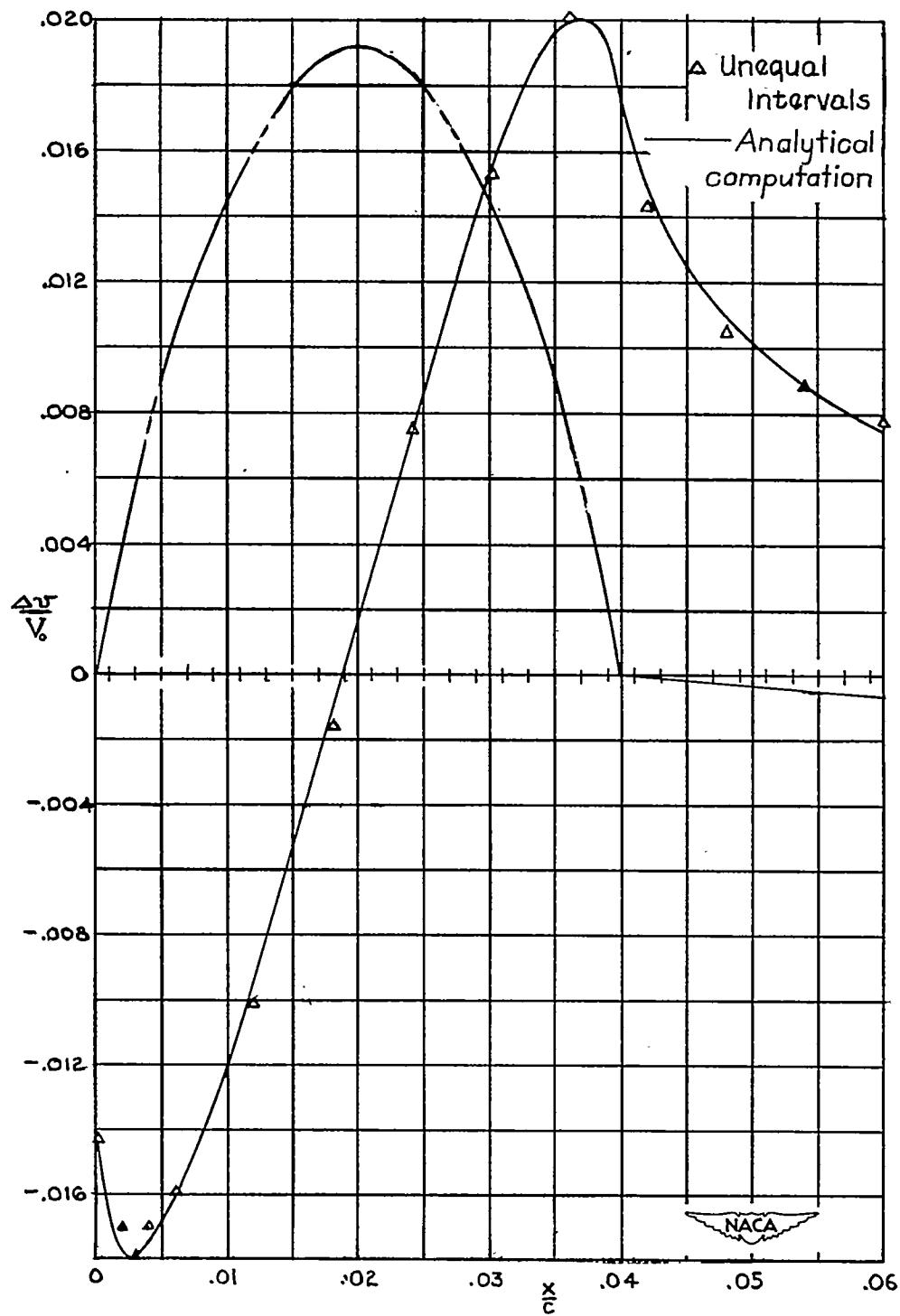
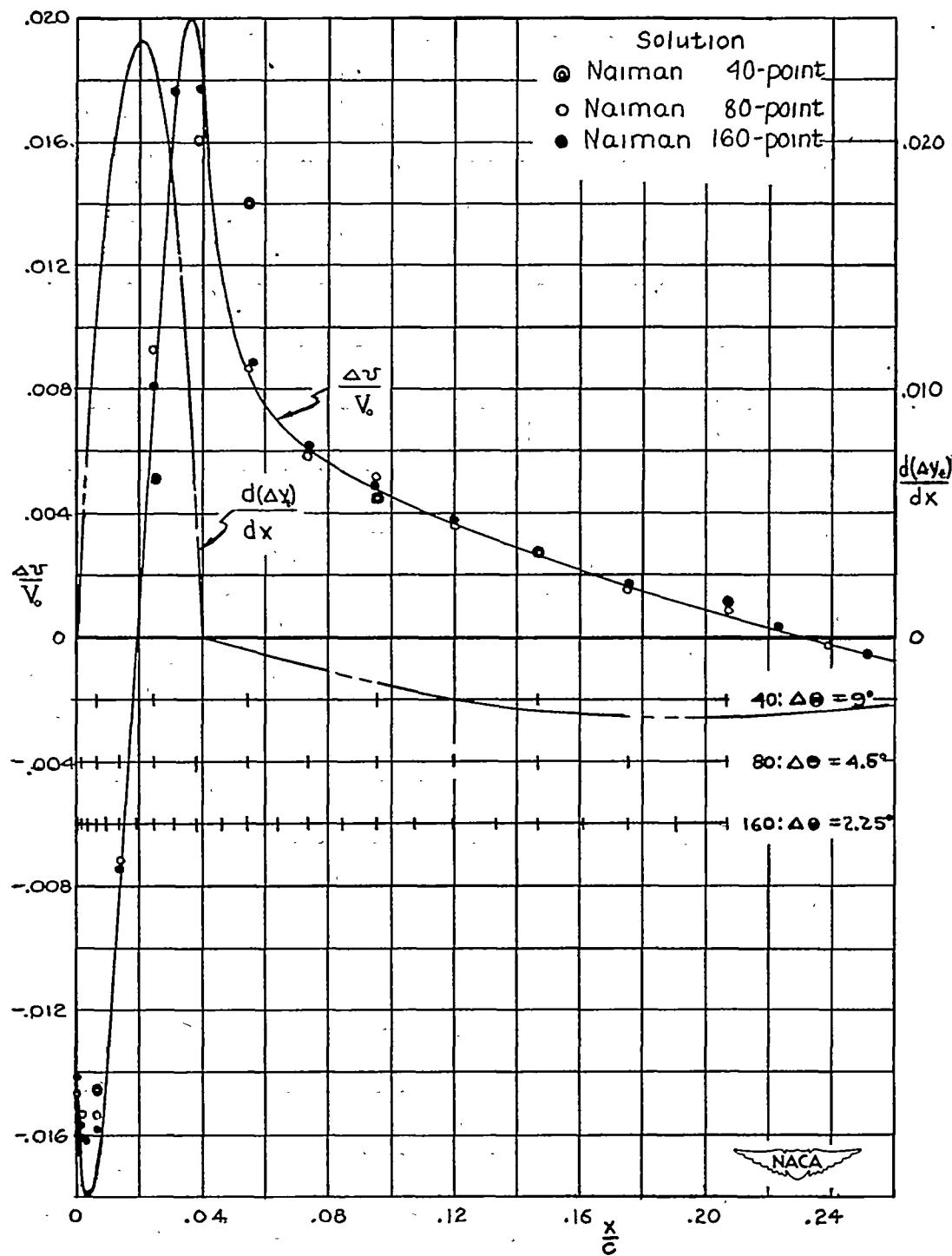
(a) Plot for $0 < x < 0.25$.

Figure 4.- Analytical computation of $\frac{\Delta v}{V_0}$ for figure 3(b) and comparison with results by computation with unequal intervals.



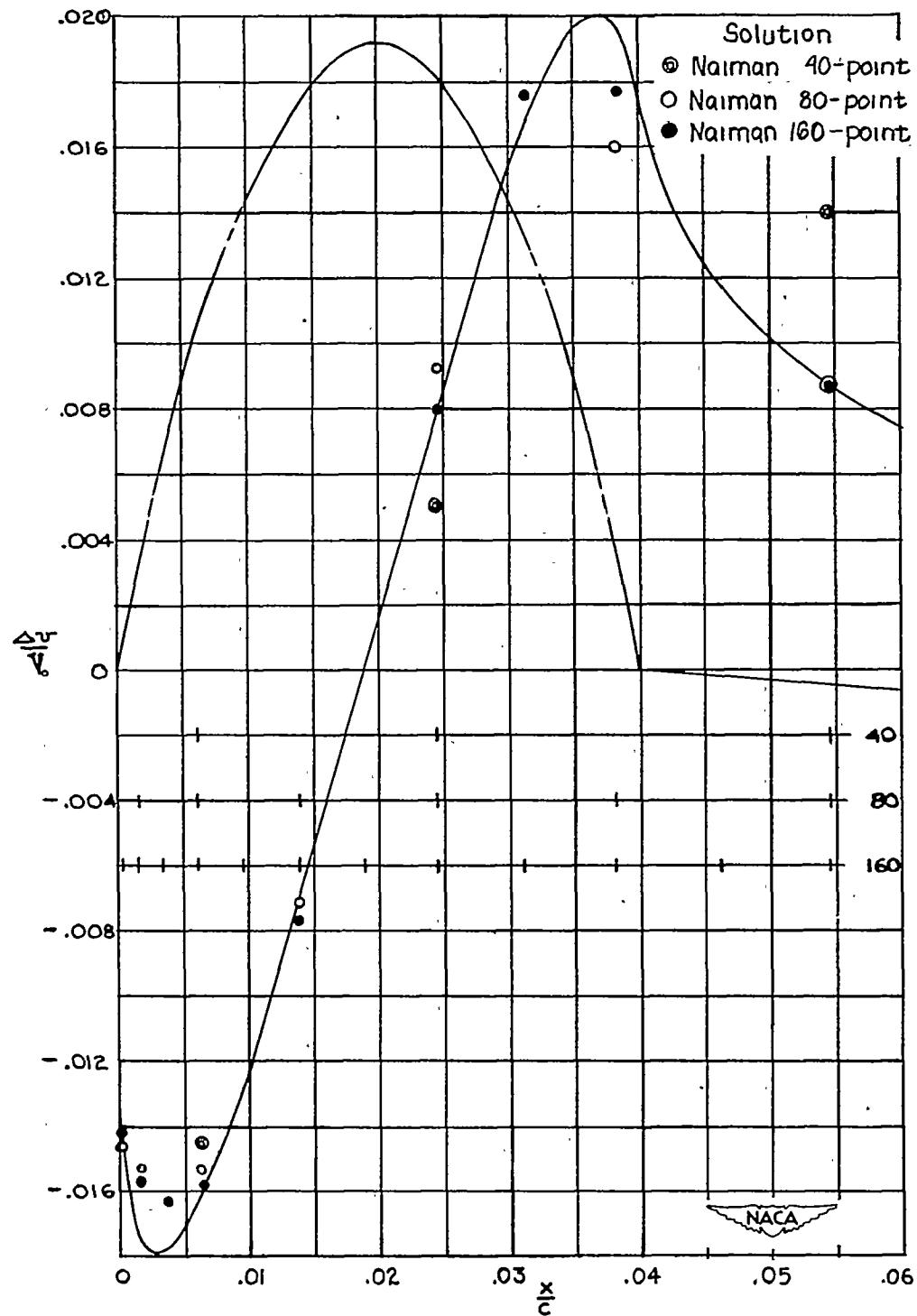
(b) Part of figure 4(a) plotted to larger scale.

Figure 4.- Concluded.



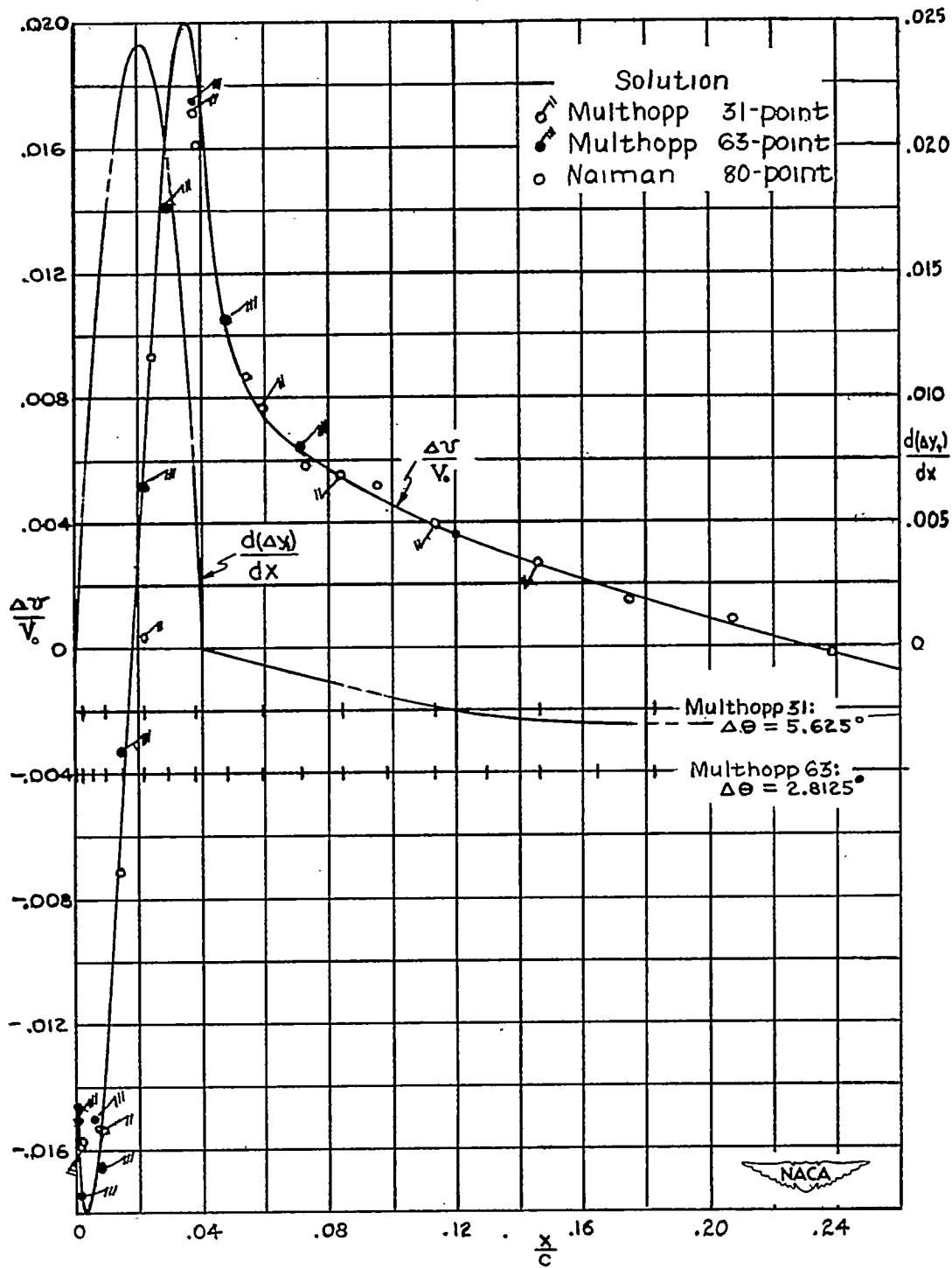
(a) Comparison with analytical results.

Figure 5.- Results obtained by Naiman's method. 40-, 80-, and 160-point solutions.



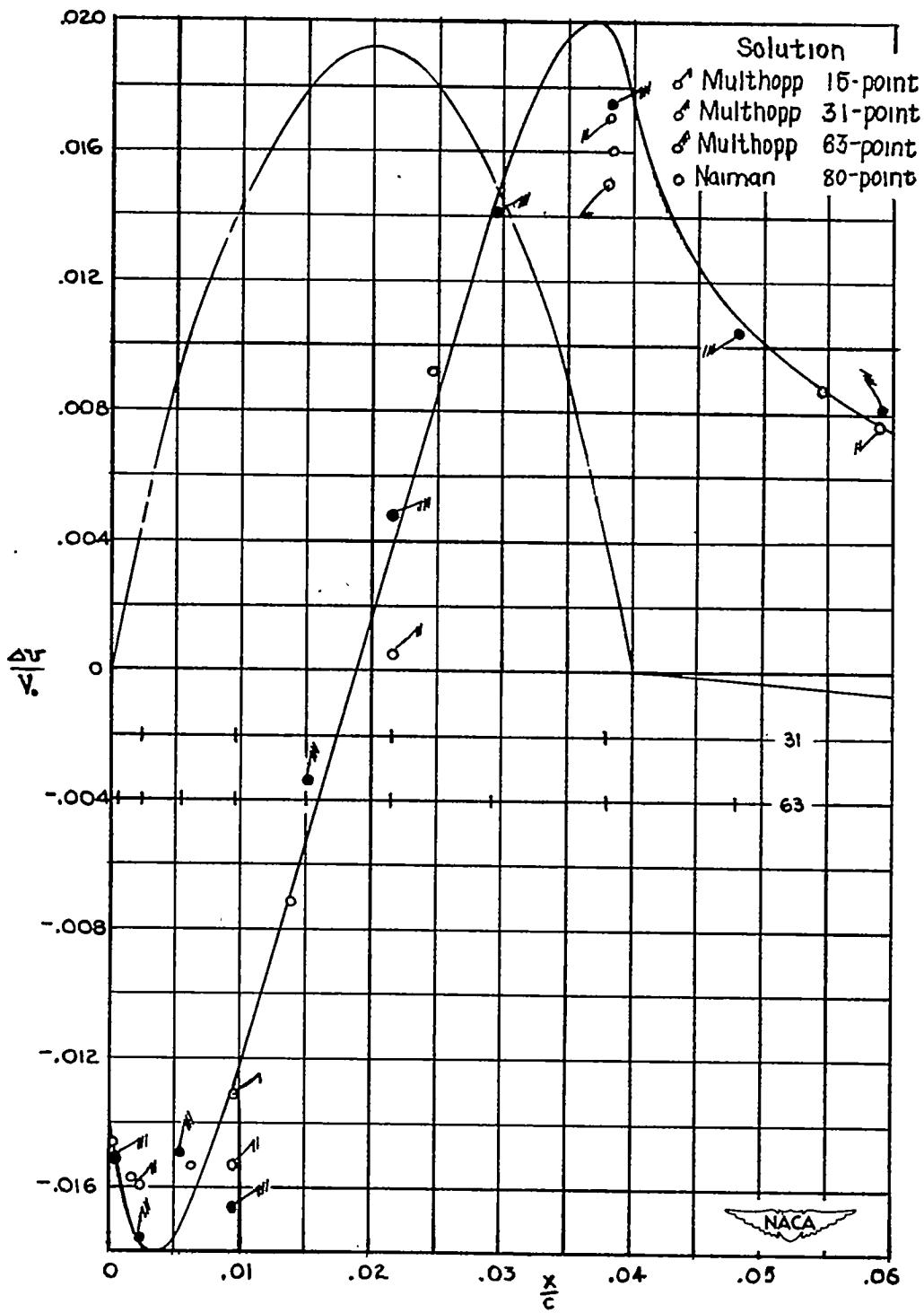
(b) Figure 5(a) plotted to a larger scale.

Figure 5.- Concluded.



(a) Comparison with analytical results and results of Naiman's method.

Figure 6.- Results obtained by Multhopp's method. 31- and 63-point solutions.



(b) Figure 6(a) plotted to larger scale.

Figure 6.- Concluded.

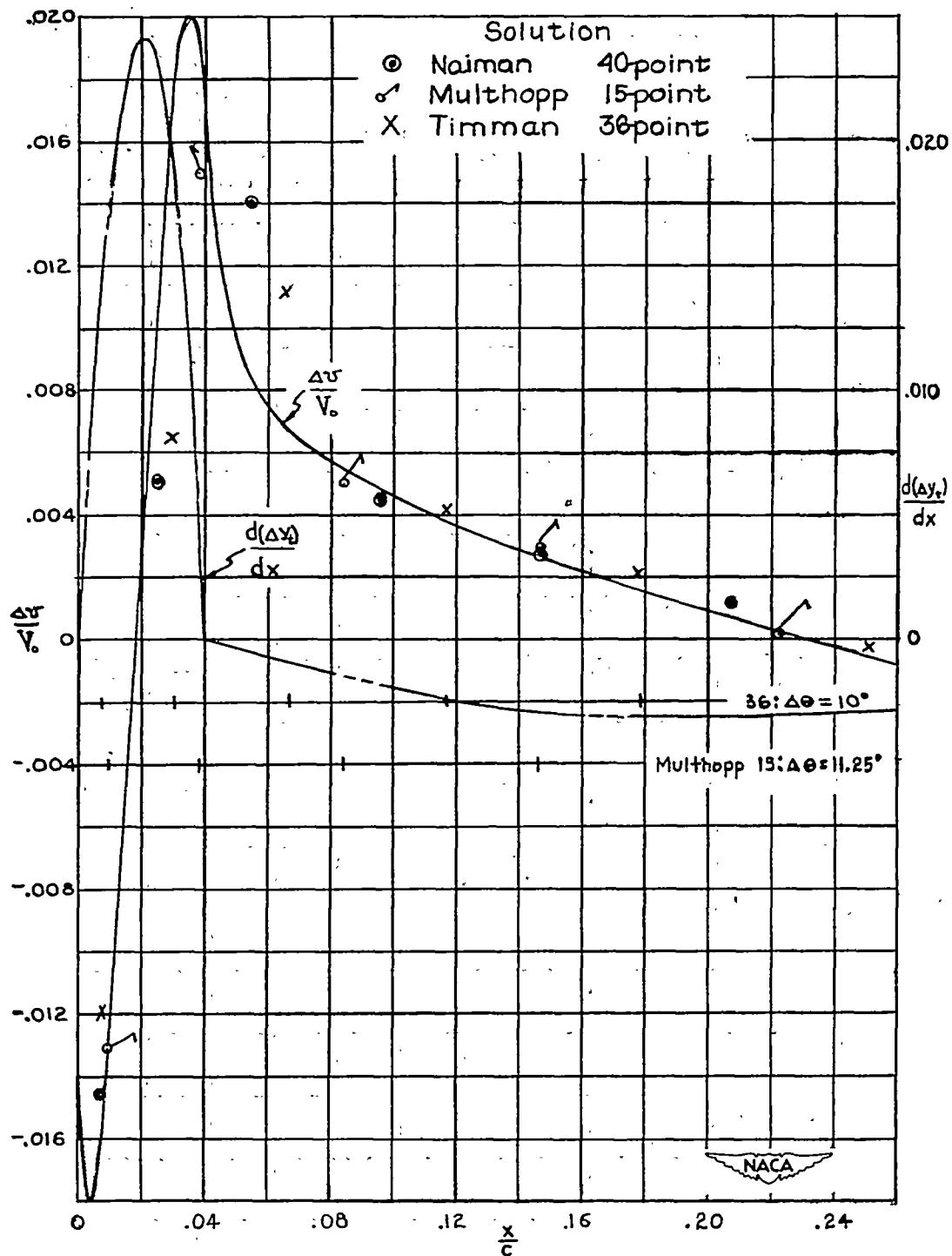


Figure 7.- Comparison of methods of Naiman, Multhopp, and Timman
with analytical solution as basis.

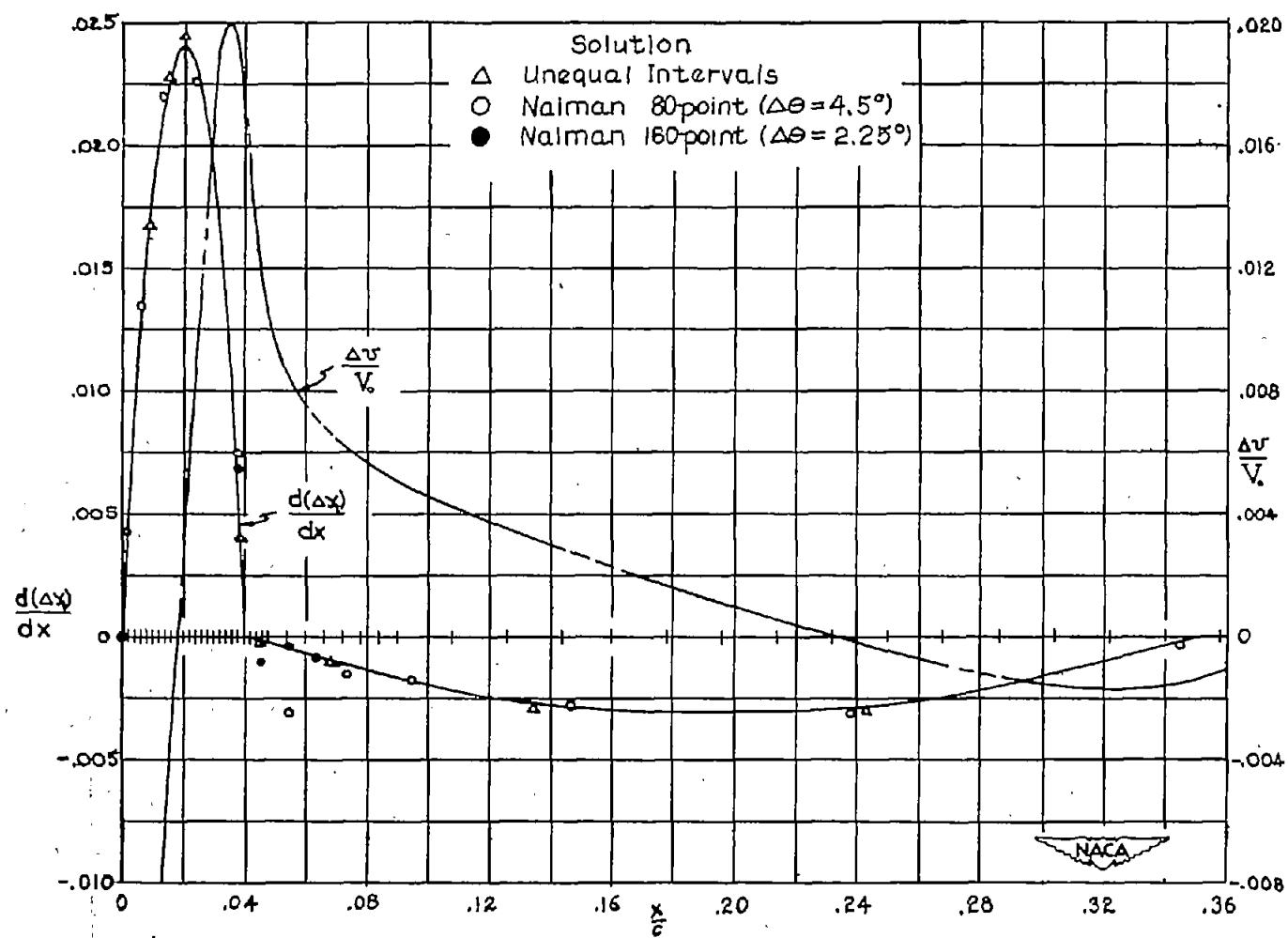


Figure 8.- Solution of inverse problem. Comparison of Naiman's 80- and 160-point solutions with that obtained by the method of unequal intervals.

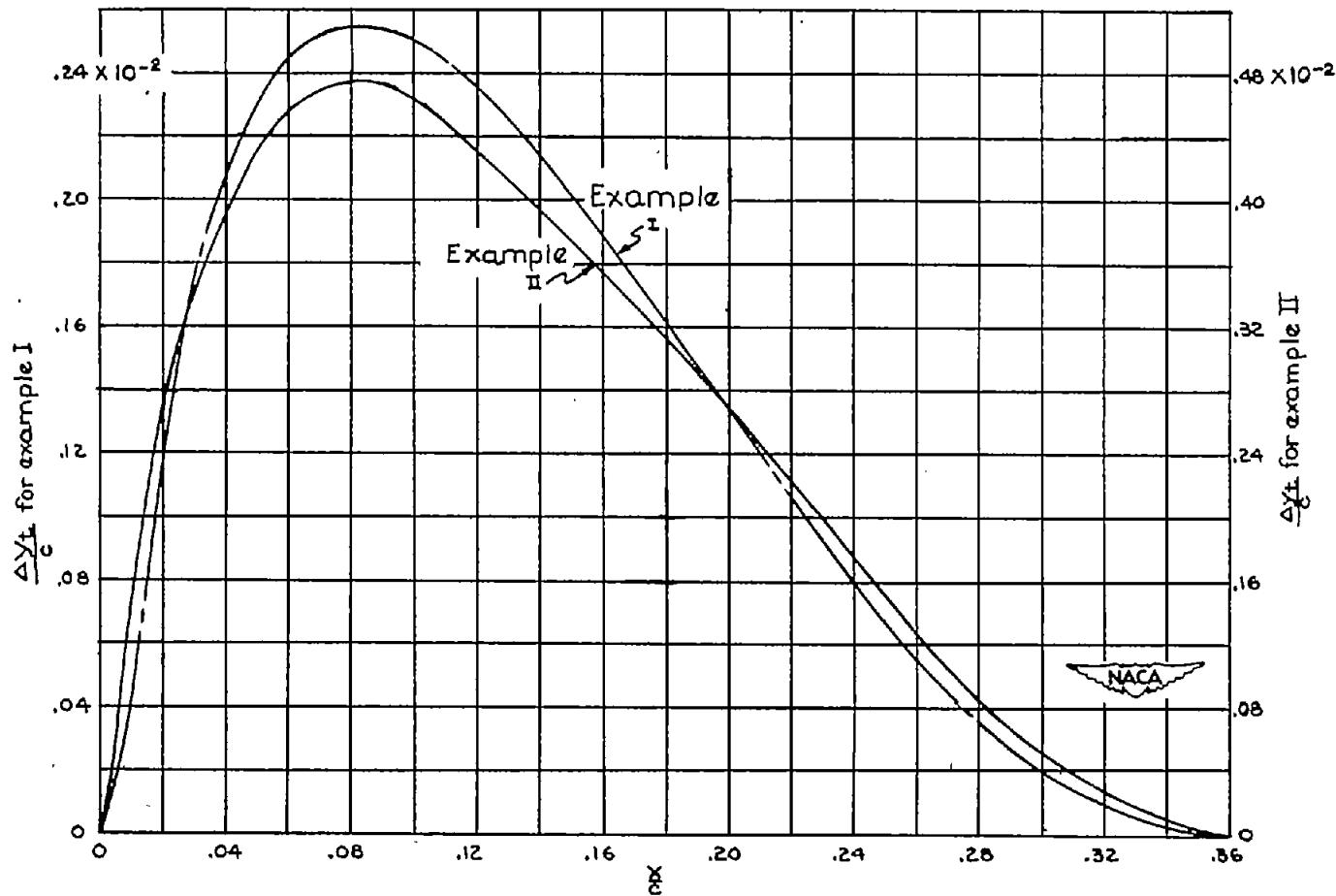
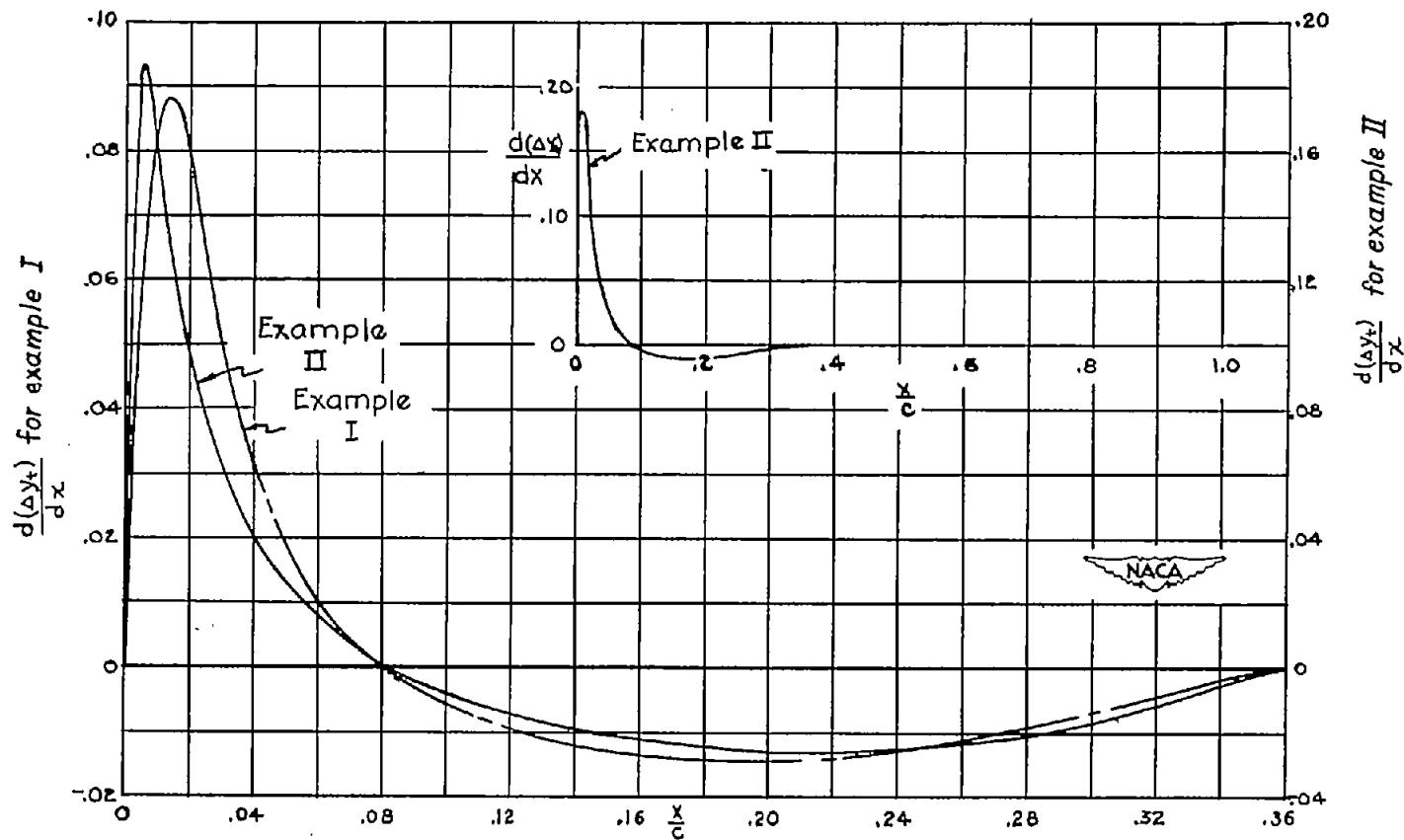
(a) Functions $\Delta y_t(x)$.

Figure 9.- Examples I and II.



(b) $\frac{d(\Delta y_t)}{dx}$ as function of x/c .

Figure 9.- Concluded.

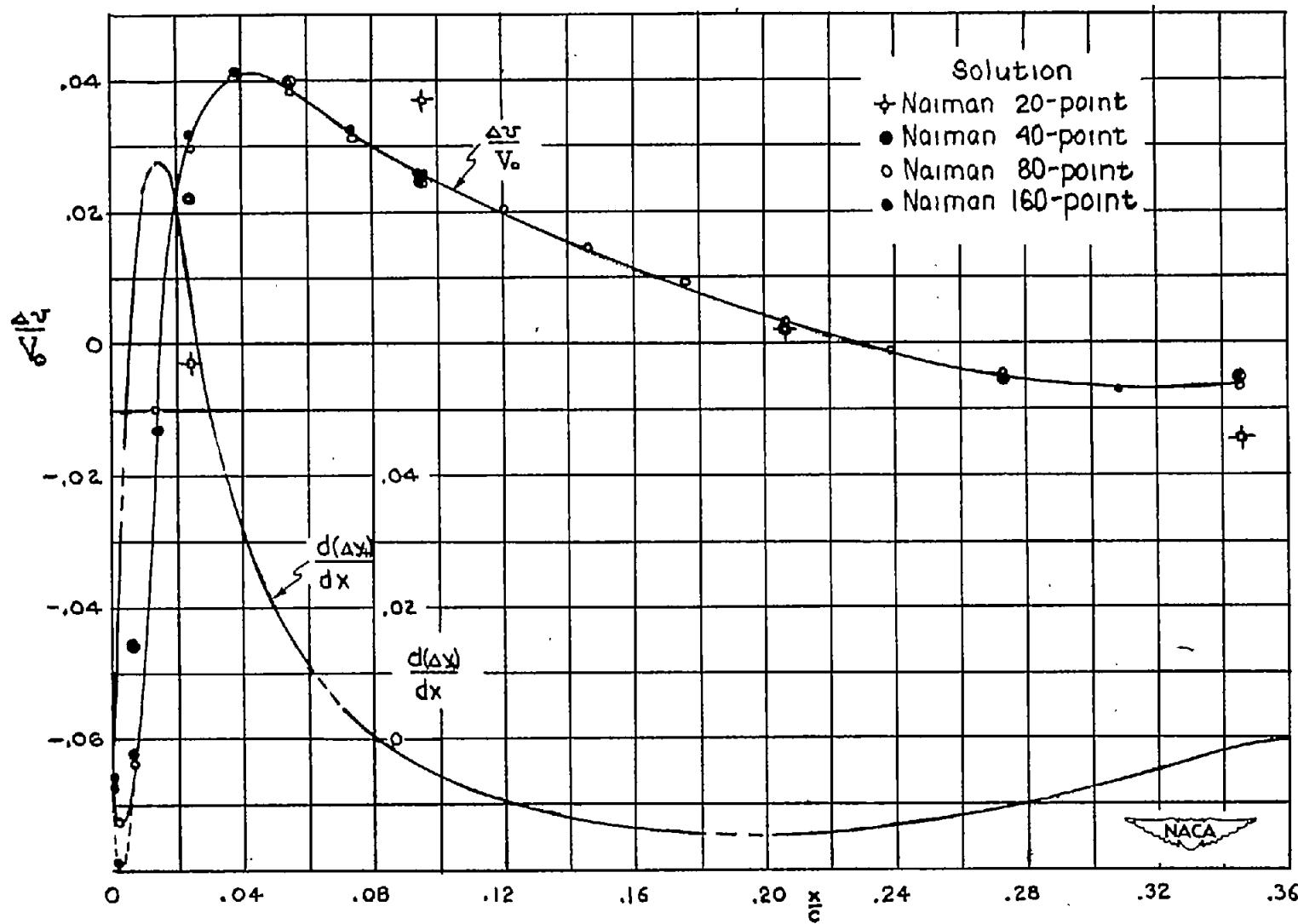


Figure 10.- Direct problem for example I by Naiman's method.

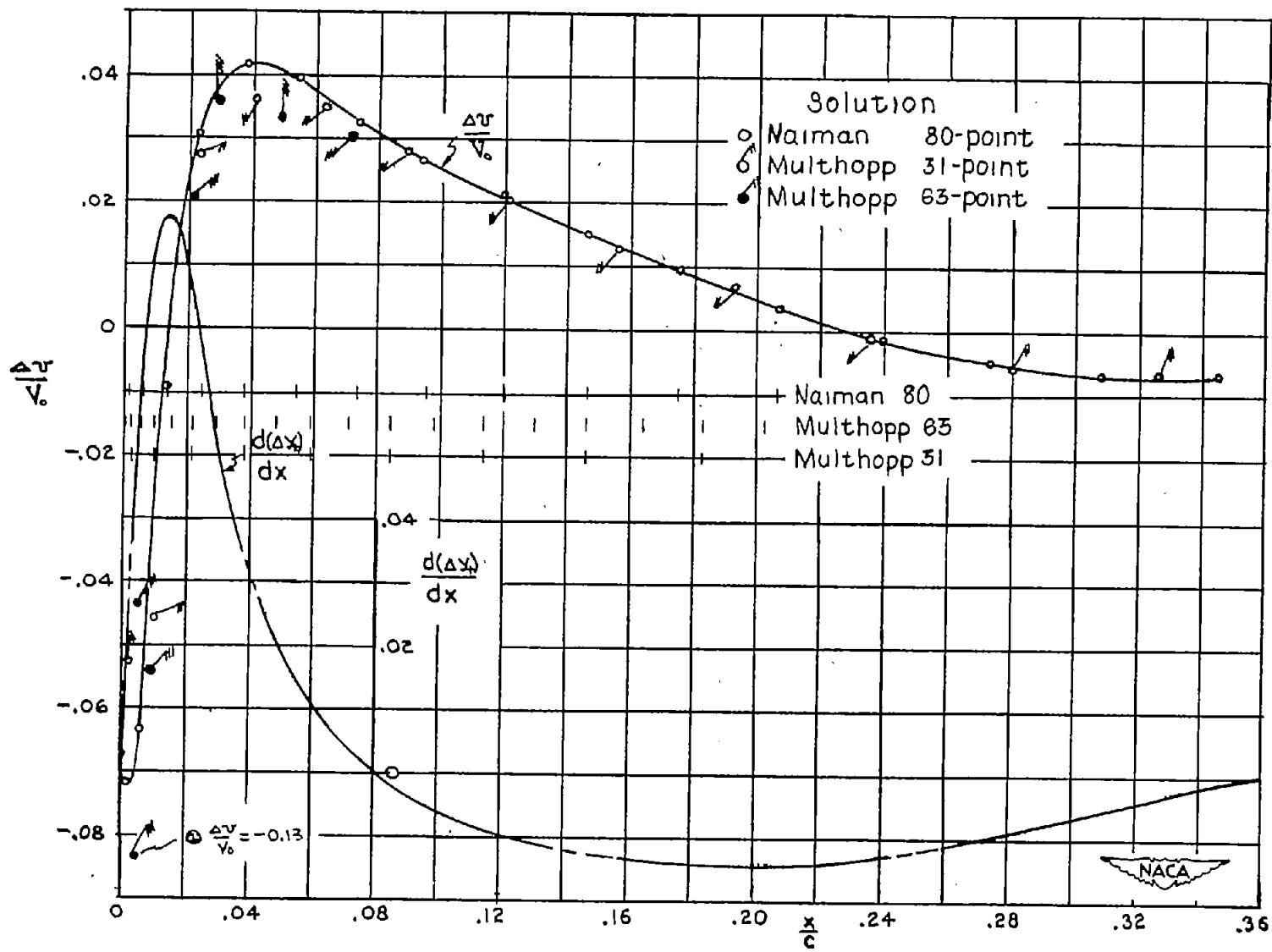


Figure 11.- Direct problem for example I by Multhopp's method.

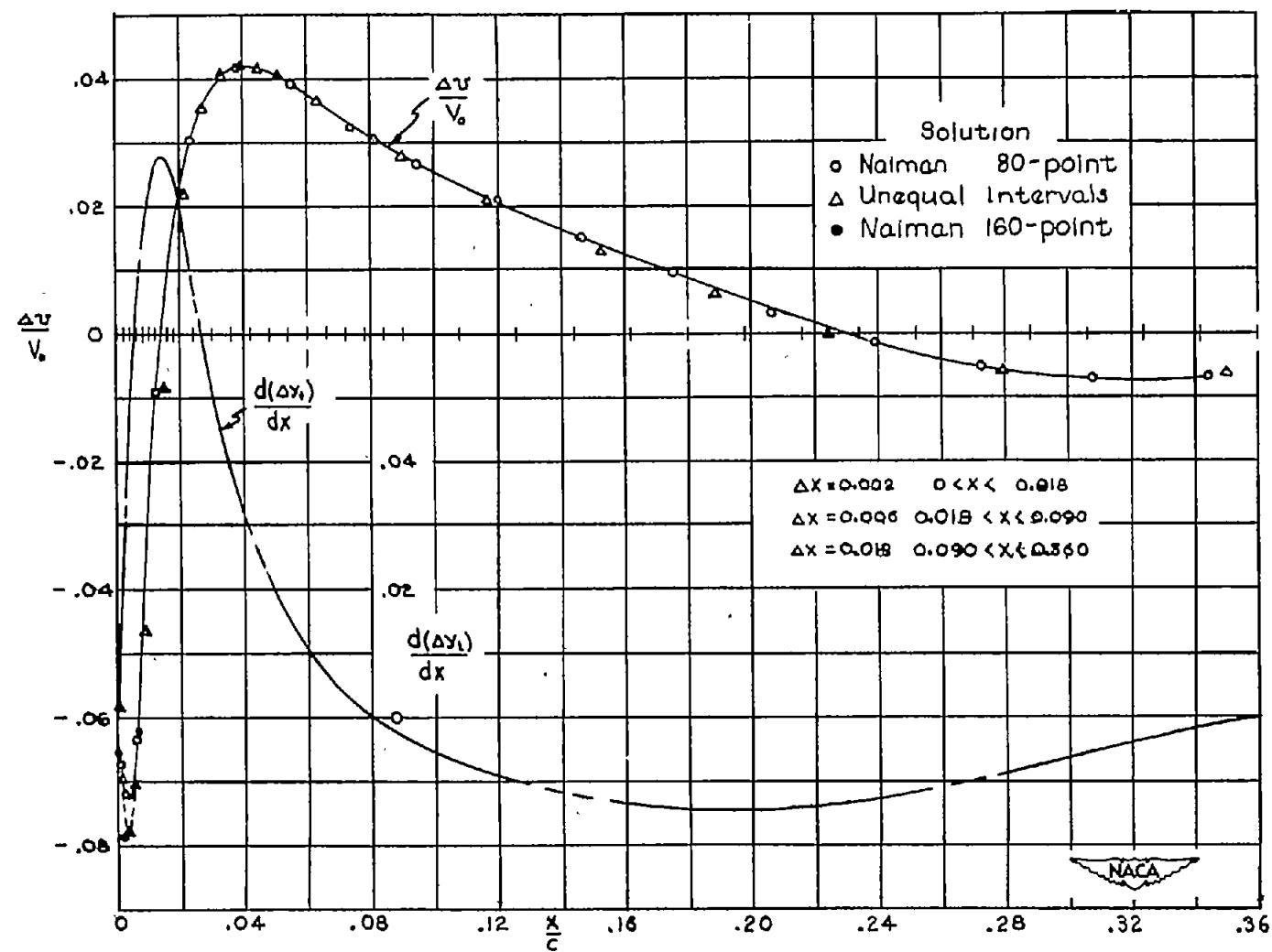


Figure 12.- Results obtained for example I by method of unequal intervals compared with results obtained by Naiman's 80- and 160-point solutions.

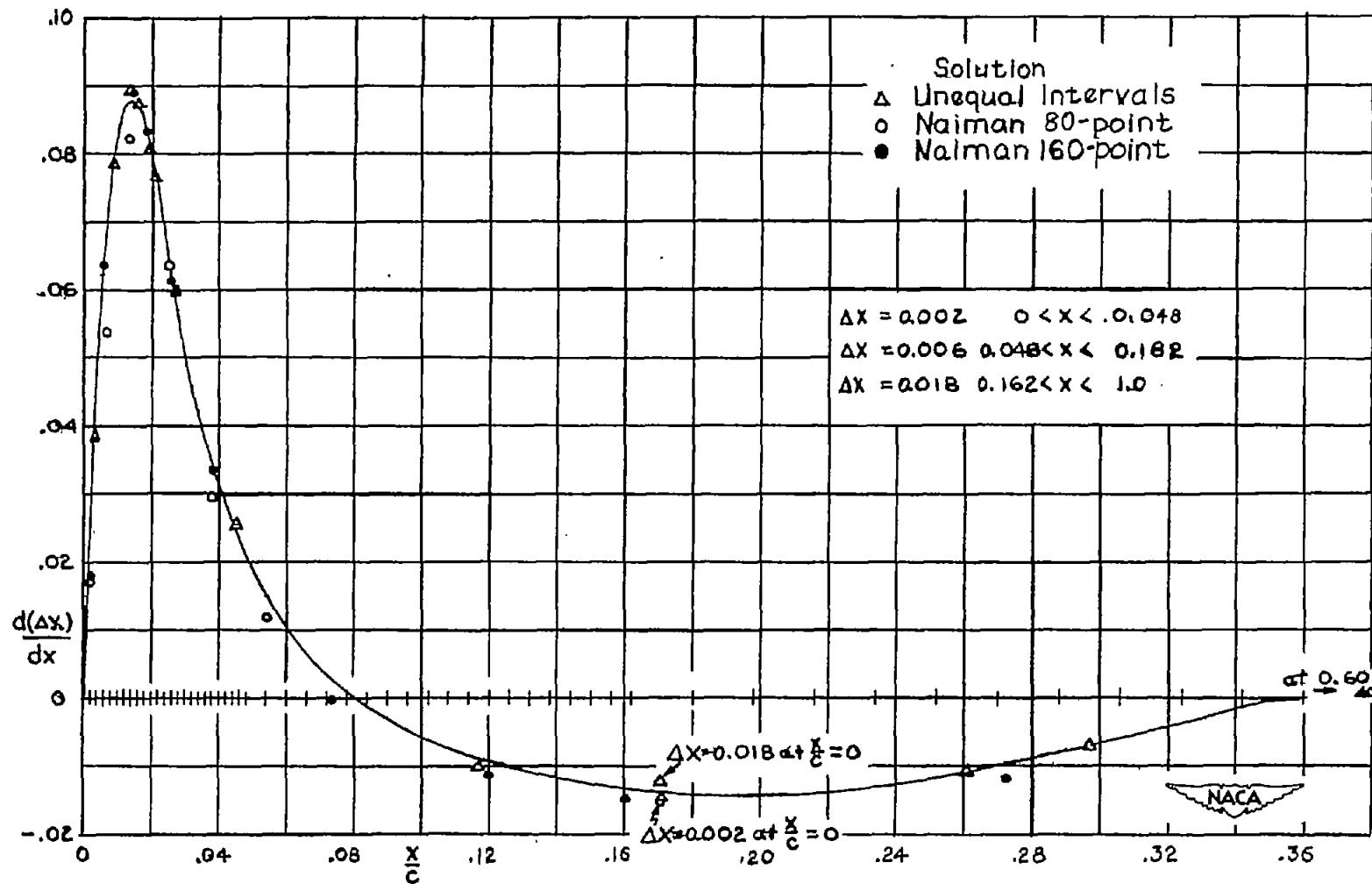


Figure 13.- Solution of inverse problem. Results obtained for example I by method of unequal intervals compared with results obtained by Naiman's 80- and 160-point solutions.

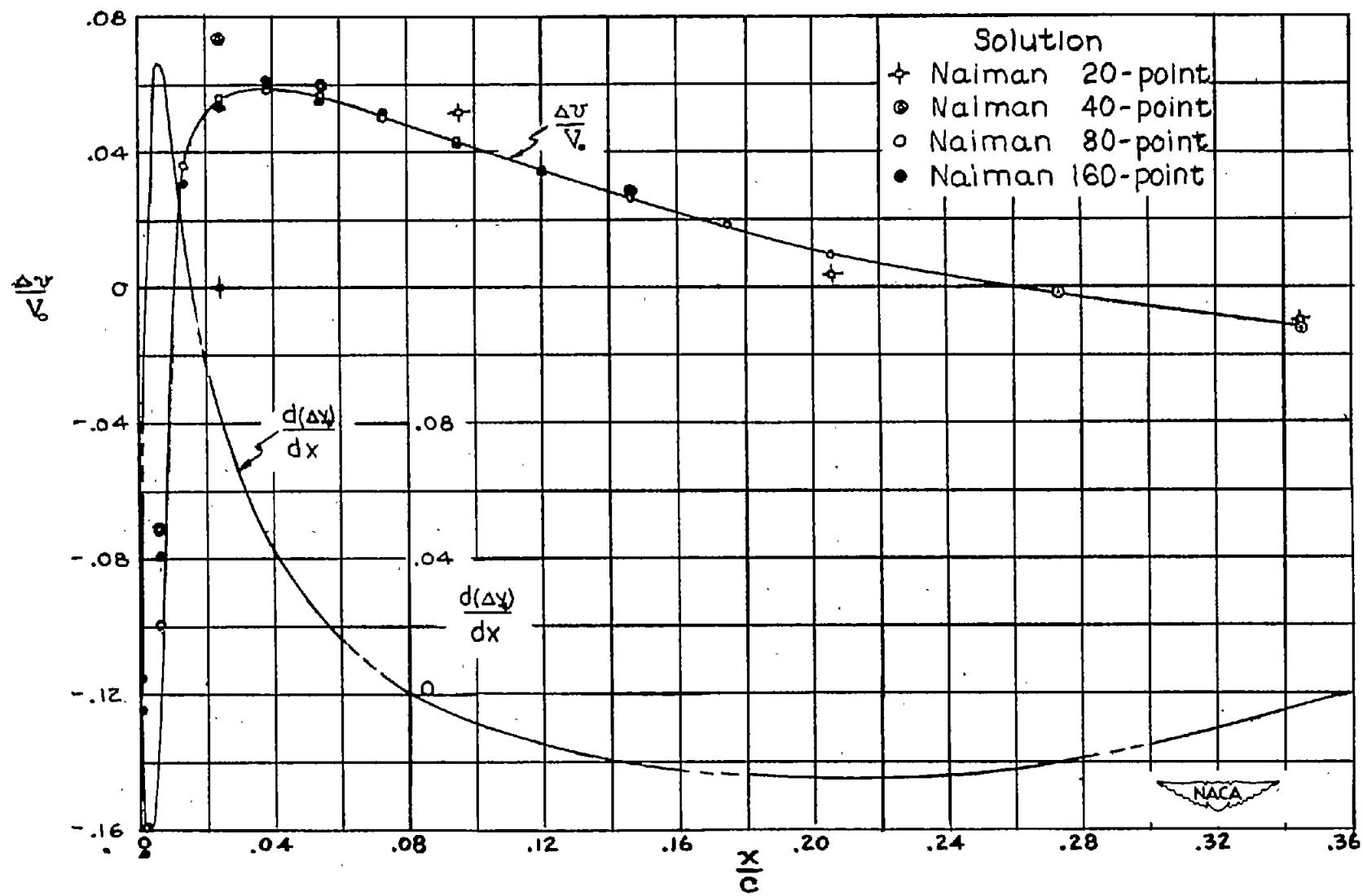


Figure 14.- Direct problem for example II by Naiman's method.

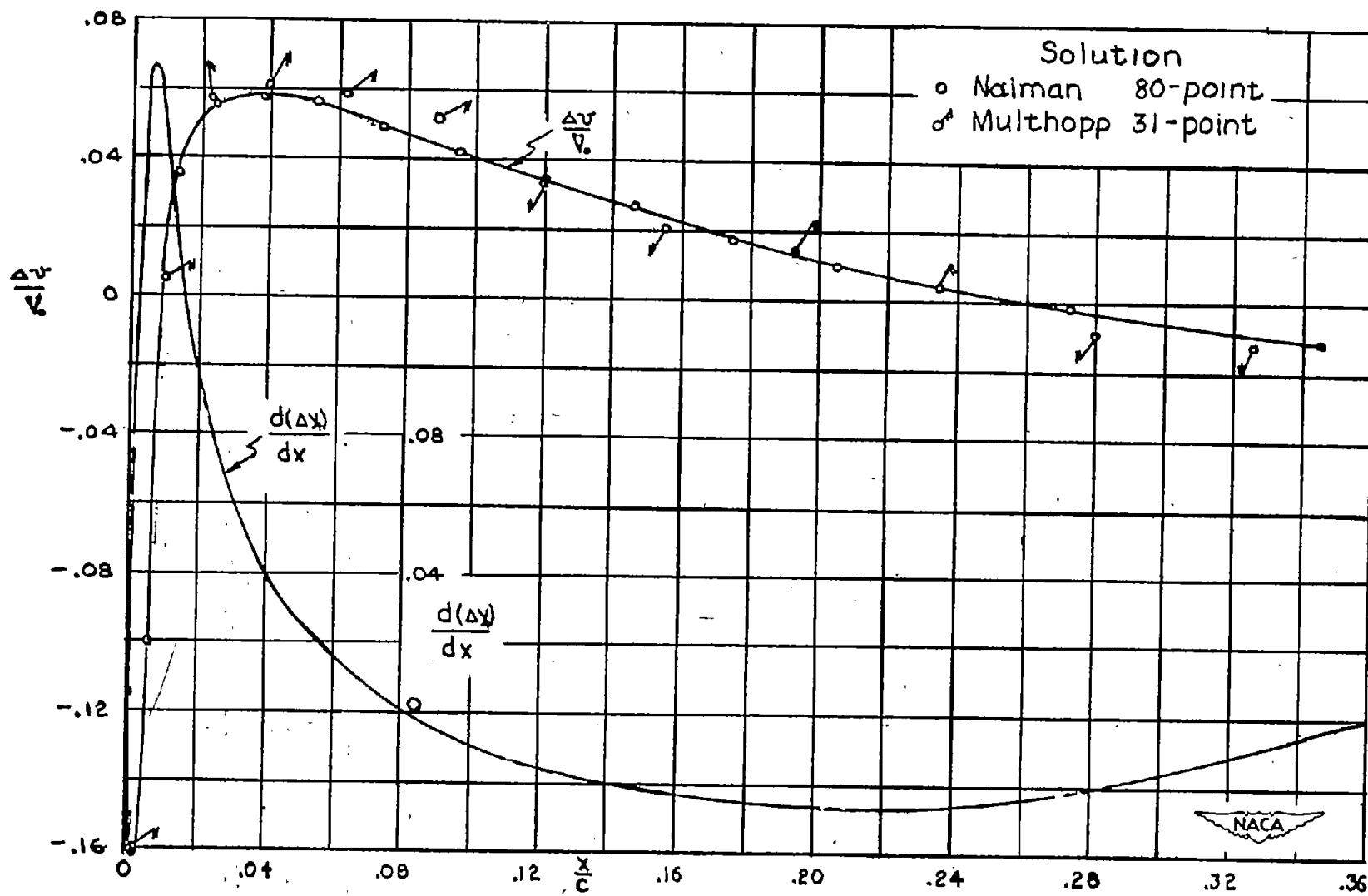


Figure 15.- Direct problem for example II by Multhopp's method.

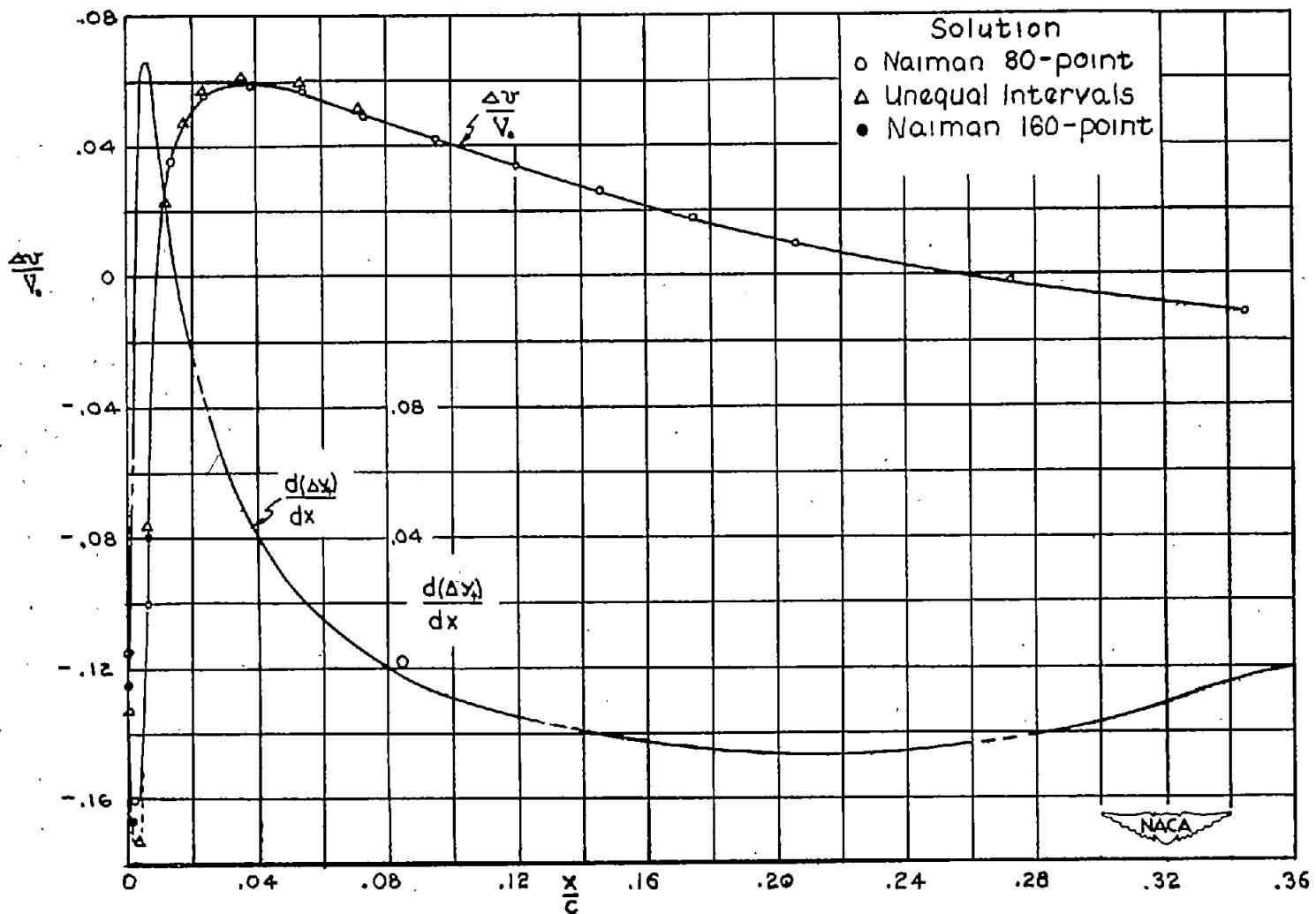


Figure 16.- Results obtained for example II by method of unequal intervals compared with results obtained by Naiman's 80- and 160-point solutions.

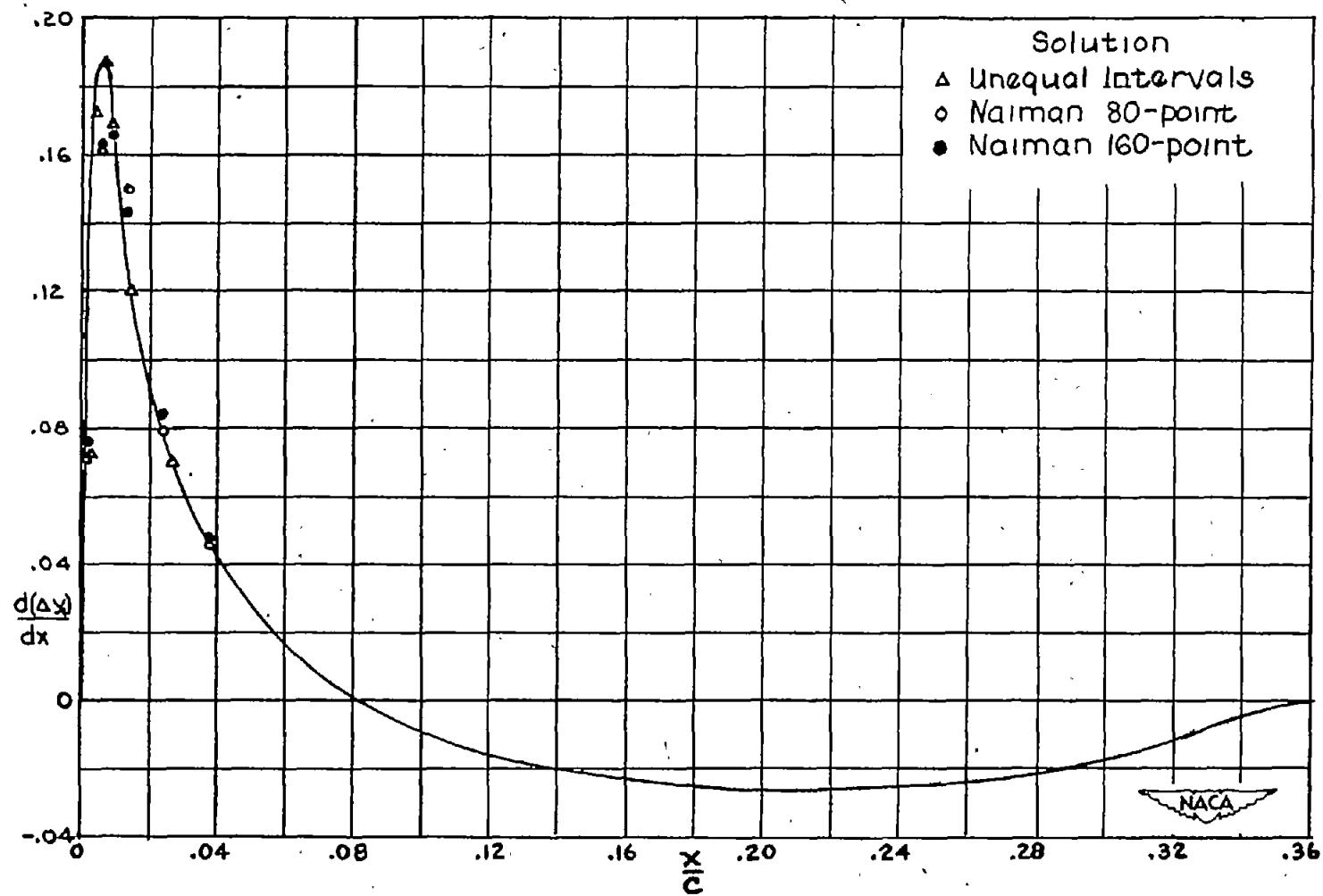


Figure 17.- Solution of inverse problem. Results obtained for example II by method of unequal intervals compared with results obtained by Naiman's 80- and 160-point solutions.

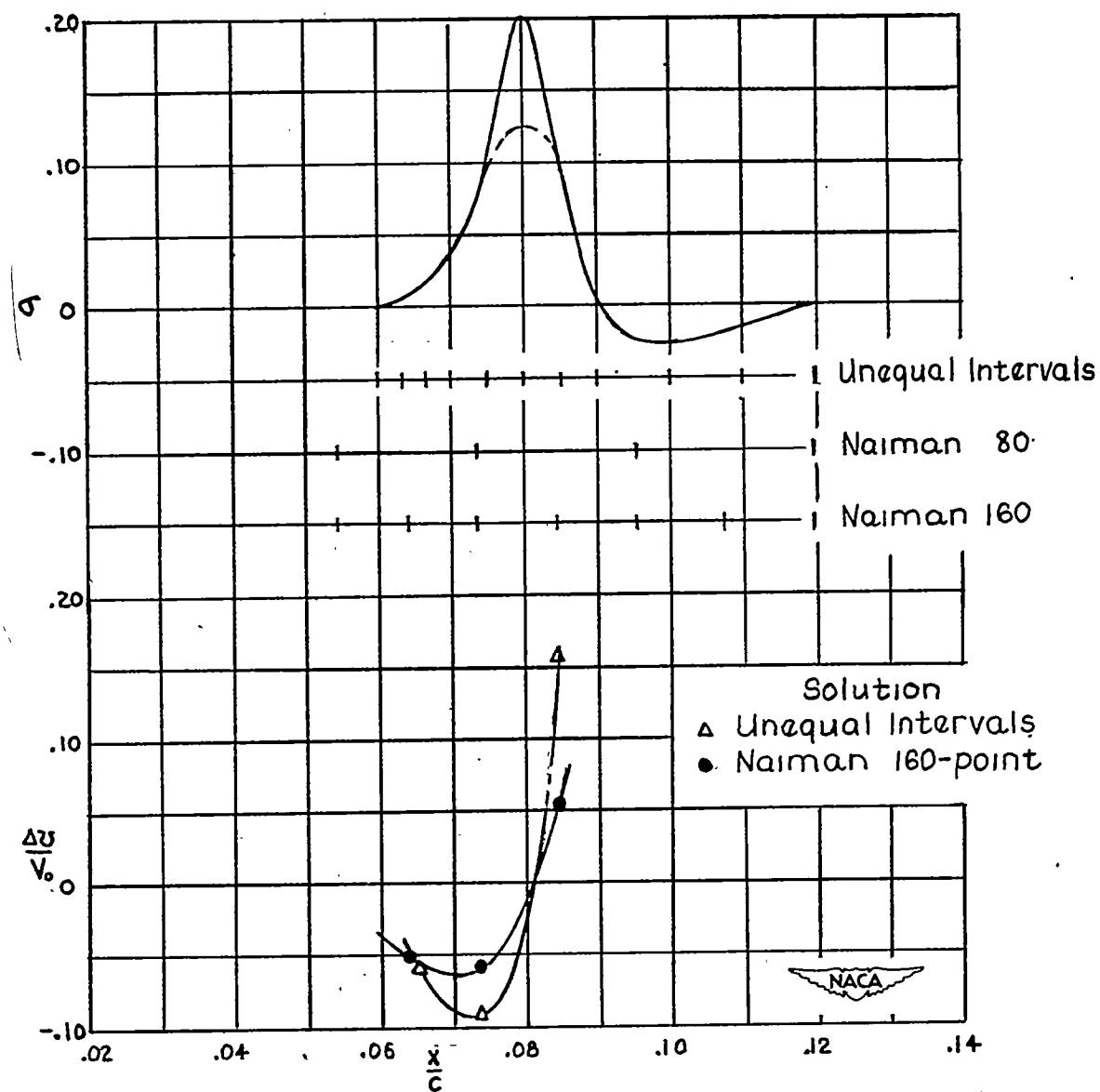


Figure 18.- Results obtained for example III by method of unequal intervals compared with results obtained by Naiman's 80- and 160-point solutions.